

New Folder Name Dent Calculation

LIGO - T940054-00-B



FACSIMILE MESSAGE

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Plainfield, Illinois 60544-8929

Fax No. is: 815 439 6010
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August 26, 1994

To: Larry Jones
LIGO Project Caltech Pasadena, California

Fax No. (818)304-9834

From: M. L. Tellalian Phone (815)439-6517

Plainfield Engineering - PAE

RE: Dent Calculation Example & GPS Convention
LIGO Design & Qualification Test - Caltech Contract C:146

Larry,

Attached is the letter regarding dents in a sugar silo center column that I talked about on Wednesday. The center column is a stiffener cylindrical shell subjected to external pressure and column load. In this case I believe that the reduction in allowable column load was governed by the axial load. Due to the relatively small axial load, the beam tubes may be governed by the external pressure. I've asked Mark Such to look into this problem and have asked for a response by September 12.

Also attached are a couple of pages out of a brochure for a GPS convention which will be held in Salt Lake City from September 20 - 23. The convention is sponsored by the Satellite Division of the Institute of Navigation and is entitled "ION GPS-94, GPS Goes Operational: Applications and Technology". Steve Hand and possibly Steve Peters will attend tutorials 501A, B, C, & D which deal with High Accuracy GPS Positioning Techniques & Survey Applications. It may be beneficial for someone from Caltech to attend as well. You can receive additional information from the Institute of Navigation, 1800 Diagonal Road, Suite 480, Alexandria, VA 22314. Their phone number and fax number are (703) 683-7101 and (703) 683-7177, respectively.

Regards,

M. L. Tellalian - Plainfield Engineering

cc: CDM/Chron

June 18, 1993



Ref: Center Column for Weibull Sugar Silo
Eay City, Michigan
Contract #933441

Five dents were accidentally made in ring number 14 of the center column near the lower edge as shown on Sheets 1 and 2. An angle stiffener 6x4x5/8 was installed 6 in. above the seam with the 4 in. leg horizontal. An analysis has been made to determine the effects of the dents on the axial compression buckling load based upon two papers (1,2) of mine and using the ECCS rules (3).

Miller Method

The local elastic buckling stress, F_{ze} , of an axially compressed cylinder is given by the following equation.

$$F_{ze} = \alpha 0.605 Et / r \quad (1)$$

The inelastic buckling stress, F_{ze} , is given by the smaller of Eq. 1 and Eq. 2.

$$F_{ze} = \frac{233 F_y}{166 + R / t} \quad (2)$$

The following equation is given in Ref. 1 for $0.605\alpha=C$.

$$C = 0.605\alpha = -0.025 - 0.286 \log(UR / t) \quad (3)$$

The following equation is given in Ref. 2 for the relationship between the amplitude of imperfection, w_o , and the unevenness factor U.

$$UR / t = \frac{w_o}{4t} \quad (4)$$

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For the center column, $R=71$ in., $t=0.3125$, $w_o=0.4375$, and $UR/t=0.35$. From Eq. 2, $C=0.1054$ and from Eqs. 1 and 2, $F_{cr}=13.46$ ksi.

The following equation has been derived in a recent research contract for column buckling.

$$F_{cr} = [1 - 0.74(\lambda - 0.15)]^{0.5} F_y \quad 0.15 < \lambda < 1.41 \quad (5)$$

$$\text{where } \lambda = \frac{KL}{\pi r} \sqrt{\frac{F_{cr}}{E}}$$

For the center column, $\lambda=0.233$ and $F_{cr}=13.21$ ksi. With $FS=1.67$ the allowable load is 920 kips.

ECCS Method

$$F_{cr} = \alpha \cdot 0.605 \cdot E_r / R \quad (1)$$

$$F_{cr} = \frac{F_y}{\gamma} \quad \gamma = 4/3 \quad F_{cr} \leq 0.5F_y \quad (6)$$

$$F_{cr} = \left[1 - 0.4123 \left(\frac{F_y}{F_{cr}} \right)^{0.6} \right] F_y \quad F_{cr} > 0.5F_y \quad (7)$$

$$\alpha_o = \frac{0.70}{(0.1 + 0.01R/t)^{0.5}} \quad \text{For } w_o = 0.4\sqrt{Rt} \quad (8)$$

$$\alpha = 0.5\alpha_o \quad \text{For } w_o = 0.08\sqrt{Rt}$$

$$\alpha = 0.338\alpha_o \quad \text{For } w_o = 0.4375 = 0.093\sqrt{Rt} \quad (\text{By extrapolation}).$$

For center column $F_{cr}=8.91$ ksi. From Eq. 5, $\lambda=0.190$ and $F_{cr}=8.83$. With $FS=1.5$ the allowable load is 820 kips.

From the above analysis the allowable load on the center column is 920 kips by the Miller method and 820 kips by the ECCS method. The difference is the two loads is due to an additional partial safety factor of $\lambda=4/3$ in Eq. 6.

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June 18, 1993

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References

1. Miller, "Buckling Stresses for Axially Compressed Cylinders", CBT-5349, 1976.
2. Miller, "Effect of Imperfections on Buckling of Axially Compressed Cylindrical Shells", Research paper, September 28, 1989.
3. ECCS, "Buckling of Steel Shells", 4th Edition, 1988.

CDM

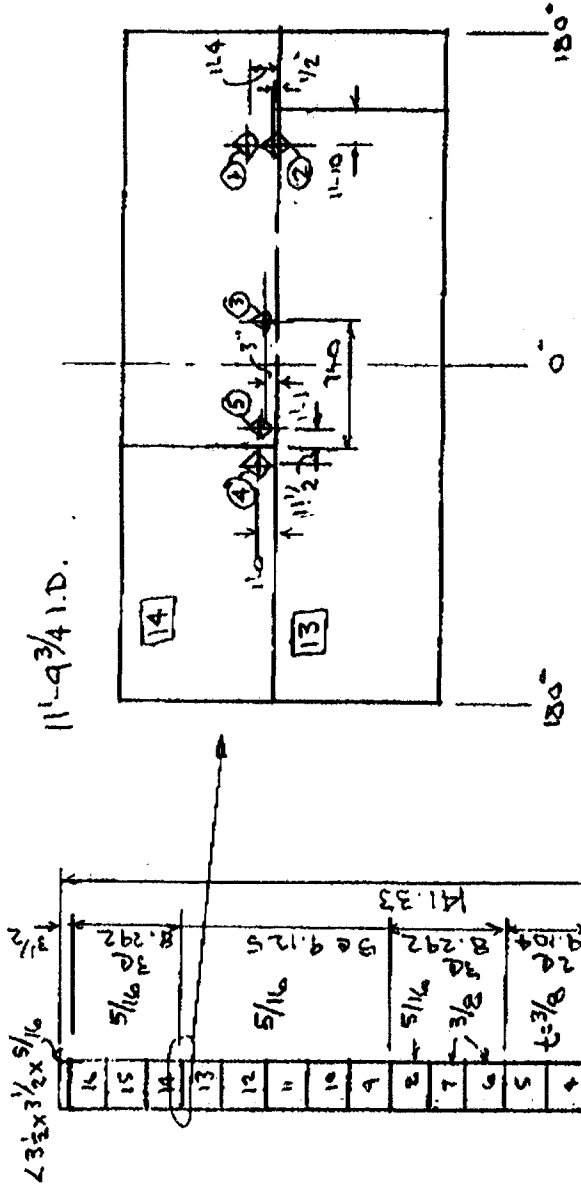
C.D. Miller
Plainfield Development, RDE

krf

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WEIBOLL SUGAR SILO
 BAY CITY MICH.
 CONT. 933441



DENT LOCATIONS

$R = 71.0 \quad t = 0.3125 \quad R/t = 227$
 $L/r = 141.33 \times 12 / 0.7 \times 71 = 34 \quad \lambda = \frac{KL}{\pi r} \sqrt{\frac{F_{yc}}{E}}$

ECCS RULES

$\bar{w} = .4375 \quad \lambda_r = 4\sqrt{RE} = 18.84 \quad \bar{w}/\lambda_r = 0.0232$

$\alpha = \frac{0.70}{(0.1 + 0.01R/t)^{1/2}} = 0.455 \quad \text{FOR } \bar{w}/\lambda_r = 0.01$

$\alpha' = .5 \times .455 = 0.227 \quad \text{FOR } \bar{w}/\lambda_r = 0.02$

$\alpha'' = 0.154 \quad \frac{\alpha'}{\alpha} = 0.338 \quad \text{FOR } \bar{w}/\lambda_r = 0.0232$

$F_{yc} = \frac{3}{4} \times 0.154 \times 0.605 \times 29000 / 227 = 8.91$

$F_a = \frac{F_{cn}}{1.5} = \frac{8.83}{1.5} = 5.89 \quad \lambda = 0.190 \quad F_{cn} = [1 - 0.75(\lambda - 0.15)^2]^{0.5} F_{yc} = 8.23$

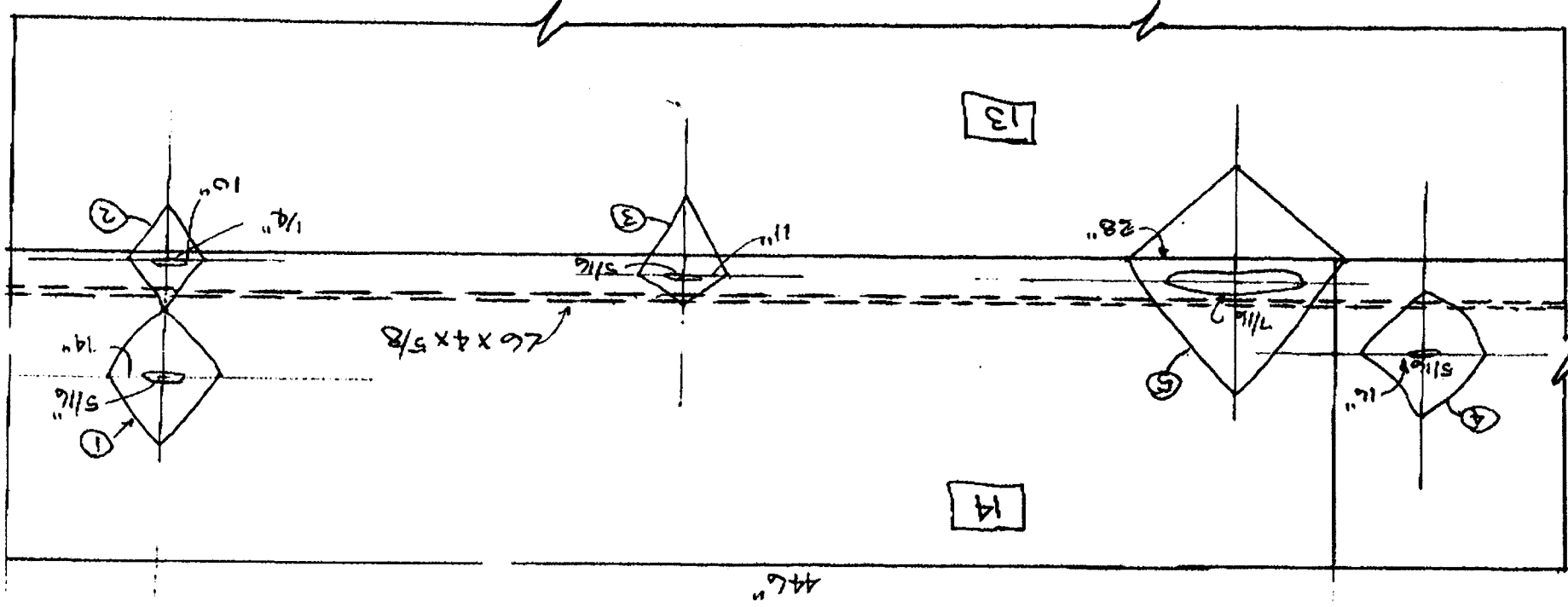
$P_a = 2\pi \times 71 \times .3125 \times 5.89 = 820 \text{ kips}$

SMT. 1
 CDM
 RDE
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QNT.2
CDM
RDE
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DENT LOCATIONS AND SIZES.

LENGTH OF RUCKLES = 69"
 $\frac{496-69}{446} = 0.845$



REFS: MILLER: (1) EFFECT OF IMPERFECTIONS ON BUCKLING OF AXIALLY COMPRESSED CYLINDRICAL SHELLS. (2) CRT 5349

$$\text{MAX. DENT} = 0.4375 = W_0 \quad W_0/t = 1.40$$

$$U = \frac{W_0/t}{FR/t} = 0.00154 \quad U \frac{R}{t} = \frac{W_0/t}{4} = 0.35$$

$$C = -0.025 - 0.286 \log (UR/t) \\ = 0.1054$$

$$F_{xe} = C E t / R = .1054 \times 29000 / 227 = 13.46 \quad \lambda = 0.233$$

$$F_{en} = .98 \times 13.46 = 13.21 \quad F_a = \frac{13.21}{2} = 6.60$$

$$P_a = 139.4 \times 6.60 \text{ KSI} = 920 \text{ KIPI}$$

SPR U?

CYLINDER - NORMAL FABRICATION

$$\frac{W_0}{t} = 4 \times 0.9005 \times 227 = 0.454 \text{ IN.}$$

$$C = 0.919 - 0.286 \log 227 = 0.245$$

$$F_{xe} = 31.3 \text{ KSI}$$

$$F_{xc} = [0.45 + 0.18 \frac{W_0}{3C}]^{1.3} = 21.8 \text{ KSI}$$

$$C = K C_x = \frac{169}{195 + 227} \cdot 0.605 = 0.242 \quad F_{xe} = 30.9$$

$$F_{xc} = \frac{233 F_y}{166 + R/t} = \frac{233 \times 36}{166 + 227} = 21.3 \text{ KSI}$$

$$\frac{F_{xe} (\text{DENTED})}{F_{xc} (\text{NORMAL})} = \frac{13.46}{21.3} = 0.632$$

$$\text{ESCS} \quad \alpha C_{cr} = .455 F_x \cdot 605 E t / R = 35.2$$

$$F_{xc} = [1 - 0.4123 (\frac{36}{6572})^{0.6}]^{1.6} \cdot 36 = 21.0$$

$$\frac{F_{xc} (\text{DENTED})}{F_{xc} (\text{NORMAL})} = \frac{11.90}{21.0} = 0.567$$

SHT. 3

CDM

ROE

6-17-93

Tutorials for Tuesday - Rooms 4, 5, and 6

Tuesday Morning Tutorials Advertisement Tuesday Afternoon Tutorials

501 C: High Accuracy GPS Positioning III
8:30 - 12:00 Tuesday, Room 5

This half day addresses methods for achieving high accuracy positioning measurements for moving platforms using the latest differential GPS techniques.

Dr. Gerard Lachapelle
University of Calgary

Differential Code and Carrier Phase Measurement Concepts

- Code correlation vs. carrier phase measurement techniques
- Measurement errors
- Impact of narrow correlator spacing code technology
- Differencing techniques
- Achievable accuracies; effect of dynamics
- Ambiguity Resolution Methods
- Static vs. kinematic; carrier cycle ambiguity
- Relationship between various methods
- Testing criteria; multipath & other errors
- Single vs. dual frequency resolution; processing
- Attitude determination case

Real Time Issues and Emerging Trends

- Data links; requirements
- Attitude reference systems
- Airborne photogrammetry
- Marine

Level: Basic knowledge of the GPS system is assumed as well as familiarity with engineering analysis methods.

501 D: High Accuracy GPS Positioning IV
1:30 - 5:00 Tuesday, Room 5

This final half day addresses precise positioning techniques particularly as they relate to surveying - both in the static and kinematic modes.

Dr. M. Elizabeth Cannon
University of Calgary

GPS Static Positioning

- Conventional static surveying procedures
- Rapid static methods; stop and go
- Impact of receiver technologies; accuracy
- On the fly (OTF) ambiguity resolution methods
- Single versus dual frequency observations
- Effect of carrier phase noise and multipath
- Integer vs. float ambiguity solutions
- Stop and go positioning
- Low cost receiver vs. geodetic receiver results; trades
- Survey validation concept

Level: Basic knowledge of the GPS system is assumed as well as familiarity with engineering analysis methods.

Case Study II: Land and Marine Positioning
Dr. Gerard Lachapelle
University of Calgary

- Effect of ambiguity resolution algorithms
- Use of multi-receiver configurations
- Ionospheric code-carrier divergence
- Multipath effects and ground planes
- P-code vs. codeless processing

Case Study II: Airborne Positioning
Dr. Herbert Landau
terrasat GmbH

- Applications and associated accuracy requirements
- Error components; long, topo, multipath
- Use of carrier phase; OTF ambiguity resolution; performance
- Receiver/MU/computer mechanization
- Experimental and production flight results

Attitude Determination with GPS
Dr. Clark Cohen
Stanford University

- Principles; error sources
- GPS errors; multipath, refraction effects
- Structural flexing, geometry
- Performance envelope
- Static and dynamic flight test results
- Level: 631B is an advanced course which assumes attendees have a good understanding of GPS signal processing.

501 C: High Accuracy GPS Positioning III
8:30 - 12:00 Tuesday, Room 5

This half day addresses methods for achieving high accuracy positioning measurements for moving platforms using the latest differential GPS techniques.

Dr. Gerard Lachapelle
University of Calgary

Differential GPS (DGPS) Techniques

- Use of post-mission orbit and timing information
- Effect of selective availability (SA)
- GPS Point Positioning

RTCM SC-104 differential corrections

- Basic code-based DGPS corrections
- Carrier phase differential corrections
- Monitor Stations
- Communications links; latency

Applications and Case Studies

- Geographic Information Systems (GIS)
- Vehicle positioning
- Attitude reference systems
- Airborne photogrammetry

Level: Basic knowledge of the GPS system is assumed as well as familiarity with engineering analysis methods.

Case Study II: Land and Marine Positioning
Dr. Gerard Lachapelle
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- Effect of ambiguity resolution algorithms
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401 C: Integration of GPS with Inertial Navigation Systems III
8:30 - 12:00 Tuesday, Room 4

In 401 C & D, current activities in GPS/INS integration will be discussed, including new approaches to decentralized filter design. Applications of low cost integration will be considered, as will the benefits of integration for GPS integrity enhancement. The inertially aided GPS concepts and techniques will be analyzed.

Mr. G. Jeffrey Geier
Motorola

Design of Centralized Filters for GPS/INS Integration

- Dynamic modeling; F, Q matrices
- New approaches to centralized filter design
- Integration of Existing Receiver Designs
- The cascaded filter design problem
- Existing and new cascaded filter designs
- Analysis of performance
- Receiver Aiding
- Carrier, code loops
- Simplified error analysis
- Partitioned design; integrated design
- Simulation results; agreement with practice

Level: Familiarity with INS and GPS technology is assumed in 401C, as well as knowledge of matrix theory.

Case studies, current activities in the field, and new areas of research are emphasized in this half day.

Mr. Geier

GPS/INS Case Studies I

- GPS/AHRS/Doppler for helicopter applications
- Equipment configuration with filter design options
- Simulation results

GPS/INS Integration Case Studies II

- Ancient integration: low cost, moderate performance
- Low cost guided weapon integration
- Current Activities and Research
- Very low cost GPS/INS integrated systems
- Jamming resistant GPS receiver
- GPS/INS integrity Monitoring; benefits of integration
- Inertially aided GPS and performance enhancement
- GPS/INS national meetings, publications and references

Level: Familiarity with INS and GPS technology is assumed, as well as knowledge of integration techniques (401 A-C desirable).

Monday Morning Tutorials

Advertisement

Monday Afternoon Tutorials

501 A: High Accuracy GPS Positioning
 8:30 - 12:00 Monday, Room 5

High accuracy positioning users have found great benefit in employing GPS to achieve a variety of accuracies (down to the centimeter level) in far less time than by conventional methods. The first half day addresses the basic principles involved.

Dr. Gerard Lachapelle
 The University of Calgary

501 B: High Accuracy GPS Positioning II
 1:30 - 5:00 Monday, Room 5

This half day focuses on how GPS measurements can be used with coordinate systems and reference networks to obtain consistent, high accuracy results.

Dr. Lachapelle

501 A: High Accuracy GPS Positioning
 8:30 - 12:00 Monday, Room 5

This course addresses the use of hazard tree analysis and risk allocation methods for the determination of RNP for each phase of flight. Navigation sensors evaluated on GNSS, LORAN, DME, IRS & INS. Introduces new concept of aircraft navigation performance (ANP) relationship.

Dr. Robert Kelly
 Consultant

501 B: High Accuracy GPS Positioning II
 1:30 - 5:00 Monday, Room 5

This half day focuses on how GPS measurements can be used with coordinate systems and reference networks to obtain consistent, high accuracy results.

Dr. Lachapelle

401 A: Integration of GPS with Inertial Navigation Systems I
 8:30 - 12:00 Monday, Room 4

GPS and INS complement each other to achieve continuous high accuracy and reliability. GPS provides precise position and velocity fixes at discrete points in time; the INS provides precise interpolation between fixes. 400A and 400B lay the groundwork for understanding current integration methods, and lead to tutorials 400C and D.

Dr. R. Grover Brown
 Consultant

401 B: Integration of GPS with Inertial Navigation Systems II
 1:30 - 5:00 Monday, Room 4

The session in this half day tie together the Kalman filtering concepts covered in the morning with their basic uses in GPS/INS integrations.

Mr. G. Jeffrey Geler
 Motorola

401 A: Integration of GPS with Inertial Navigation Systems I
 8:30 - 12:00 Monday, Room 4

GPS and INS complement each other to achieve continuous high accuracy and reliability. GPS provides precise position and velocity fixes at discrete points in time; the INS provides precise interpolation between fixes. 400A and 400B lay the groundwork for understanding current integration methods, and lead to tutorials 400C and D.

Dr. R. Grover Brown
 Consultant

401 A: Integration of GPS with Inertial Navigation Systems I
 8:30 - 12:00 Monday, Room 4

GPS and INS complement each other to achieve continuous high accuracy and reliability. GPS provides precise position and velocity fixes at discrete points in time; the INS provides precise interpolation between fixes. 400A and 400B lay the groundwork for understanding current integration methods, and lead to tutorials 400C and D.

Dr. R. Grover Brown
 Consultant

401 B: Integration of GPS with Inertial Navigation Systems II
 1:30 - 5:00 Monday, Room 4

The session in this half day tie together the Kalman filtering concepts covered in the morning with their basic uses in GPS/INS integrations.

Mr. G. Jeffrey Geler
 Motorola

401 A: Integration of GPS with Inertial Navigation Systems I
 8:30 - 12:00 Monday, Room 4

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