New Folder Name DATA BOOK

FILE: T900002

LIGO 40m PROTOTYPE SERVO SYSTEM DATA BOOK

M. E. ZUCKER

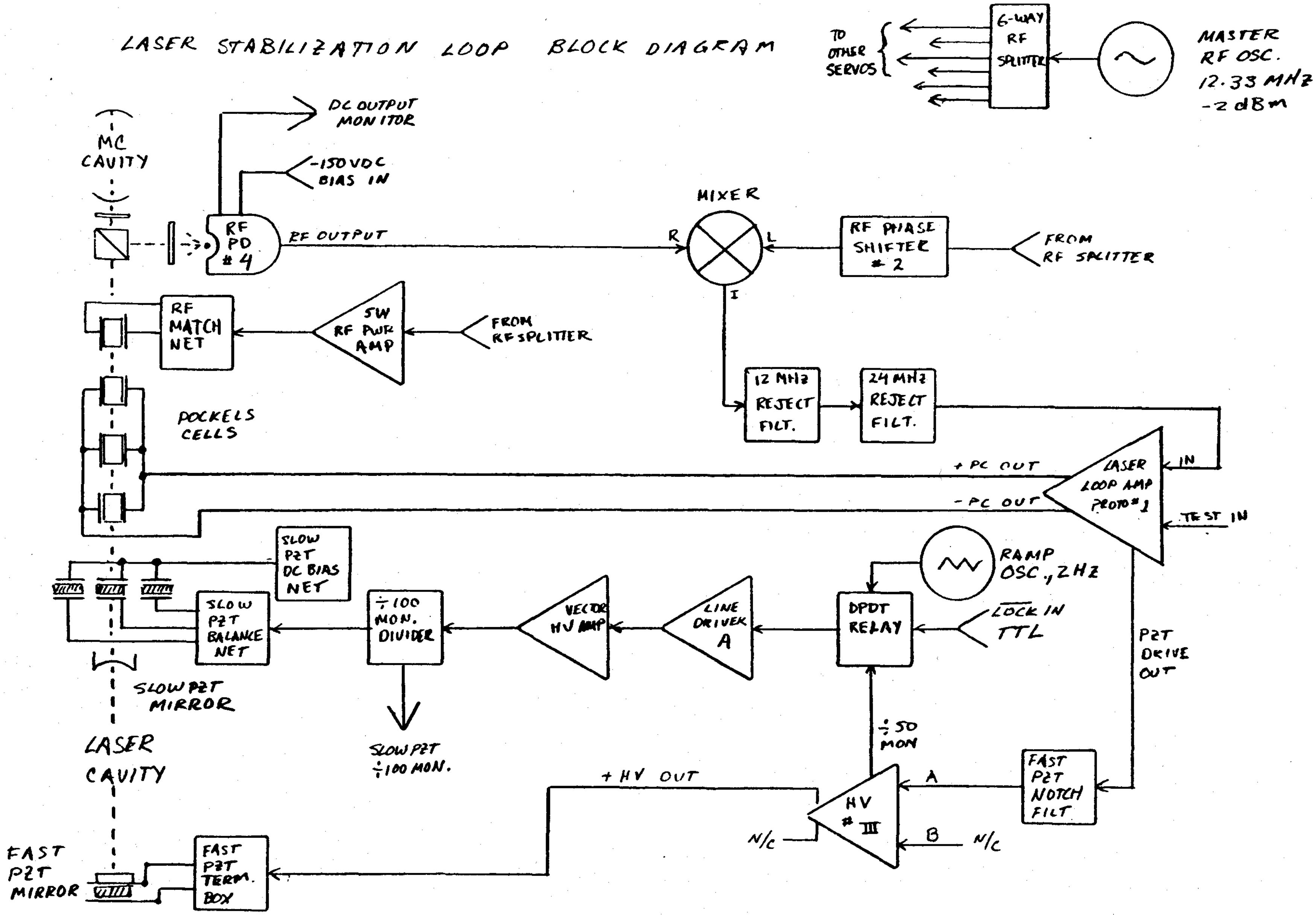
5 DECEMBER 1990

VERSION 1.0

B. LASER LOOP: GENERAL

10/10/90 ME

LASER STABILIZATION LOOP BLOCK DIAGRAM

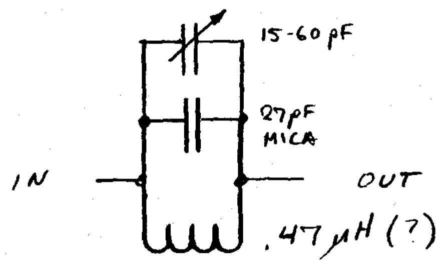


B1

10/10/90 MEZ

LASER STABILIZATION LOOP

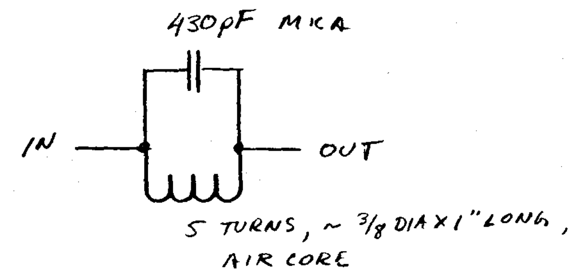
RF REJECTION FILTERS;



12.3 MHz REJECT

-35 dB peak atten

-3dB BW 7MHz - 16MHz



24.6 MHz REJECT

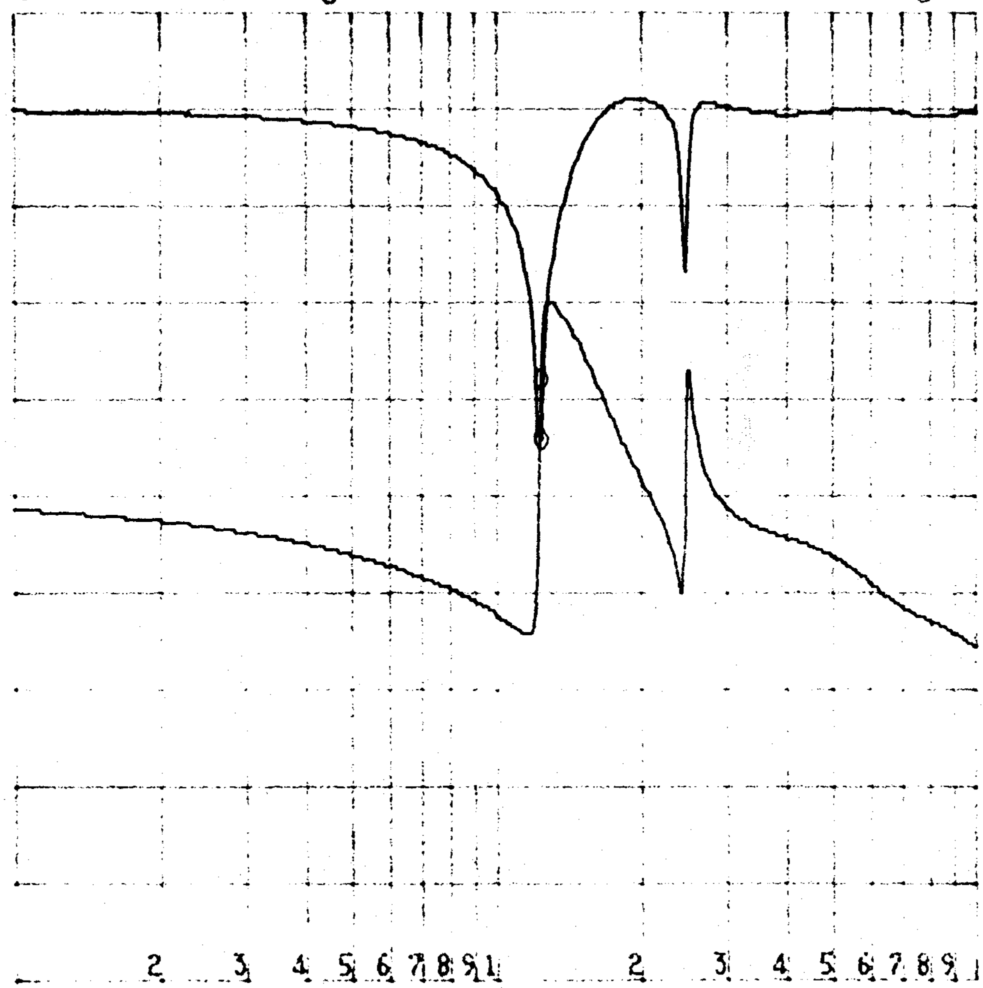
-17 dB peak atten

-3dB BW 23 MHz - 25MHz

TRANSFER FUNCTION OF BOTH IN SERIES
STORED ON HP4195A FLOPPY DISK
DISK LABEL "ZUCKER, START 10/10/90, DISK #1"
FILE NAME "LLNOTCHES1"

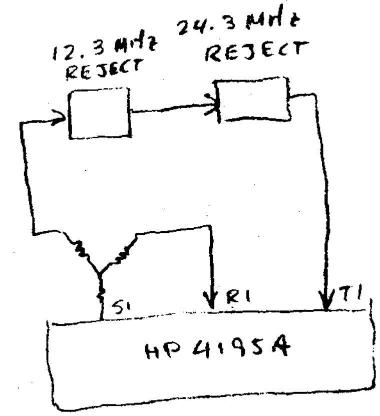
10/10/90 MEZ

NETWORK
A: REF B: REF 0 MKR 12 302 687.708 Hz
10.00 225.0 T/R -34.1216 dB
[dB][deg] θ 54.4350 deg



DIV DIV START 1 000 000.000 Hz
10.00 45.00 STOP 100 000 000.000 Hz
RBW: 1 KHz ST: 4.33 sec RANGE: R= 10, T= 10dBm

TRANSFER FUNCTION,
LASER SERVO LOOP
RF REJECTION
NOTCH FILTERS

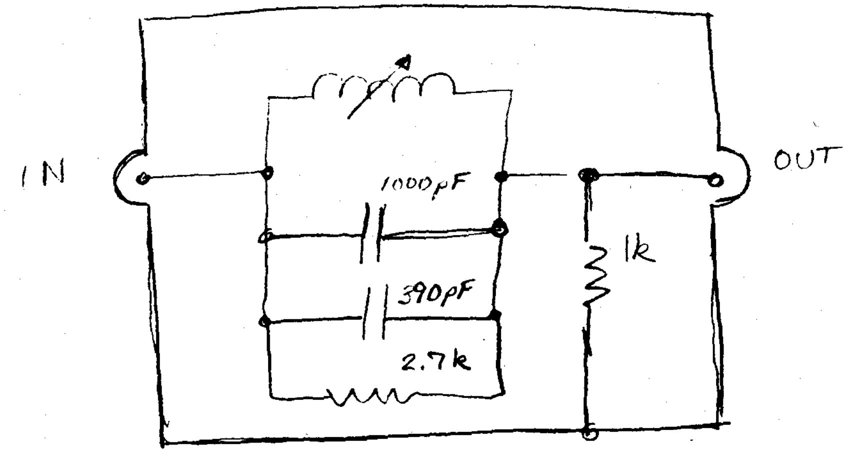


FILE "LLNOTCHES1"
DISK #1, 10/10/90, "ZUCKER"

B3

11/8/90

FAST PZT NOTCH FILTER



B4

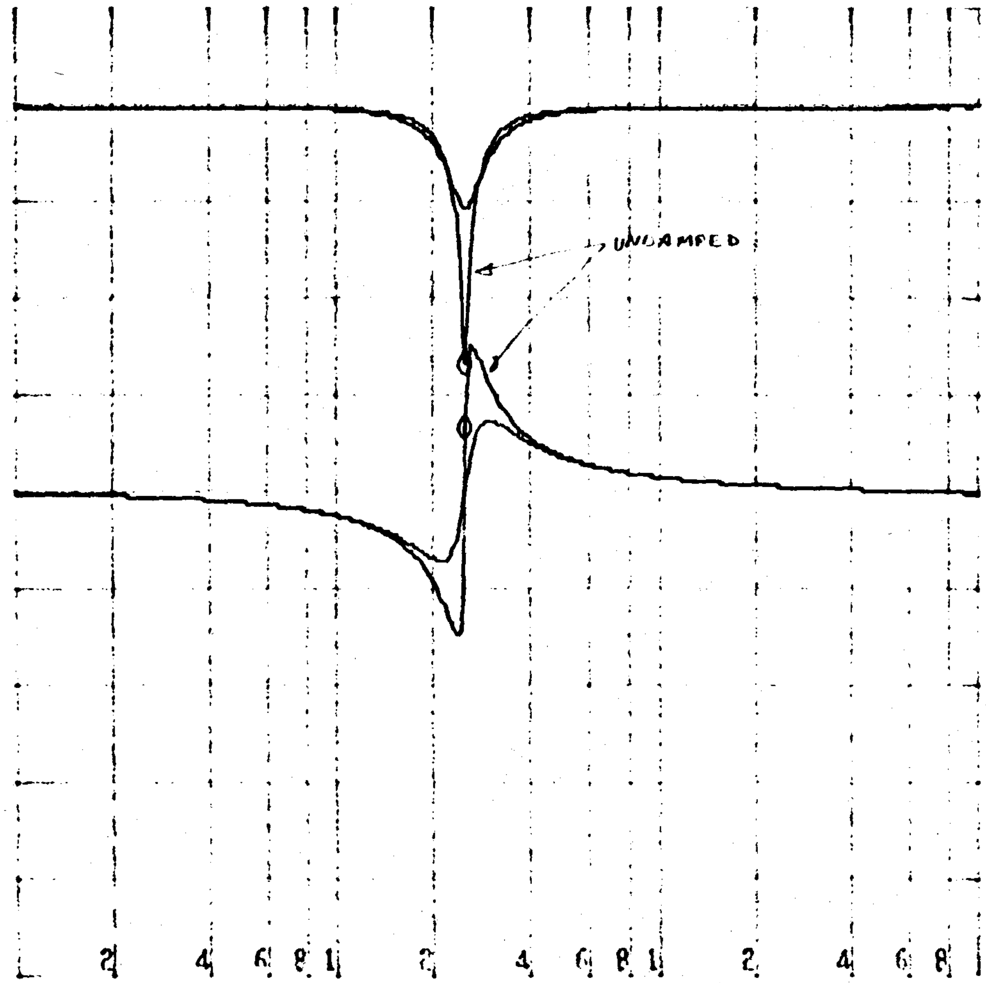
11/6/90 €}

NETWORK Cor

A: REF B: REF 0 MKR 252 638.771 Hz

10.00 225.0 T/R -27.0474 dB

[dB][deg ·] θ 28.8915 deg



DIV DIV START 10 000.000 Hz

10.00 45.00 STOP 10 000 000.000 Hz

RBW: 300 Hz ST: 13.7 sec RANGE: R= 10, T= 0dBm

REF= 1.00000E+01

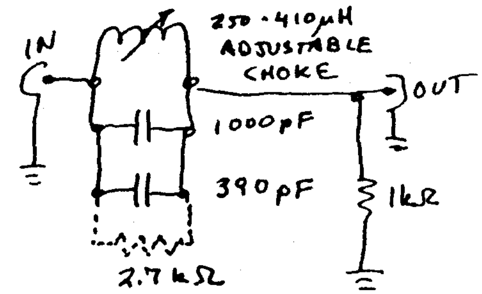
XF

FP2T NOTCH FILTER

RED, BLUE :

AS BEFORE,
NO DAMPING SHUNT

BLACK, PURPLE :
2.7kΩ DAMPING
SHUNT ACROSS LC

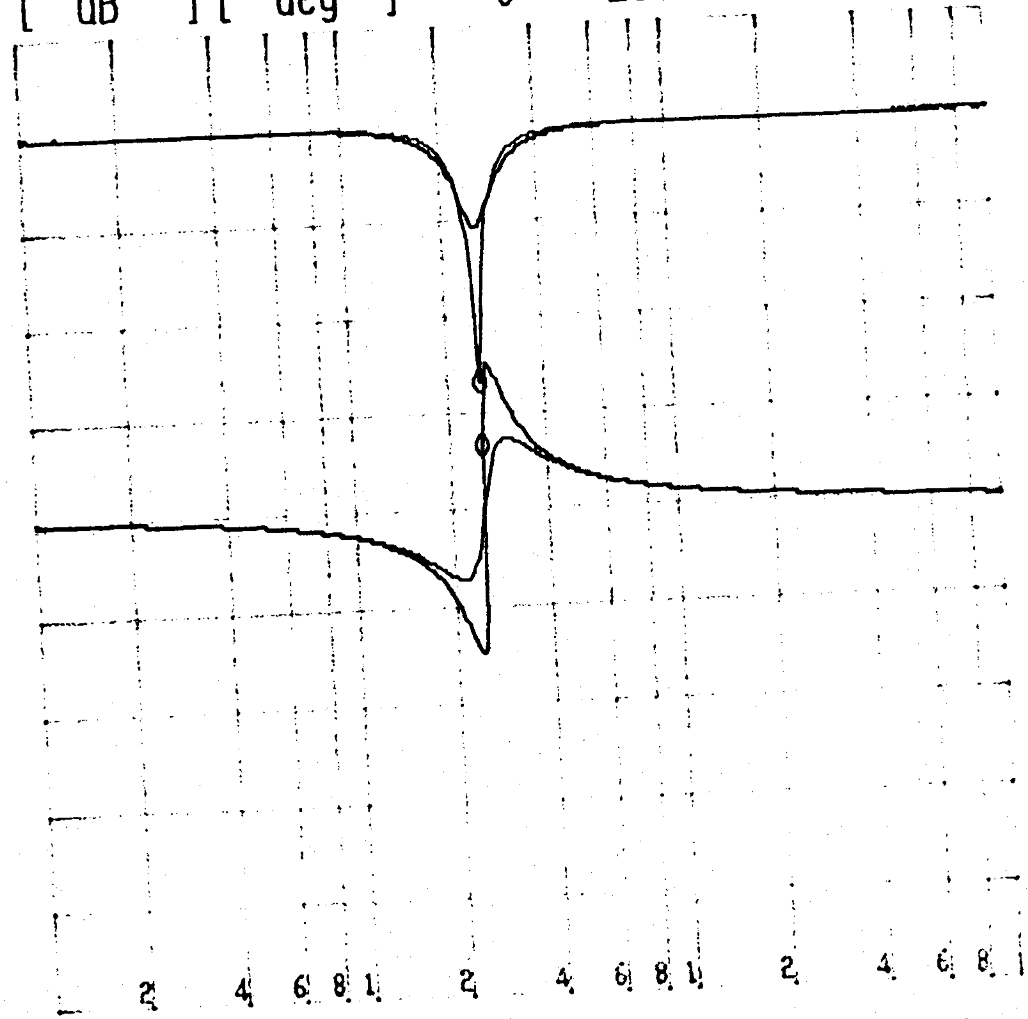


(TEST COND: DRIVEN BY
50Ω SOURCE
OF 4195A & SPLITTER)

B5

11/6/90 me}

NETWORK Cor
A: REF B: REF 0 MKR 252 638.771 Hz
10.00 225.0 T/R -27.0474 dB
[dB][deg] θ 28.8915 deg

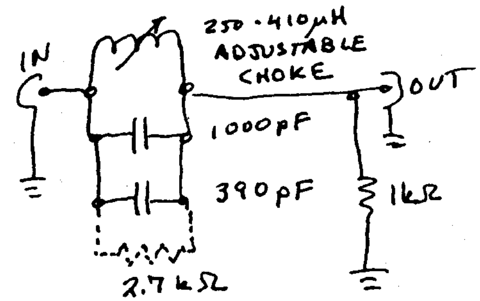


DIV 10.00
DIV 45.00
START 10 000.000 Hz
STOP 10 000 000.000 Hz
RBW: 300 Hz ST: 13.7 sec RANGE: R= 10, T= 0dBm

XF
FP8T NOTCH FILTER

RED, BLUE :
AS BEFORE,
NO DAMPING SHUNT

BLACK, PURPLE :
2.7kΩ DAMPING
SHUNT ACROSS LC



(TEST COND: DRIVEN BY
50Ω SOURCE
OF 4195A + SPLITTER)

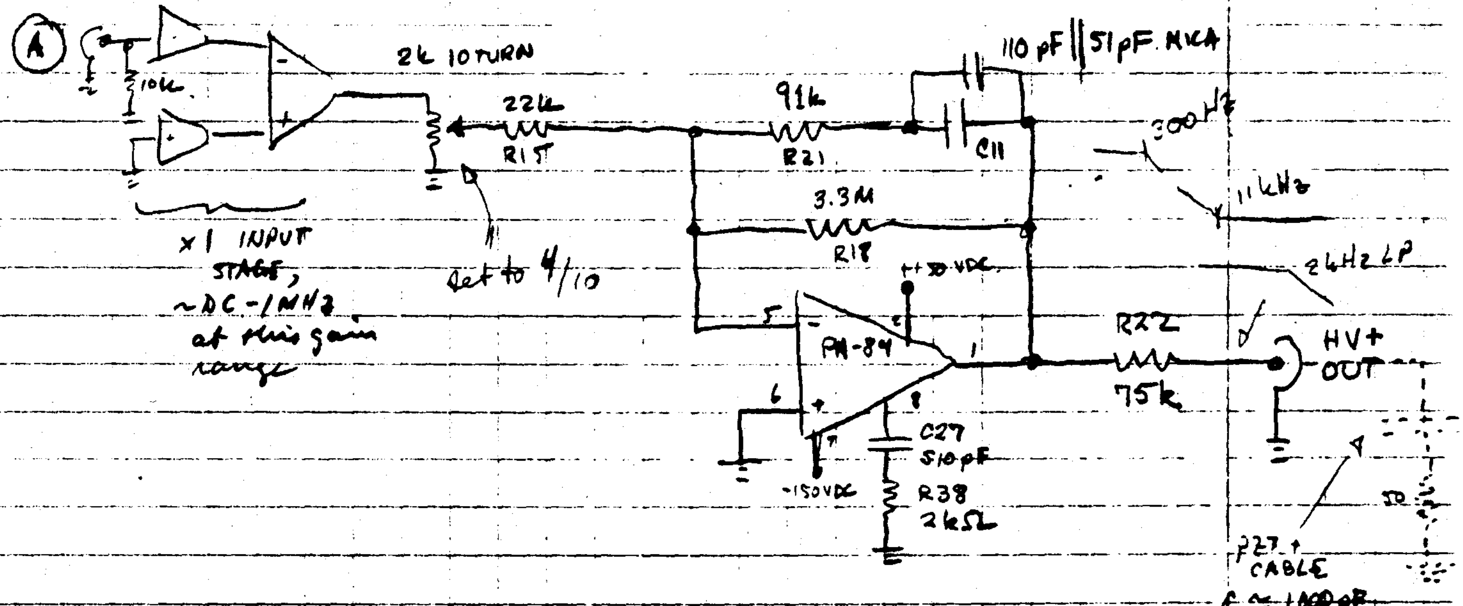
HV # III (PARTIAL SCHEMATIC)

10/25/89

Temporarily setting aside the mystery of the loop gain measurement discrepancy, decided to work on improving laser stabilization loop some more.

JH and BT improved on loop gain by improving the PZT drive amplifier. Previously HV #1 had been used, range x1, vernier + 2/10, ⇒ DC Gain ≈ 6 dB effective single pole (due to $Z_{out} \approx 160\,k\Omega$ / $Z_{PZT} \approx 800\,pF$) @ 1 kHz, extra phase shift at 100 kHz of about 20° due to strays in amplifier circuit (5 pF // 330k ⇒ 100 kHz due to strays across FB loop!)

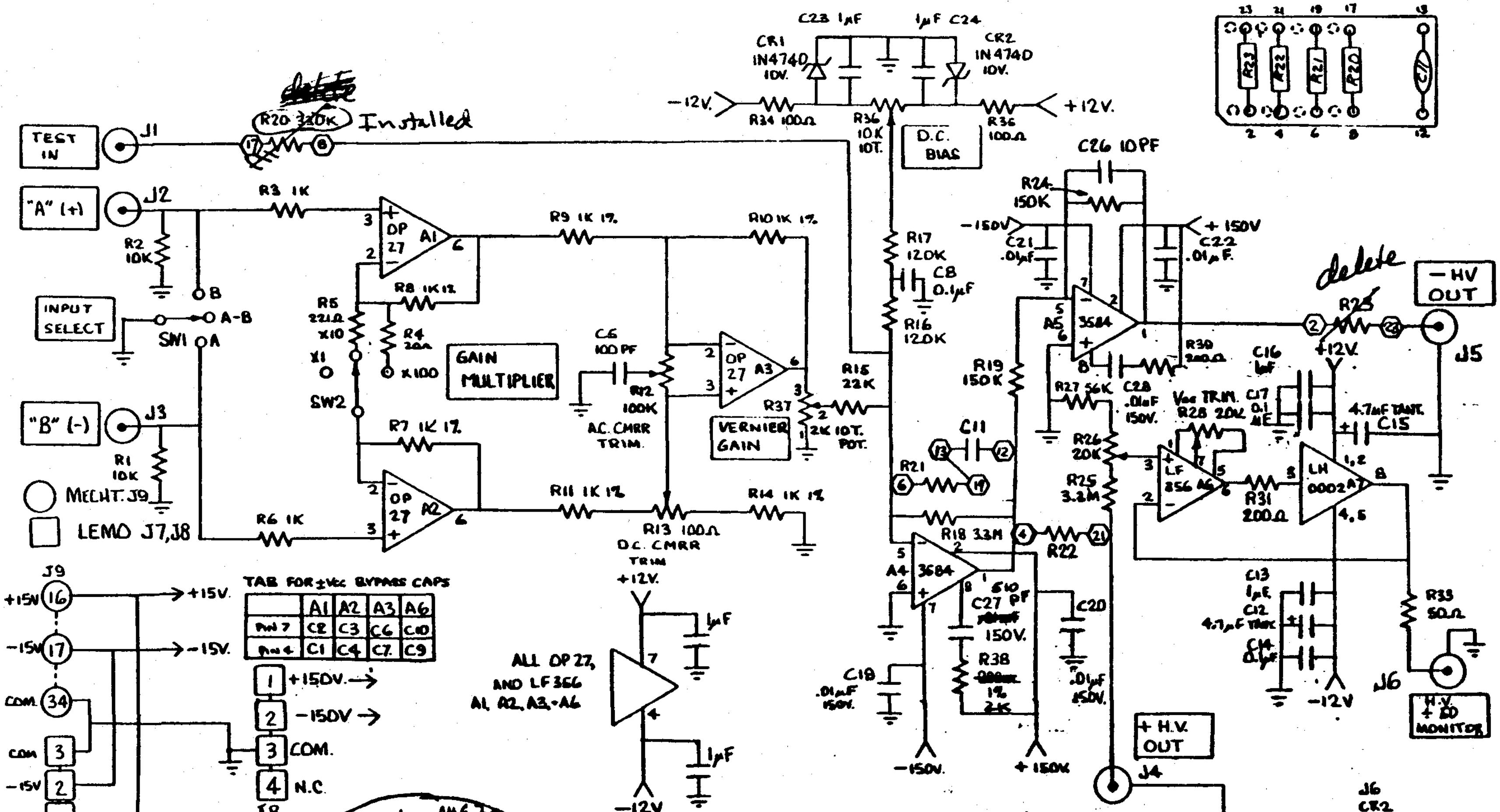
Installed improved circuit (abbreviated diagram below, complete diagram + tfer-function to follow)



HV # III
AS CONFIGURED 10/24/89 FOR SUCCESSFUL LOCKING IN LASER STABILIZATION SERVO LOOP

NB) ÷50 mon. still drives line driver + "Vector" HV amp exactly as before.

HV # III INSTALLED 10/24/89 TO DRIVE FAST PZT MIRROR IN LASER LOOP



	A1	A2	A3	A6
Pin 7	C2	C3	C6	C10
Pin 4	C1	C4	C7	C9

10/24/89 ME
SETTINGS:
INPUT → "A"
MULTIPLIER → x1
VERNIER → 4.0/10

NOTES 1. ┌J┐ INDICATES JUMPER TO SHORT
2. J7, J8, and J9 ARE ALL MOUNTED ~~ON BACK PANEL~~

LAST: J6, CR2, A7, C28, R39
NO'S SKIPPED: C25, C18, R32, R30, R29

SMARTWRK FILE C:\SMARTWRK HVAMP.PCB
DRAWN FROM E. LINDELEF OF 9-1-87 PRO HVAMP.PL
ADDED COMP CARRIED PIN NO'S TO DWG
REPLACES 87-0901-1

CALIFORNIA INSTITUTE OF TECHNOLOGY
GRAVITATIONAL PHYSICS

HV AMPLIFIER ± 150V.

DRAWN BY B.TINKER	DATE 3-4-88	DRAWING NO.	
CHECKED BY	SCALE		
APPROVED BY	W.O.		

88-0304-1

R20 = 330K
C11 = ~~51pF~~ → 150 pF 10/24/89 ME
R21 = 91K
R22 = 75K
~~R23~~ R23 } not used

MODIFIED 10-2?-89 B.T.

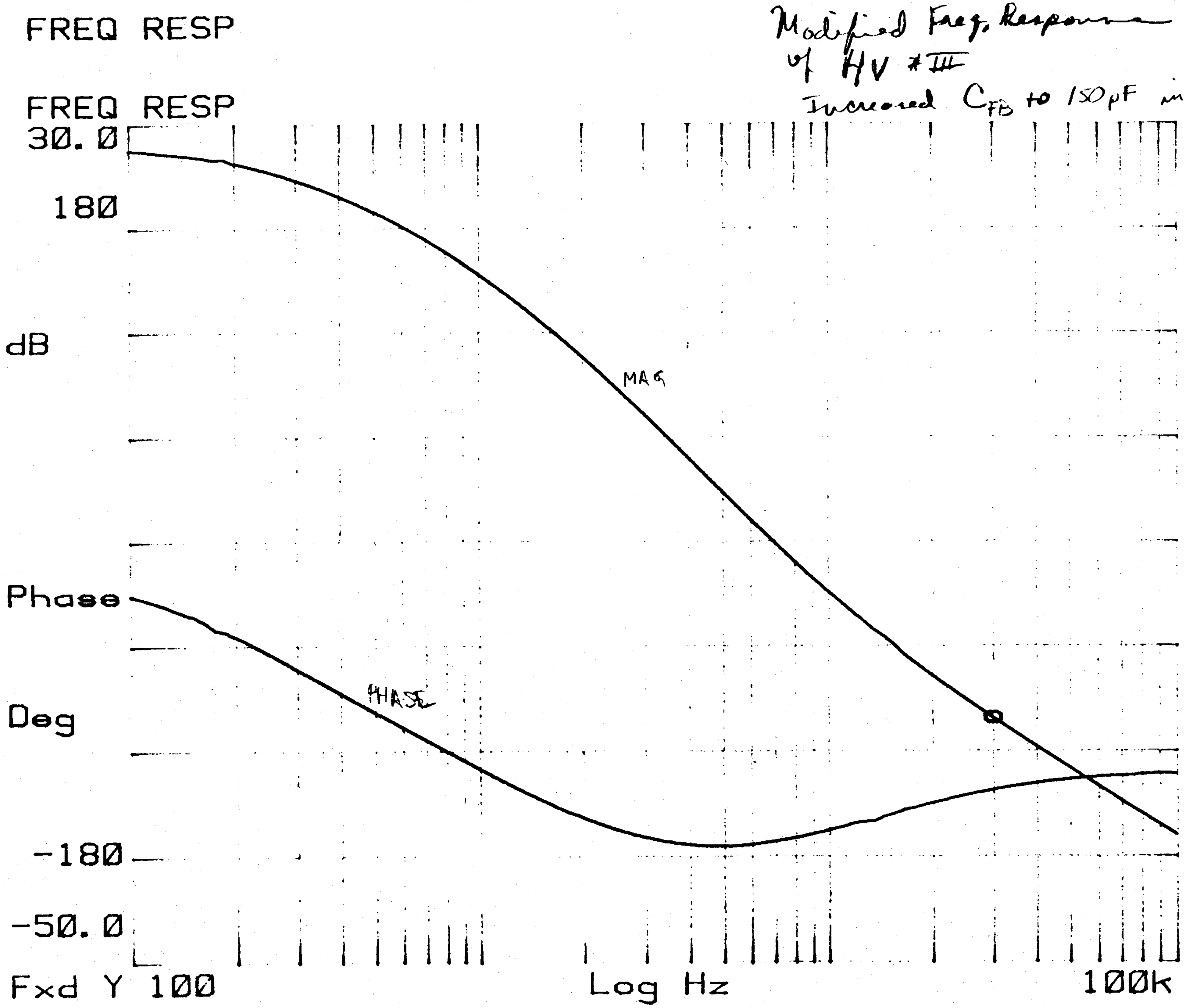
	WAS	IS
C27	.01μF	510pF
R38	200Ω	2K 1%

MOD. 1 S/N. 3

X=29.854kHz
Ya: 5.758 dB

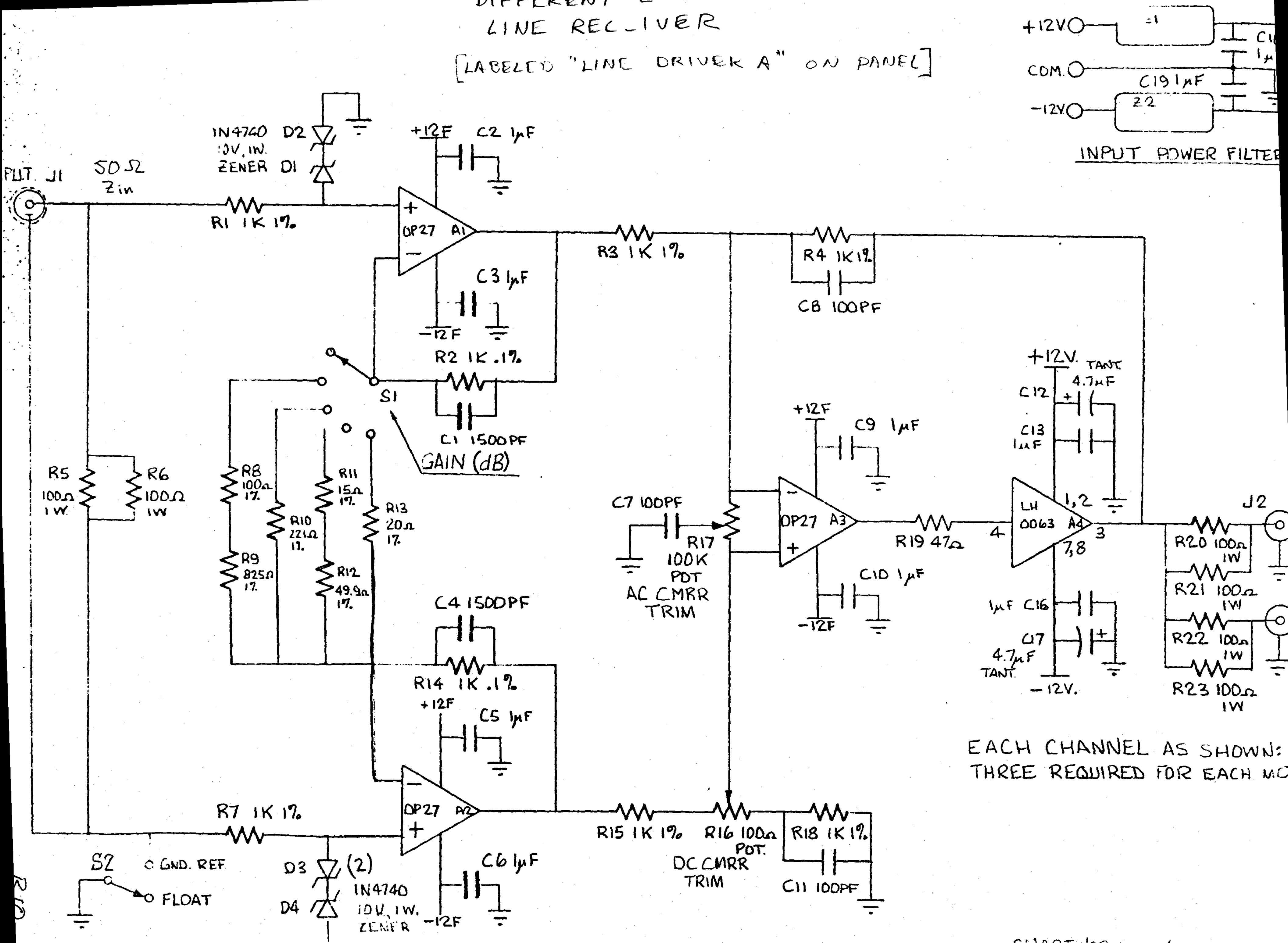
(3) 10/24/89 15:41

Modified Freq. Response of HV #III
Increased C_{FB} to 150pF in PA-84 Ckt.



DIFFERENT L
LINE REC-IVER

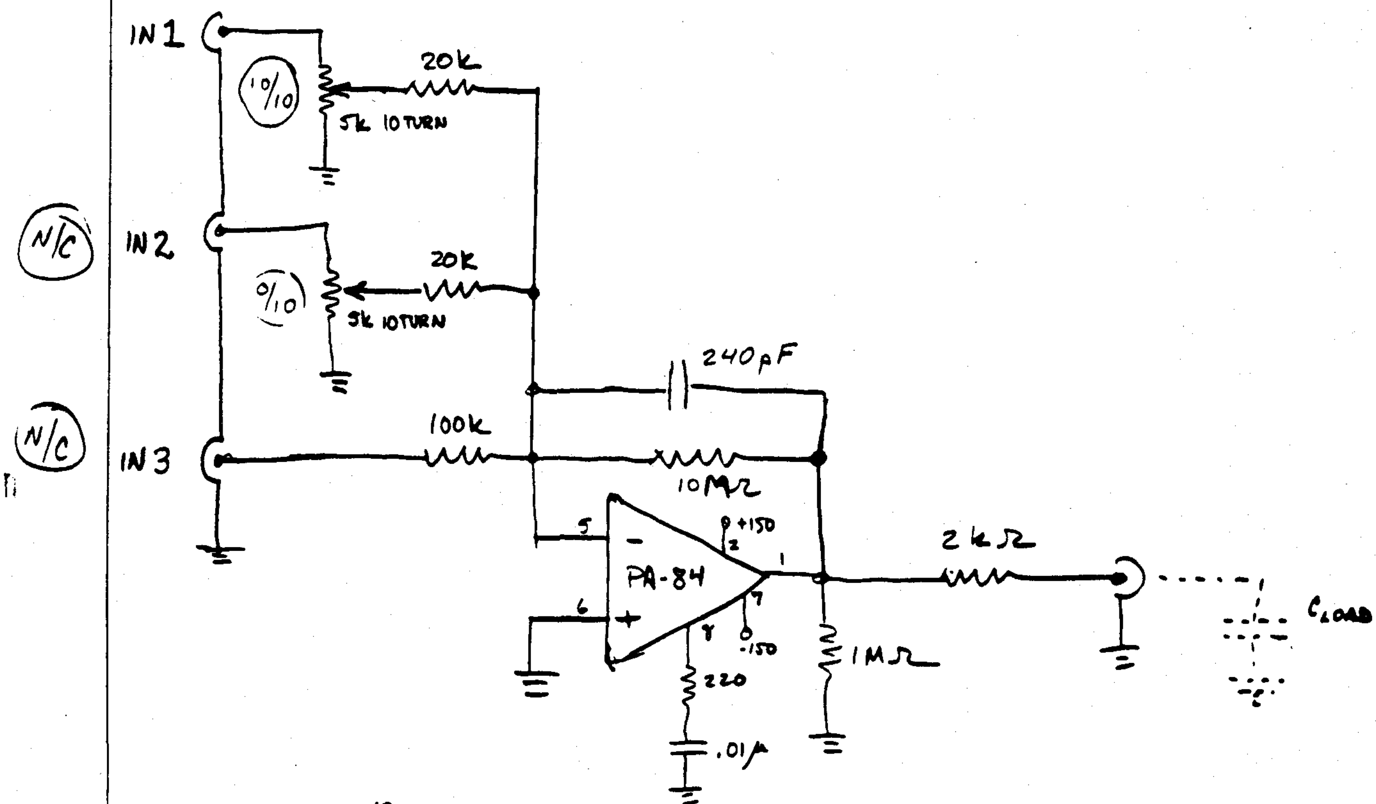
[LABELED "LINE DRIVER A" ON PANEL]

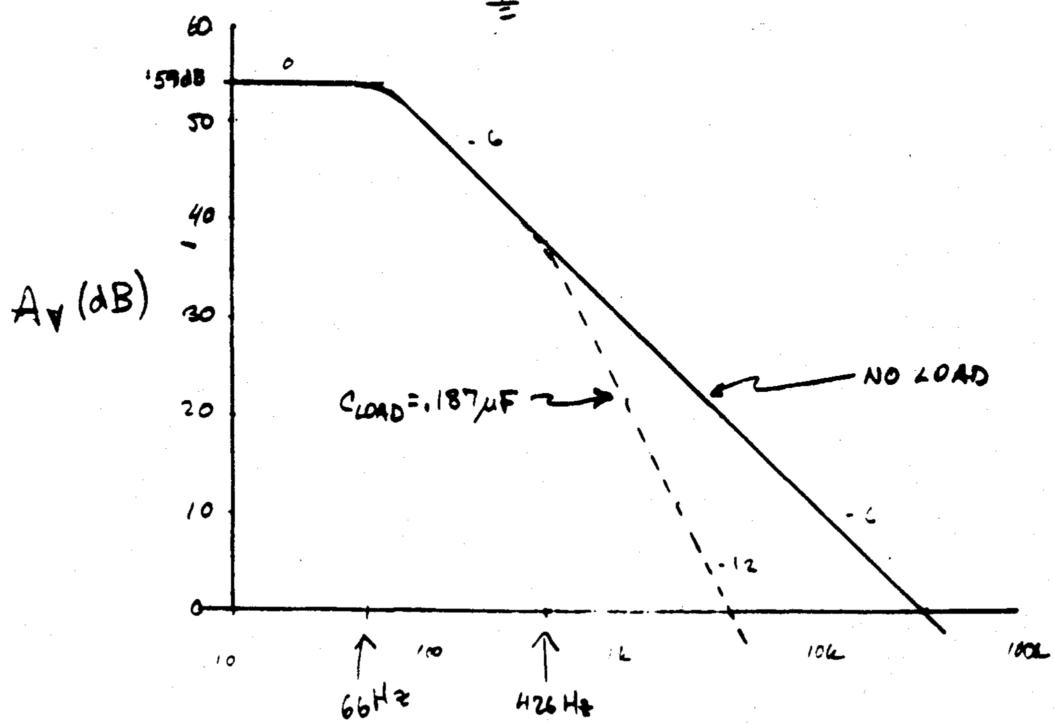


EACH CHANNEL AS SHOWN:
THREE REQUIRED FOR EACH MO

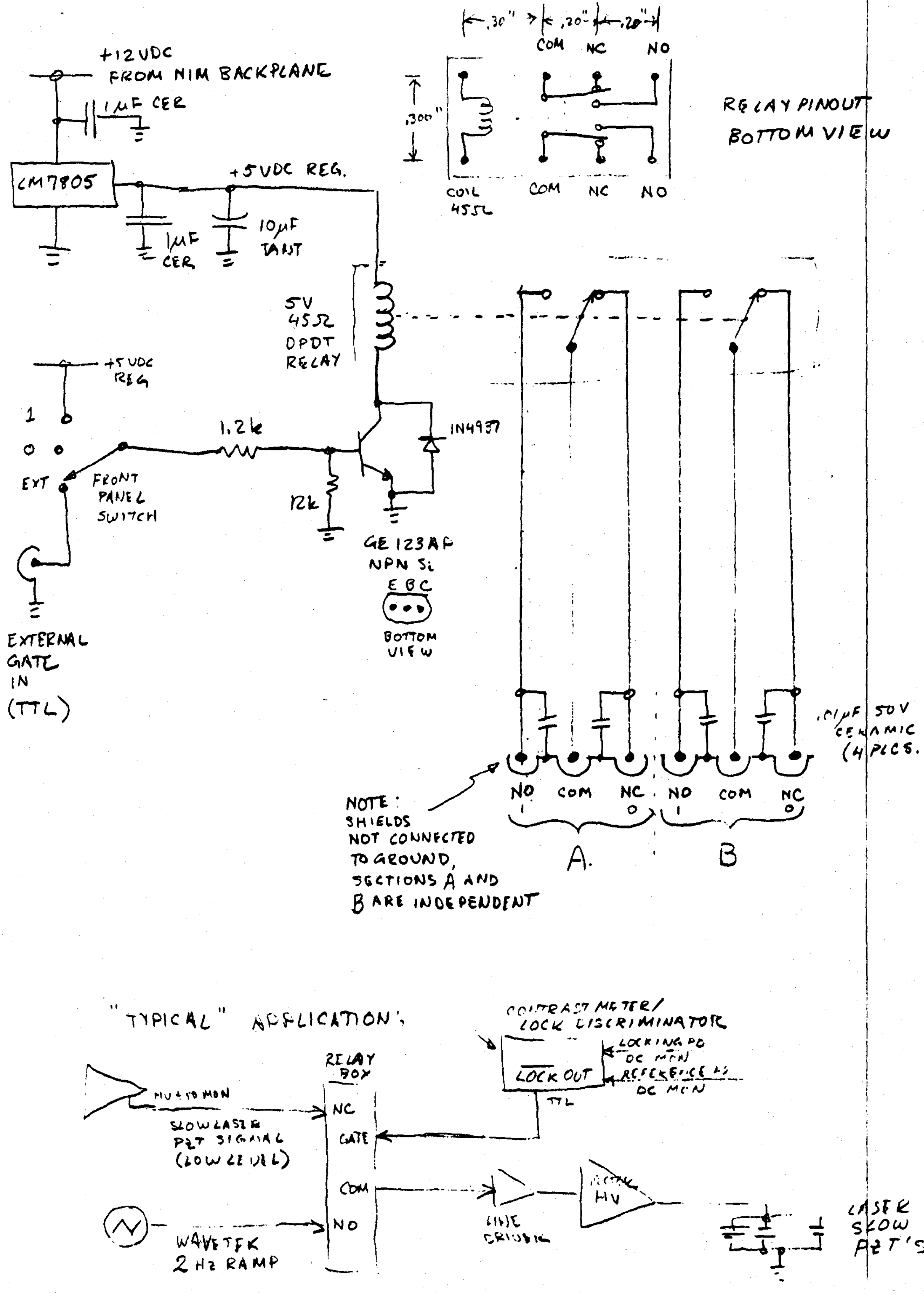
11/15/88 MEZ

MODE CLEANER SERVO LOOP "VICTOR H.V. AMP"



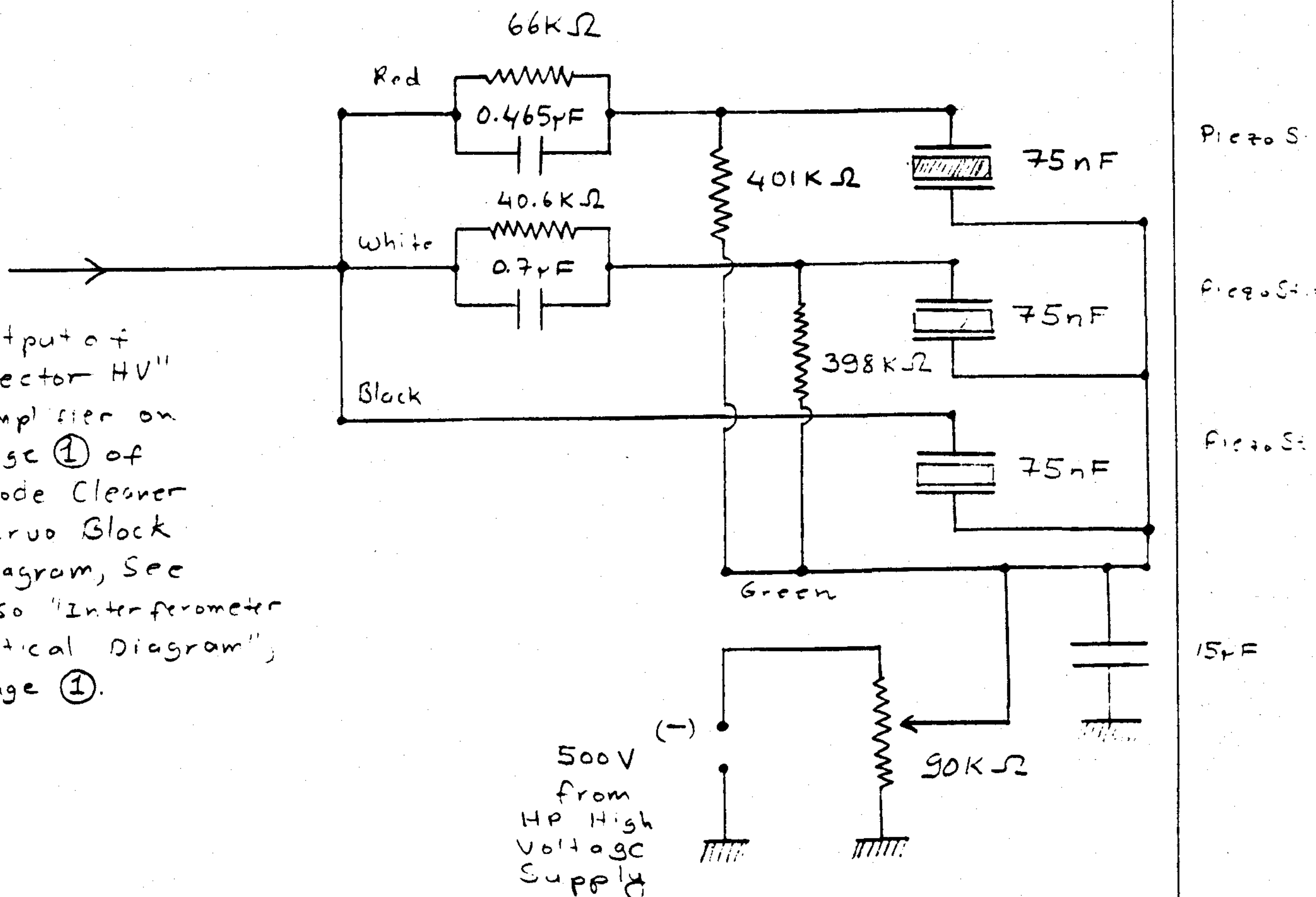


DPDT RELAY FOR AUTOMATIC LASER RE-LOCK



3 Piezo Stack Balancing Network

(For the Laser "BARNEY")



Output of "Vector HV" Amplifier on page ① of Mode Cleaner Servo Block Diagram, See also "Interferometer Optical Diagram", page ①.

"Also on page ① of "Mode cleaner servo Block Diagram".

Page ① of ①
July 25, '89 YG

C. LASER LOOP: SENSORS AND ACTUATORS

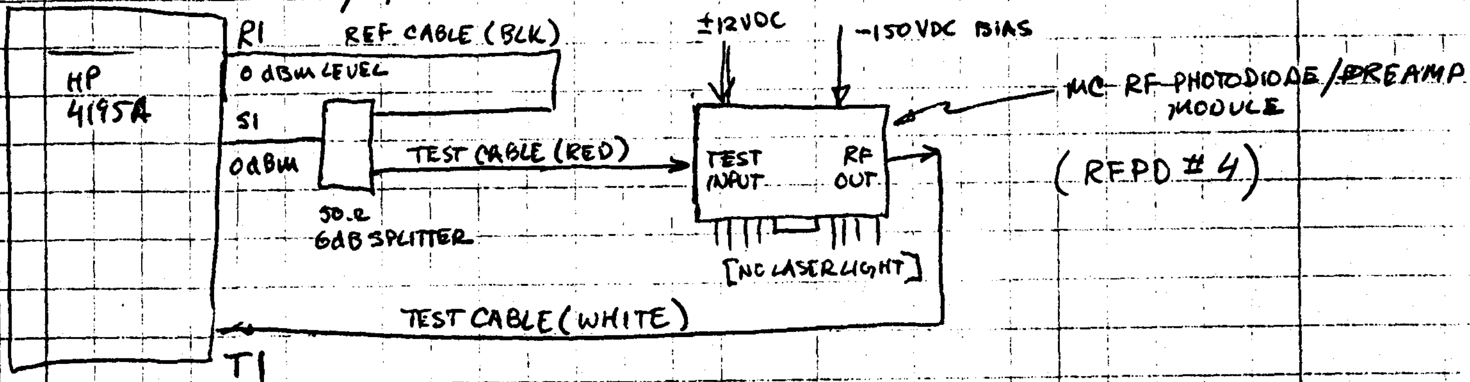
SENSITIVITY OF RF DETECTION SYSTEM + "OPTICAL GAIN"

8/4/89 M.E. Zucker 18:20

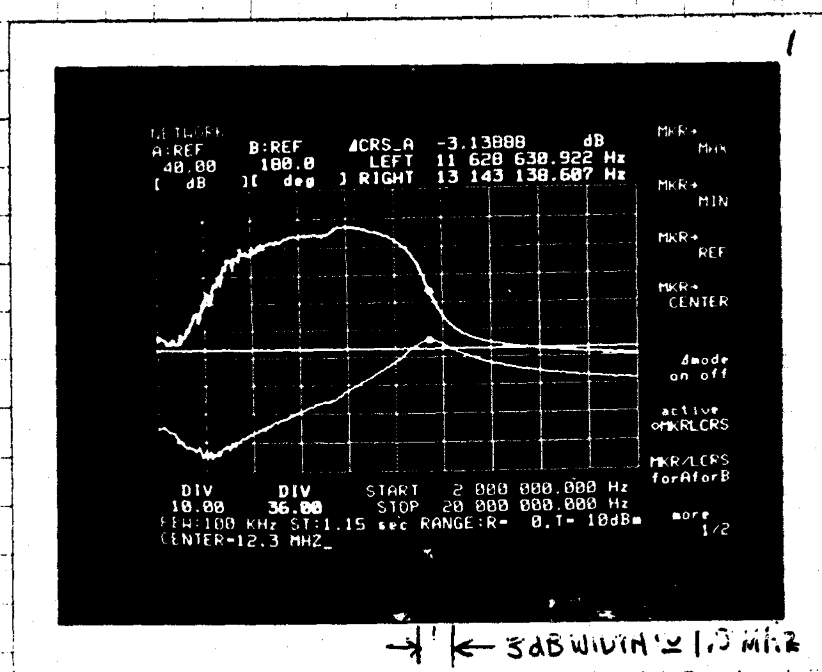
Recording measurements of optical and electronic transfer functions of various key elements of the etalon-pockels cell laser stabilization loop. (A.K.A. "Mode Cleaner Servo")

① Measured response of mode cleaner RF photodiode / preamp module at RF frequency using HP 4195A network analyzer

Setup:



8/9/89 10:15



UPPER TRACE; ARG(T_1/R_1), DEG

LOWER TRACE: $|T_1/R_1|$, dB

← 3dB WIDTH ≅ 1.5 MHz

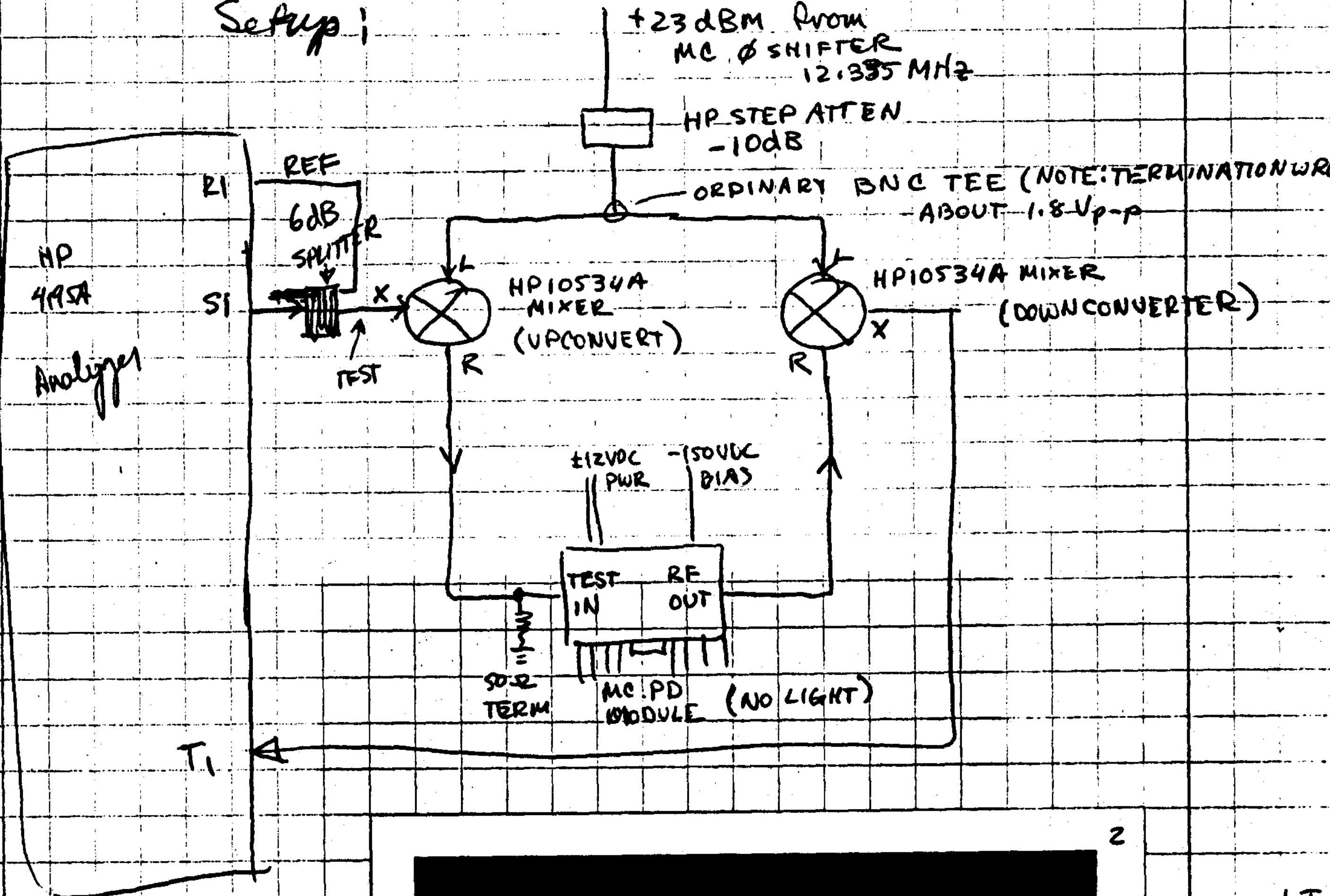
LINEAR FREQUENCY SCALE, 2 MHz → 20 MHz

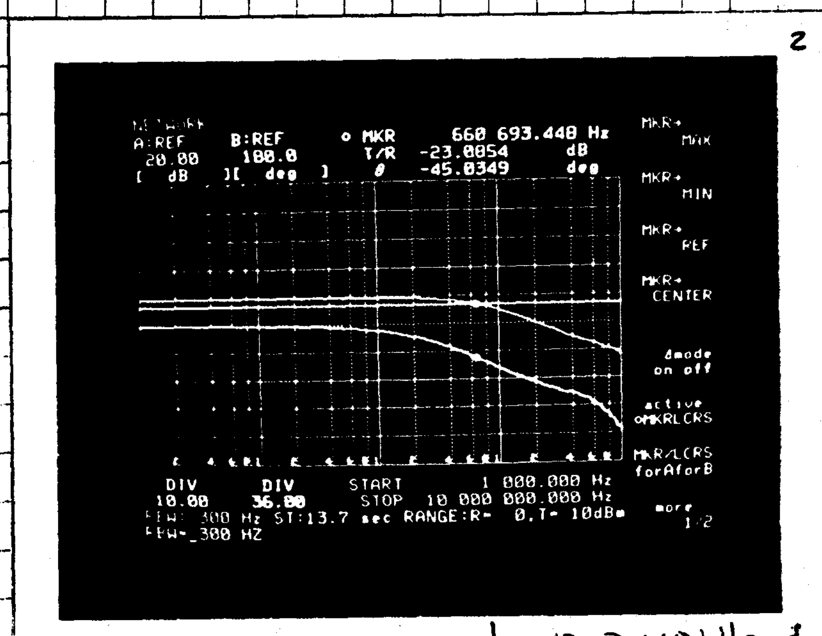
NOTE THAT PHASE IS + 40° AT CENTER FREQUENC

8/4/89 Cont'd. MEZ

② Measured "equivalent baseband response" of RF photodiode unit by upconverting the network analyzer's sweep to 12.33 MHz (amplitude modulation, suppressed carrier, just like an optical phase error produces).

Setup:





TOP: $\left|\frac{T_1}{R_1}\right|$

BELOW: ARG(

-3dB @ 660 kHz

EFFECTIVE POLE DUE TO PHOTODIODE BANDPASS

C2

8/8/89 Analysis of "Optical transfer function" measurements;

(MEZ) Transfer function on page 004Y must be corrected for
- (a) mis-termination of mixer
- (b) delay in long cable used to excite PC
- (c) the bandpass transfer function of the photodiode.
- (d) the propagation delay in the light path and in the RF cable from the photodiode to the mixer.

The results of this analysis (which is attached to subsequent pages for future reference) are summarized as follows;

With; photodiode now in use on MC (700 kHz "pole" due to bandpass)
950 mV out of lock, 400 mVDC in lock (contrast = 58%)
modulation index $\simeq 0.4$ $\left(\frac{P_{SIDEBAND}}{P_{CARRIER}} \simeq 0.04\right)$

we get;

$$\frac{\delta V(\text{mixer output, } 50\Omega \text{ term})}{\delta V(\text{ONE GSÄNGER PM-25 POCKELS CELL})} \simeq 5\times10^{-3}\frac{V}{V} \times \left(\frac{1}{1+\frac{jf}{700\,\text{kHz}}}\right)$$

Also, from the pockels cell terminals to the mixer output there is a frequency-dependent phase shift which is consistent with a propagation delay of (40 ± 10) nsec; the optical path between pockels cell → cavity → photodiode is about 6.5 m (⇒ 22 nsec), and the cable linking the PD w/ the mixer is 2.3 m (⇒ 11 nsec at 0.7c) for a calculated delay of 33 nsec. There are probably also delays associated with the diode proper, the internal buffer, or the pockels cell itself, but these should not contribute more than 5 nsec total in my estimation.

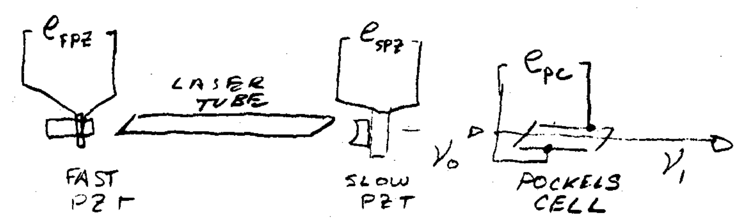
LASER PHASE & FREQUENCY ADJUSTMENT ACTUATORS

MEZ 10/17/90

ν = laser frequency $\simeq 5.8 \times 10^{14}$ Hz or so

ϕ = laser phase

f = audio or video fluctuation frequency



1. Pockels cell;

$$\dot{\phi}_0 = 2\pi\nu_0, \quad \phi_1 = 2\pi\nu_0 t + \frac{2\pi n_{pc} l_{pc}}{\lambda}$$

where l_{pc} = length of Pockels cell, and
n_{pc} = refractive index of cell;

$n_{pc} = n_0 + \alpha e_{pc}$

where α = electrooptic coefficient of cell crystal (V^{-1})

so $\nu_1 = \dot{\phi}_1/2\pi = \nu_0 + \frac{\alpha l}{\lambda}\dot{e}_{pc}$

Example: Gränger PM-25 cell, at $\lambda = 514.5$ nm,

has $\alpha l = 0.26$ nm/V*, so for a sinusoidal e_{pc} at frequency f,

$e_{pc} = V_0 \cos(2\pi f t)$, we get an output frequency

$$\nu_1(t) = \nu_0 - \frac{2\pi \alpha l f}{\lambda} e_0 \sin(2\pi f t)$$

$$= \nu_0 - 3.2 \times 10^{-3} \left(\frac{e_0}{1V}\right)\left(\frac{f}{1Hz}\right) \sin(2\pi f t) \text{ Hz}$$

*corresponding to 1kV/order at this λ.

10/17/90 MEZ

2. Fast PZT mirror;

as long as the laser oscillates in a single longitudinal mode labeled k

$$\nu^k = k\frac{c}{2d}$$

where k is a (large) integer and d is the spacing of the laser cavity (assume $n_{laser} = 1$). The piezo expands or contracts in proportion to e_{FPZ}, so

$d = d_0 + \beta e_{FPZ}$ and

$$\nu^k = \frac{kc}{2(d_0+\beta e_{FPZ})} \simeq \frac{kc}{2d_0}\left(1 - \frac{\beta e_{FPZ}}{d_0}\right)$$

$$\equiv \nu_0^k\left(1 - \frac{\beta e_{FPZ}}{d_0}\right) \quad \text{for } \beta e_{FPZ} \ll d_0$$

Example; the laser Barney has $d_0 \simeq 2.3$ m and its fast PZT has

$$\beta \simeq \frac{1 \text{ order}}{550\text{V}} \simeq 4.7 \times 10^{-10} \frac{\text{m}}{\text{V}} \quad \text{so}$$

$$\frac{\nu^k - \nu_0^k}{e_{FPZ}} \simeq \frac{\beta \nu_0^k}{d_0} = 120 \frac{\text{kHz}}{\text{V}}$$

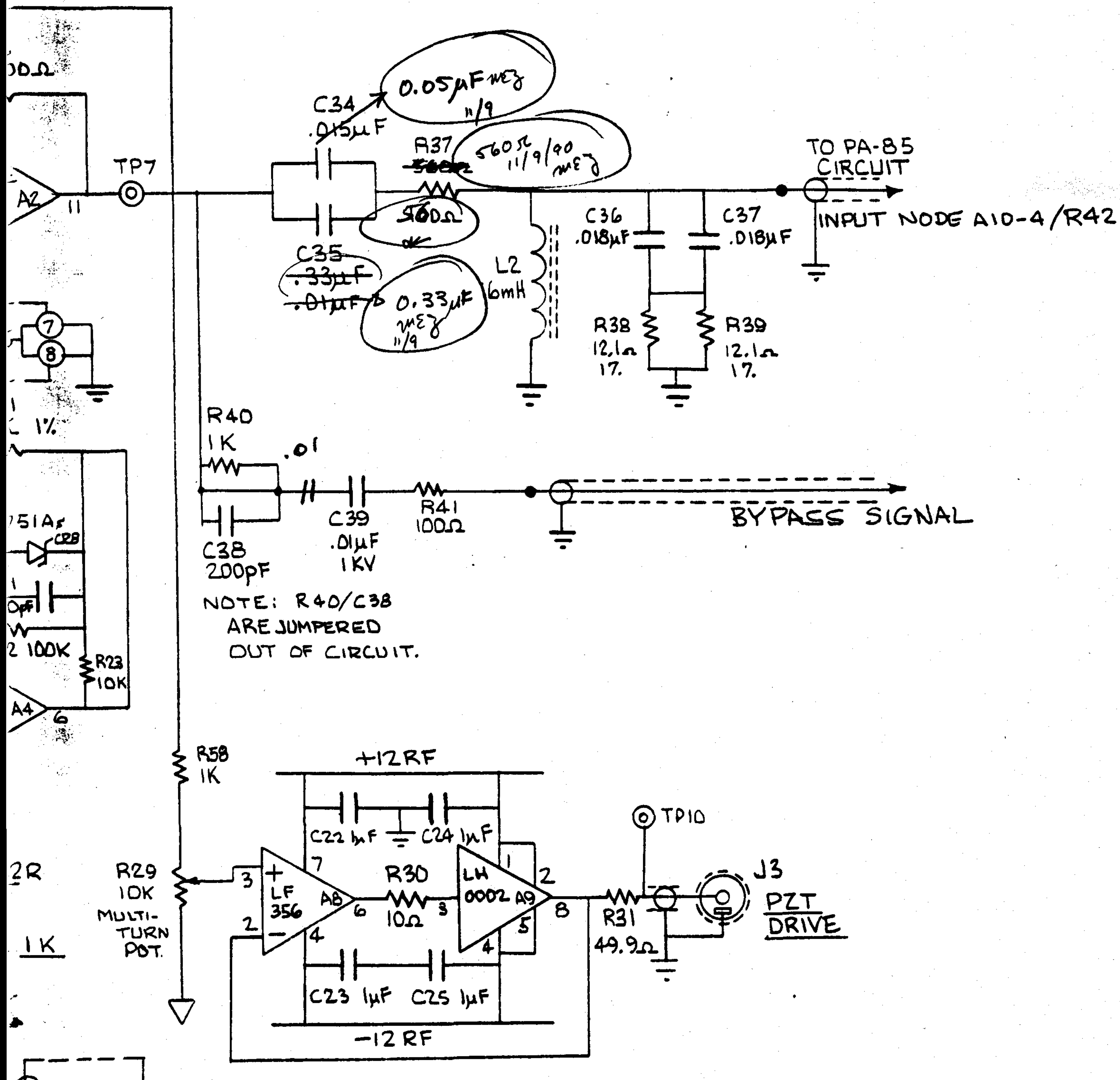
3. Slow PZT mirror; same as fast PZT, different β.

Example; for Barney, $d_0 \simeq 2.3$ m,

$$\beta \simeq \frac{1 \text{ order}}{70\text{V}} \Rightarrow$$

$$\frac{\nu^k - \nu_0^k}{e_{SPZ}} \simeq 930 \text{ kHz/V}$$

D. LASER LOOP: PROTOTYPE #1



LASER LOOP AMPLIFIER VER. 1 PROTOTYPE I VER. 1

ADDED = COMPONENENTS

REBUILD 11-8-90
B.T.
J.C.

Diagram Revised 11/9/90 MEZ

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GRAVITATIONAL PHYSICS

LASER LOOP AMPLIFIER - SECTION 1

DRAWN BY B.T.	DATE 10-9-89	DRAWING NO
CHECKED BY	SCALE	
APPROVED BY	W.O.	

D1