

BASELINE SUSPENSION DESIGN FOR LIGO II - UPDATE

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for the GEO suspension team

LSC, Hanford 15th August 2000

LIGO-G000295-00-D

GEO suspension team for LIGO II

G Cagnoli, M Casey, D Crooks, A Grant,
J Hough, H Lueck, M Plissi, N Robertson,
S Rowan, P Sneddon, K Strain, C Torrie,
H Ward

+ summer students (M Keuntje, M Perreur-Lloyd)

Outline of Talk

- General developments (NAR)
- Updating and optimisation of thermal noise curves (internal plus pendulum) incorporating latest thermoelastic models (NAR)
- recent work on sapphire/silica bonding (SR)

Summary of Baseline LIGO II Design (BSC)

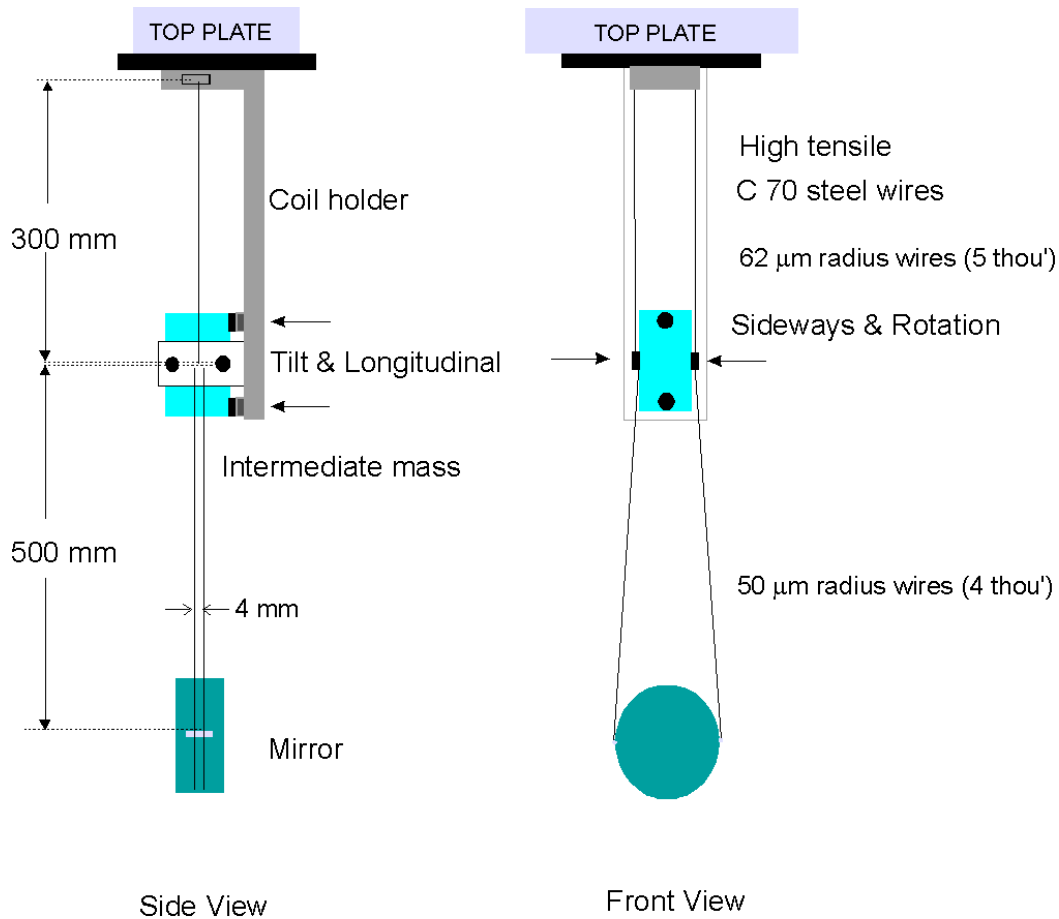
- Quadruple pendulum incorporating 3 stages of enhanced vertical isolation using blades
- fused silica ribbons suspending sapphire mirror
- local control sensors/actuators or eddy current damping on top mass
- overall length ~ 1.7 m
- all locally controlled freqs. in range 0.4 - 5.5 Hz
- global control above 0.01 Hz, split between 3 controllers on 3 lowest stages, acting against quad reaction pendulum

Progress on GEO 600

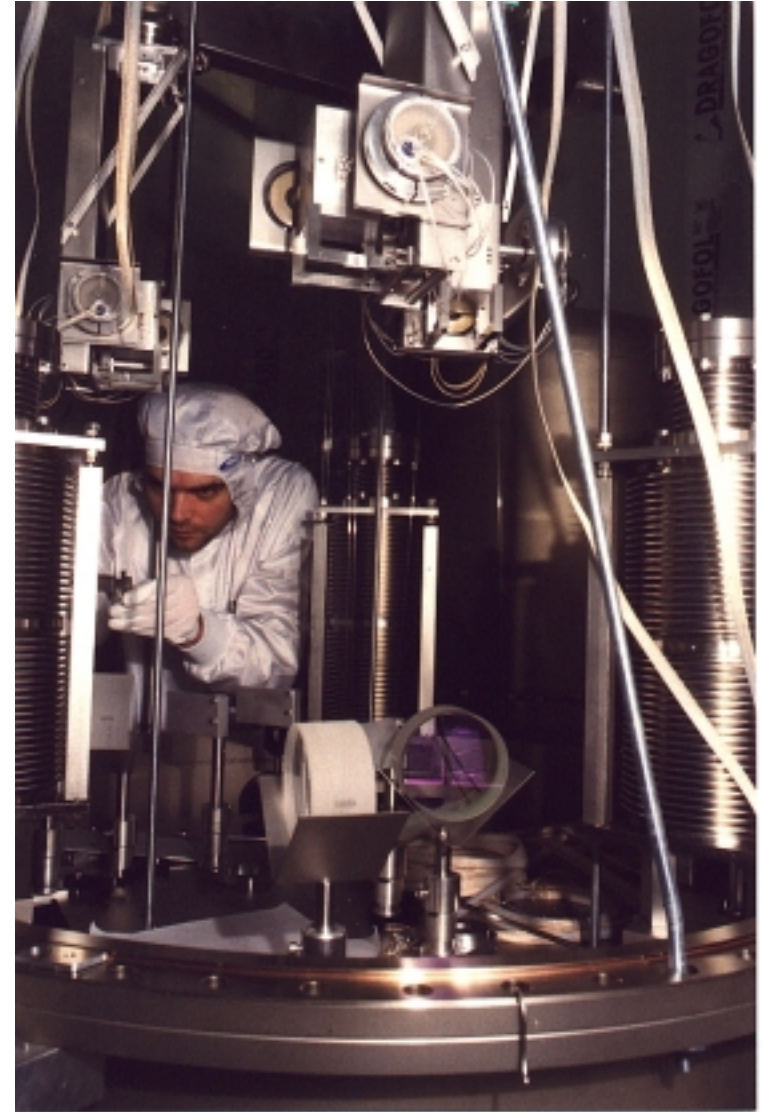
Suspensions

- modecleaner mirrors, power recycling mirror, near mirror and far mirror (east arm) installations (see pictures)
- pulling machine for GEO fibres currently being assembled - to Ruthe site in September
- first silica suspensions scheduled for Autumn (far north and far east mirrors)

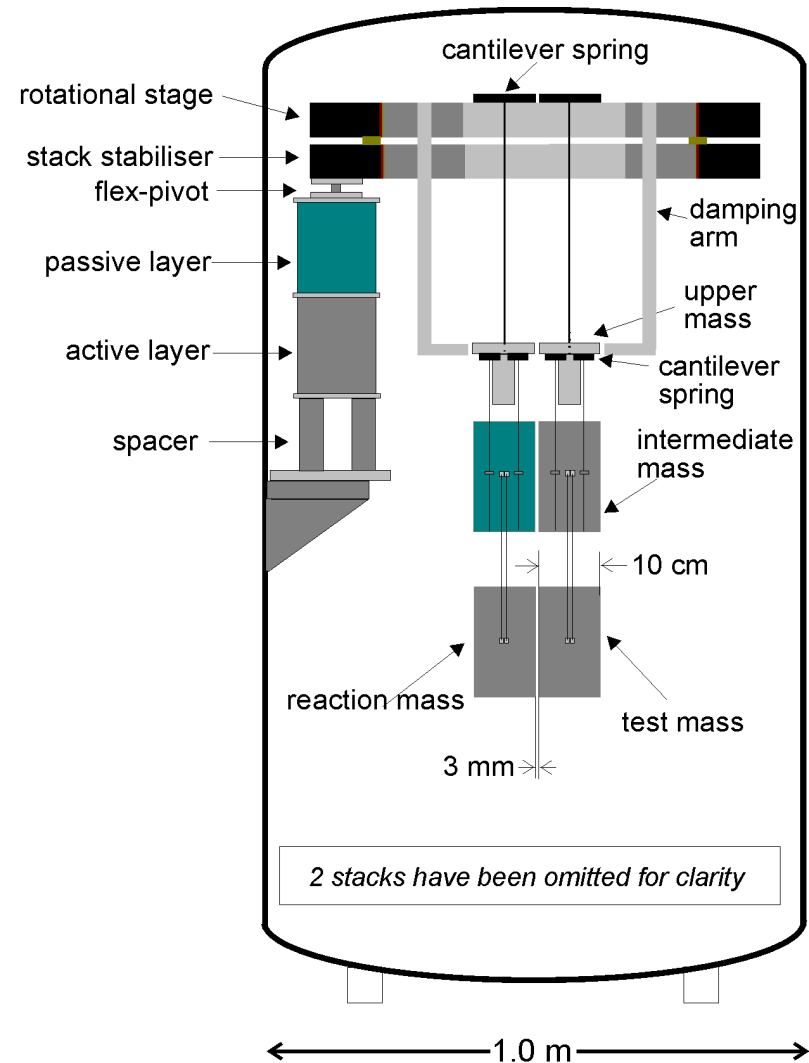
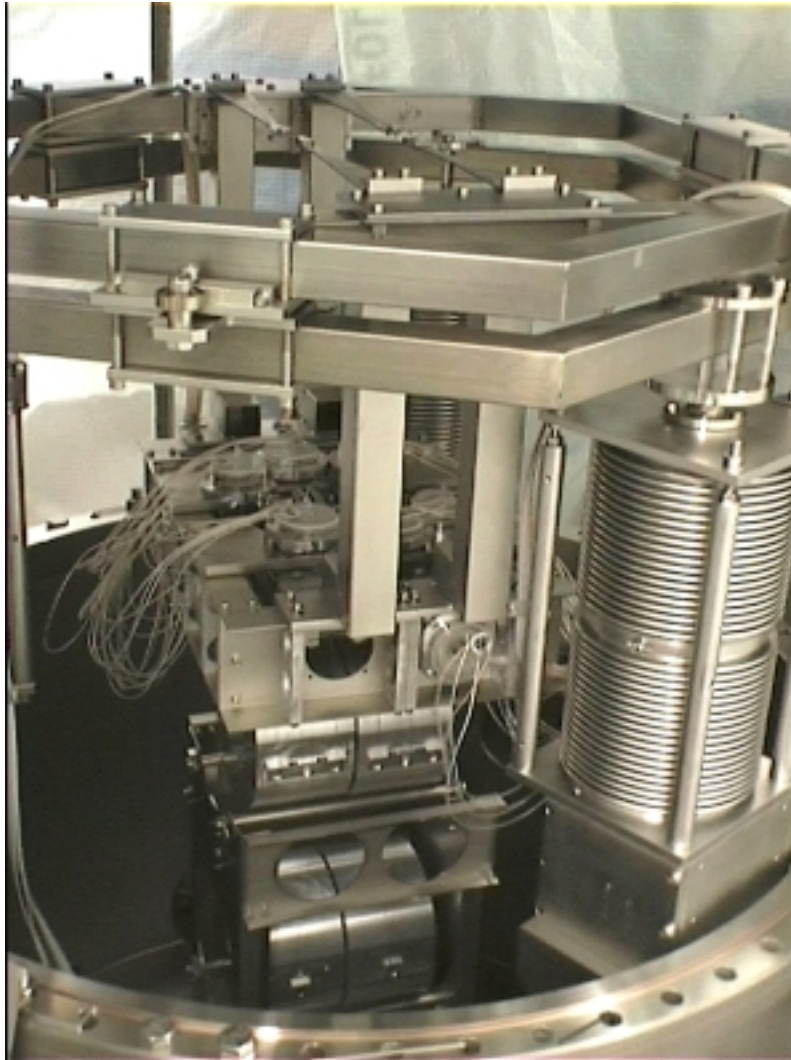
modecleaner suspension



Schematic of Modecleaner suspension



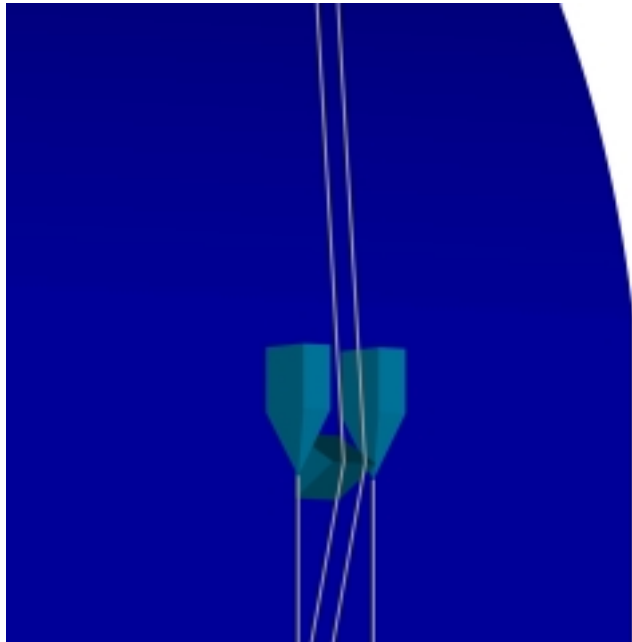
GEO triple pendulum suspension



Mechanical Developments on LIGO II design

- Autocad diagrams
- experimental work on cantilever blade attachments (2 wires from one blade)
- preliminary eddy current damping tests

Autocad - quadruple suspension (details)

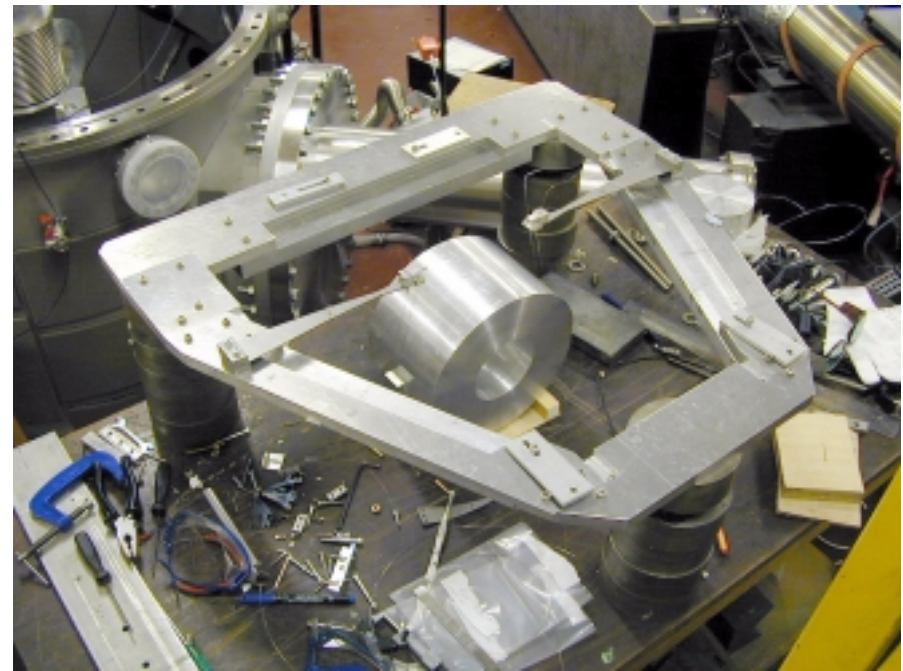


side of silica mass

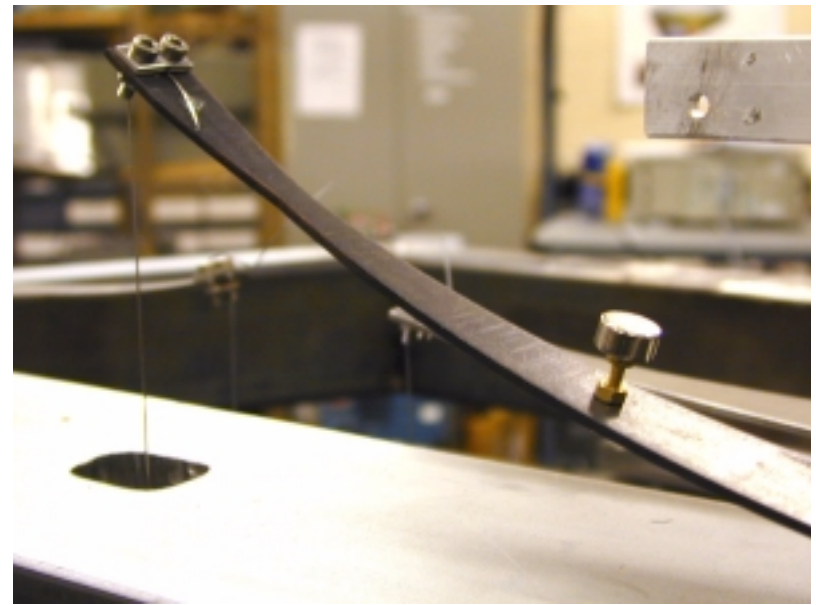
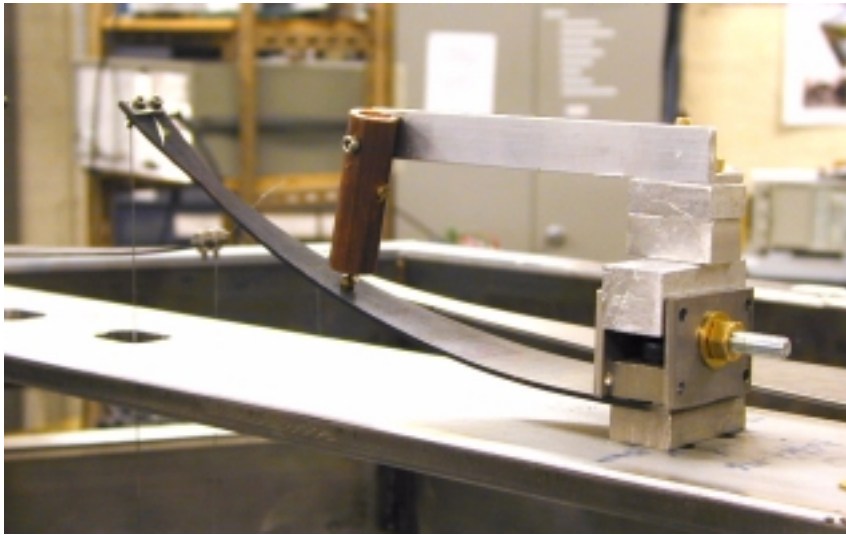


upper mass - exploded view

Cantilever Blade Investigations



Eddy Current Damping



damper for blade internal mode - NdFeB magnet in Cu tube
damping constant $\sim 0.6 \text{ kg s}^{-1}$

Future Work

- continuation of overall quadruple design + build wire/dummy mass prototype over the next year
- continuation of thermal noise developments
 - further modelling incl. cross-coupling
 - assembly of ribbon pulling machine
 - strength and loss tests on ribbons
 - bonding and welding - further strength and loss tests

Thermal Noise Calculations

- The codes used give a good approximation but are not yet completed

Suspensions

- 4 coupled harmonic oscillators
- Vertical and Horizontal degree of freedom
- Transfer Function calculations V, H
- Total transfer function $T^2 = H^2 + (\epsilon V)^2$
- Fluctuation - Dissipation Theorem

Internal

- Structural damping
- Thermoelastic damping (Braginsky)
- Add effects in quadrature

- They are upgraded from January reflecting new effects and new parameters

Upgrading the Internal Thermal Noise

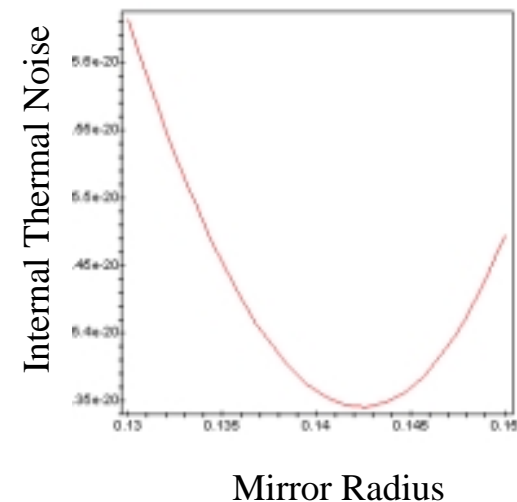
- K. Thorne correction for Finite Sized Test Mass
- Sapphire physical parameters (E. Gustafson)

4 parameters: mass, mirror radius,
thickness, beam radius

Mass fixed at 30 kg.- thus thickness defined by
mirror radius.
Ratio of beam to mirror radius set by keeping
loss < 1 ppm.

Find mirror radius which minimises
thermal noise

Internal Th-Ns has
a minimum at
mirror radius = 14.25 cm



Upgrading the Suspension Thermal Noise

- Violin modes modelled for the silica stage
- Total (standard + new) thermoelastic damping in the steel wires and silica suspension
- Standard thermoelastic damping in the blades
- More realistic dilution factors for the steel stages
- Surface losses in the silica suspension

(A.M. Gretarsson, G.M. Harry, *Rev. Sci. Instrum.*, 70 (10), 4081-4087)

New Thermoelastic Damping

- Thermoelastic damping is an effect of thermal expansion
- For a pre-stressed body, thermal expansion depends on coefficient of thermal expansion *and* coefficient of the Young's modulus with temperature
(Cagnoli and Willems)
- In this case the change in strain is proportional to the temperature change through an effective thermal expansion coefficient

$$\alpha_{eff} = \alpha - \beta \frac{\sigma_0}{E}$$

$$\beta = \frac{1}{E} \frac{dE}{dT}$$

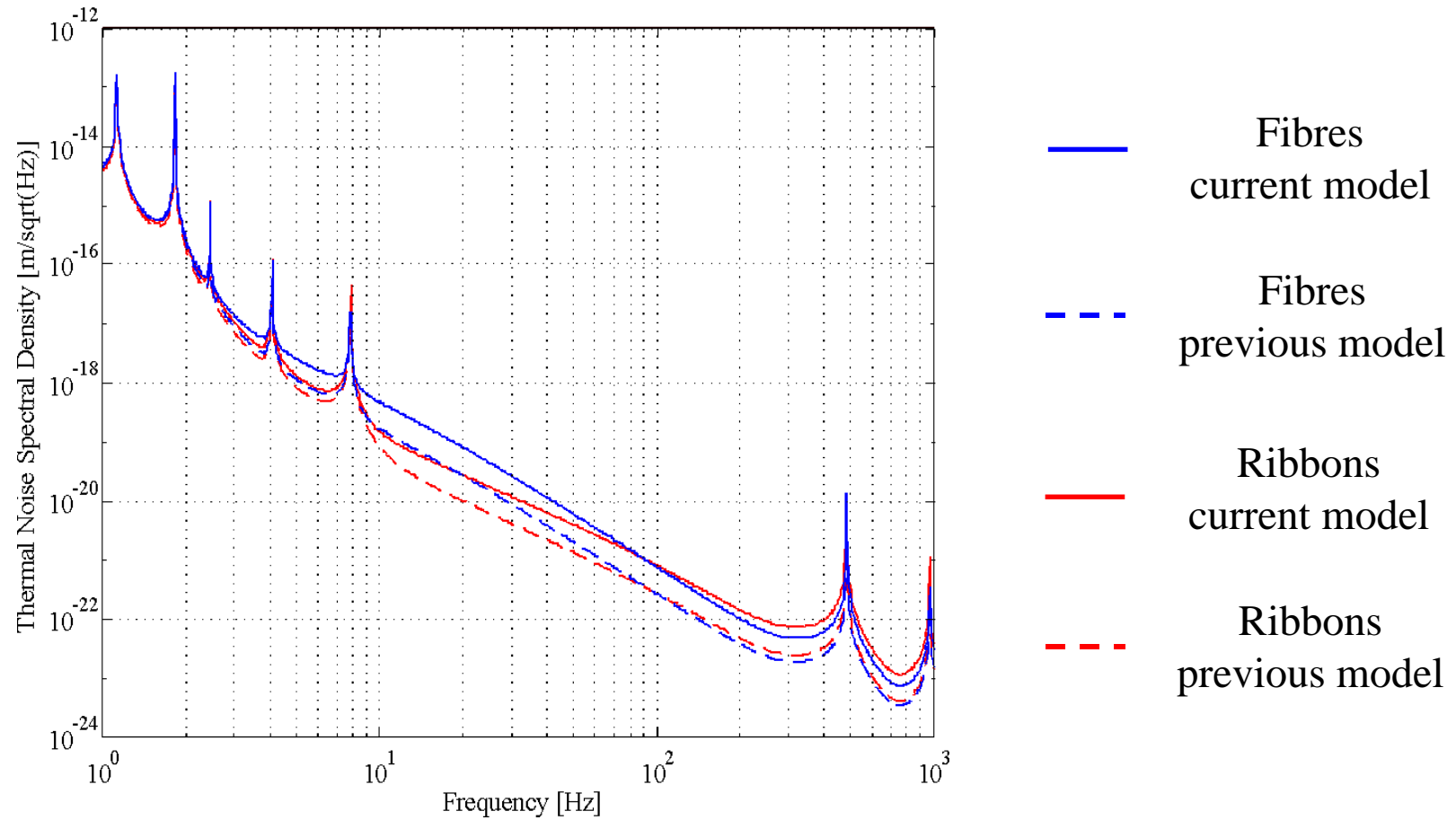
New Thermoelastic Damping

Material loss angle

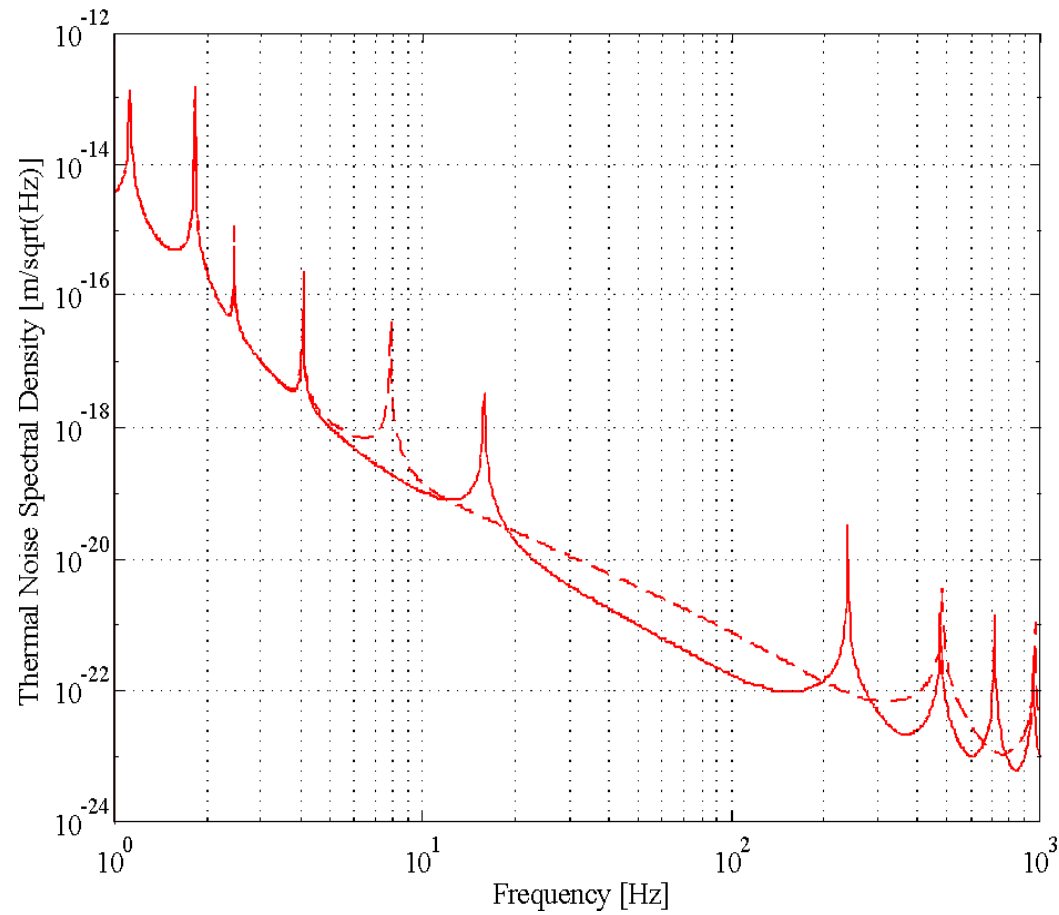
$$\varphi_{mat} = \varphi_0 + \Delta \frac{\omega \tau}{1 + (\omega \tau)^2} \quad \text{with } \Delta = \alpha_{eff}^2 \frac{E T}{\rho C_V}$$

- For a particular static stress the effective thermal expansion is null-hence the thermoelastic damping, normally dominant at low frequency, goes to zero.
- The null condition can in principal be achieved in the LIGO II design by increasing the cross section of the silica suspension.

LIGO II parameters as defined in January 2000



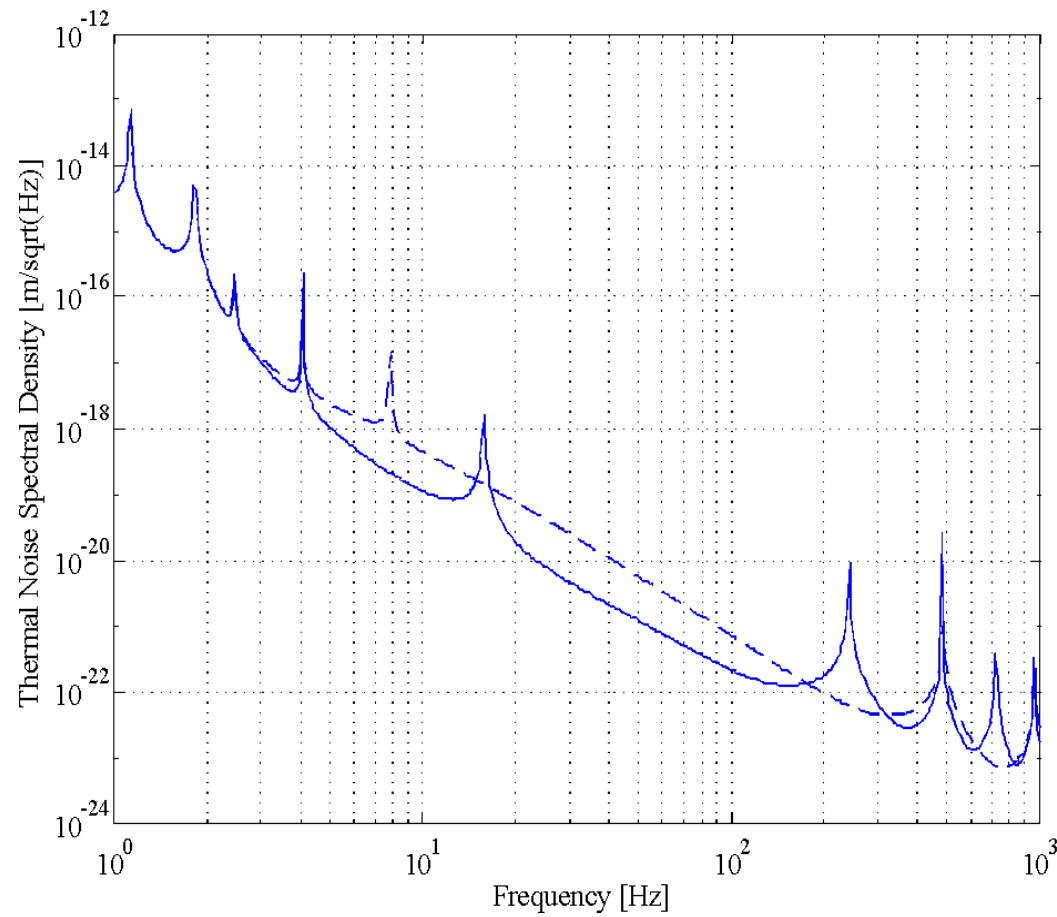
Ribbons: New Model



— Thermoelastic
Damping nulled
(200x2069)um

- - - January parameters

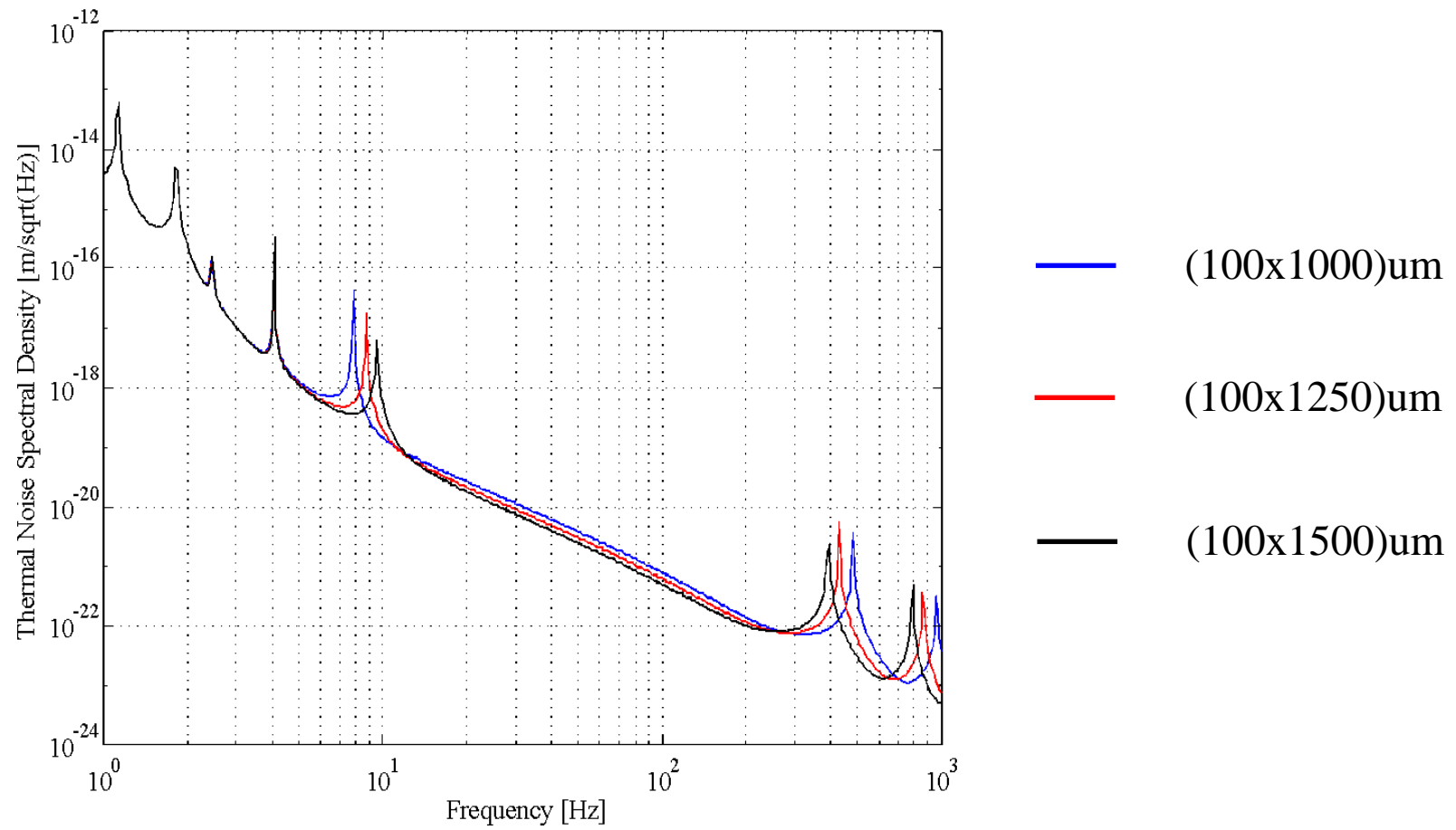
Fibres: New Model



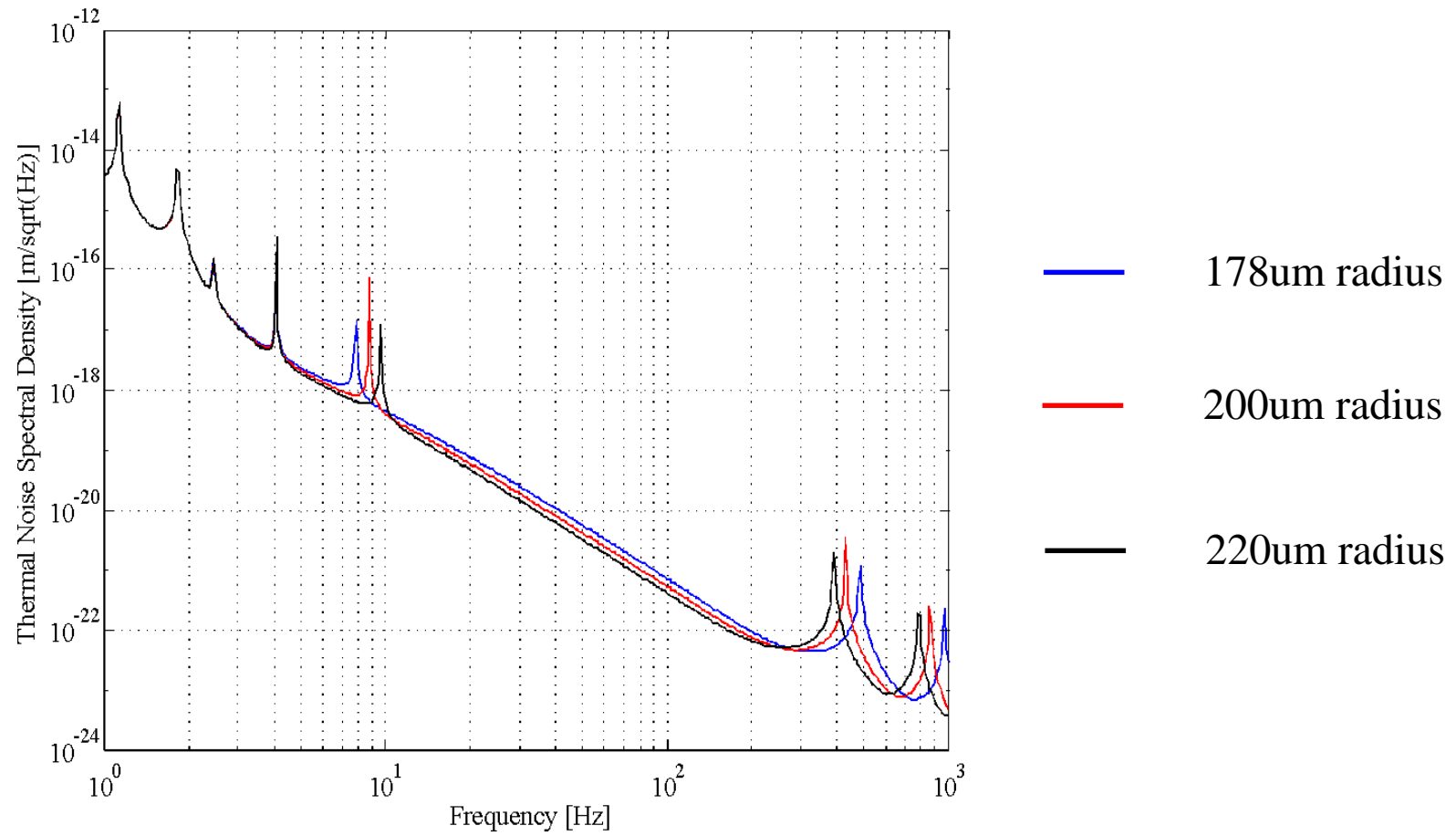
— Thermoelastic
Damping nulled
(362um radius)

- - - January parameters
(178um radius)

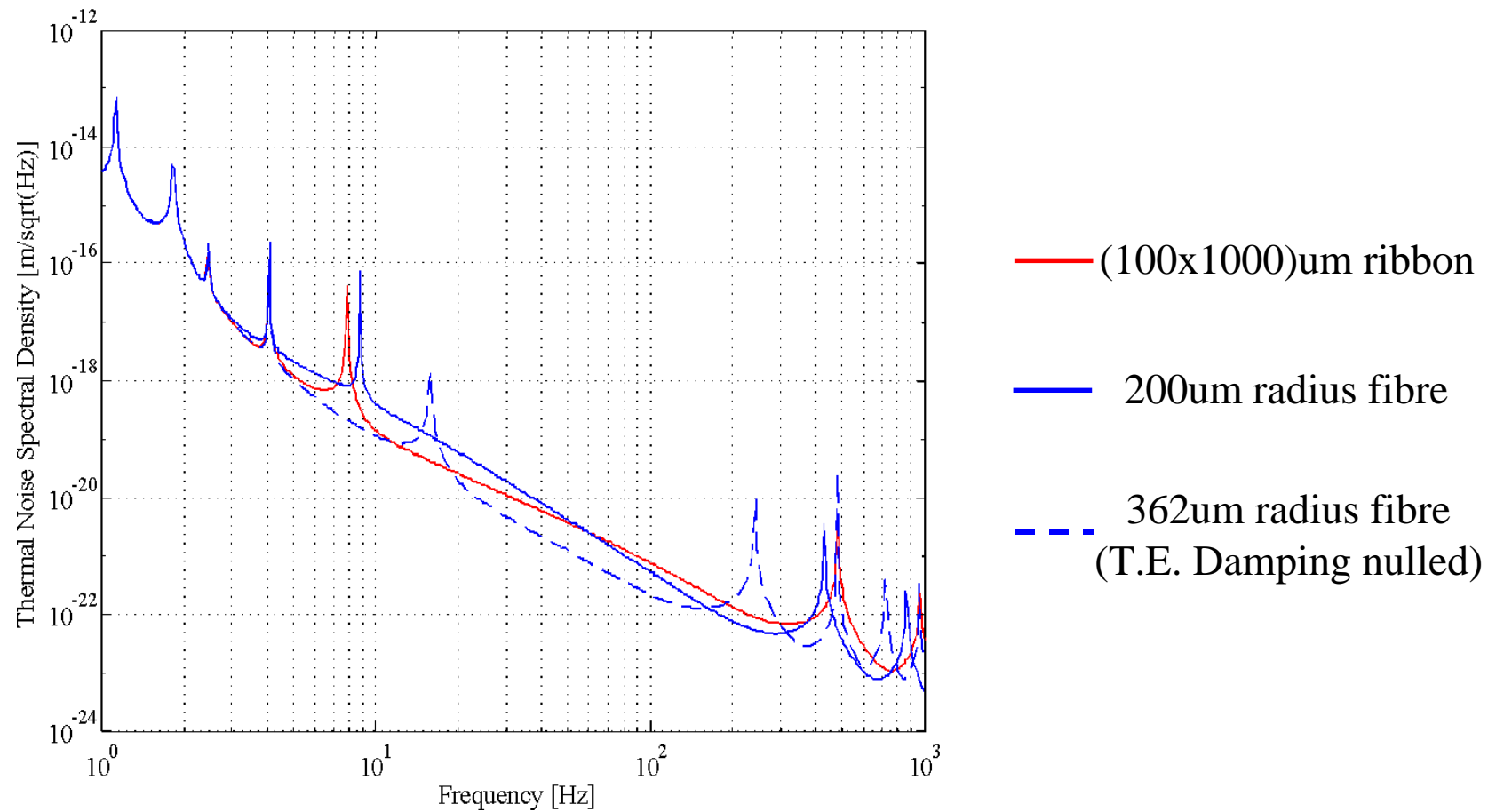
Ribbons: New Model

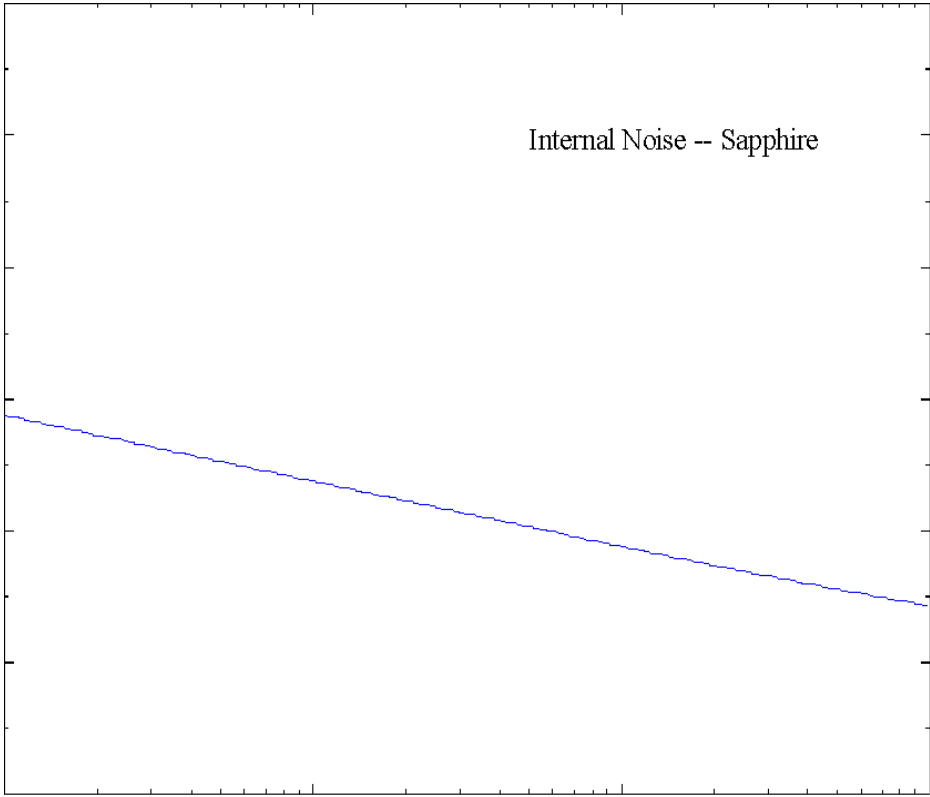


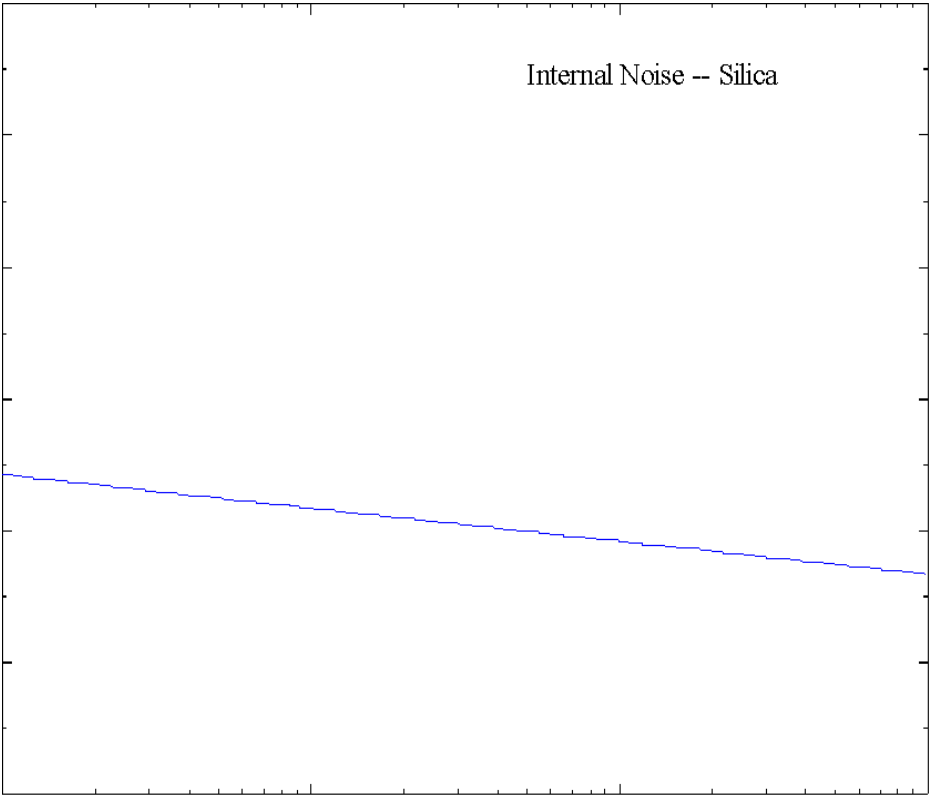
Fibres: New Model

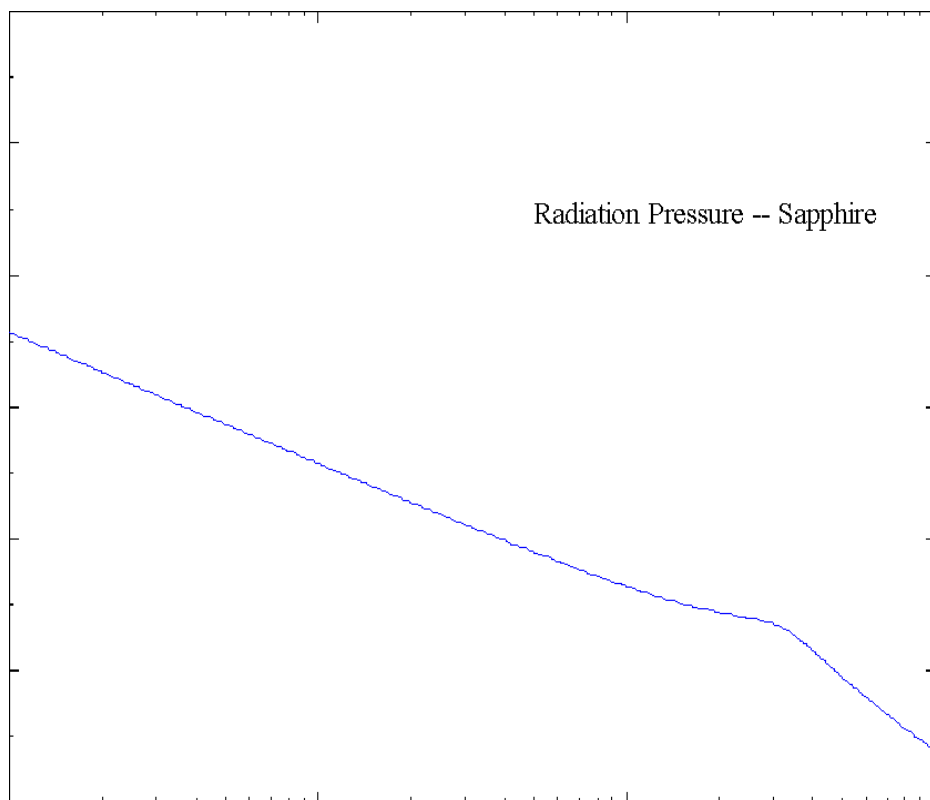


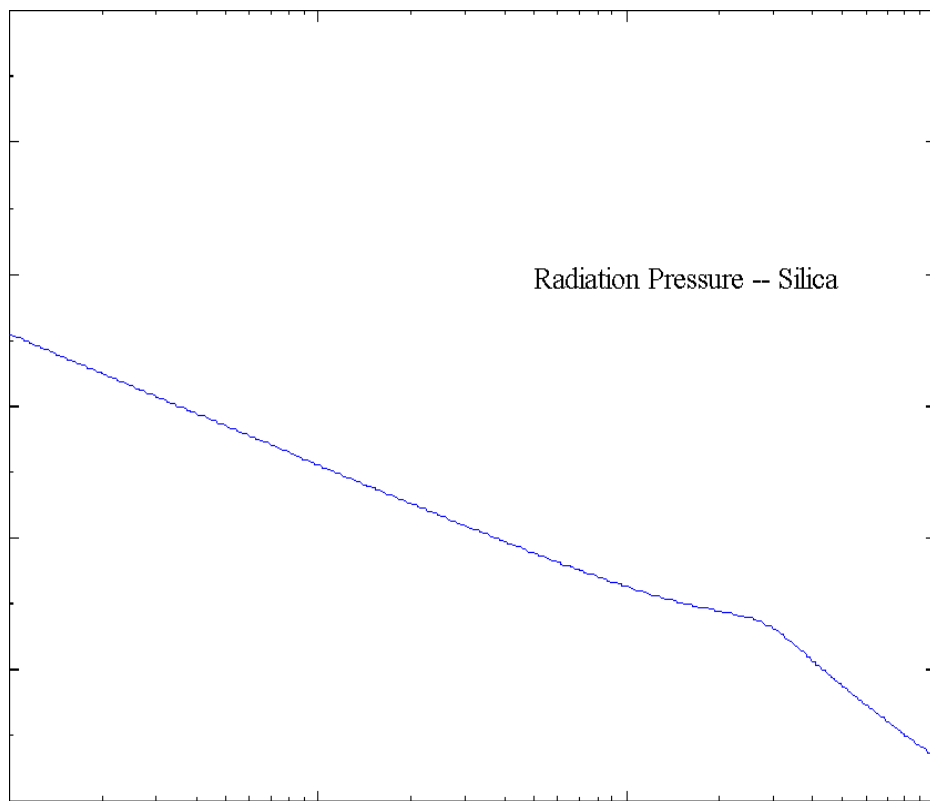
Comparison Between Ribbons and Fibres











Angular Noise Coupling

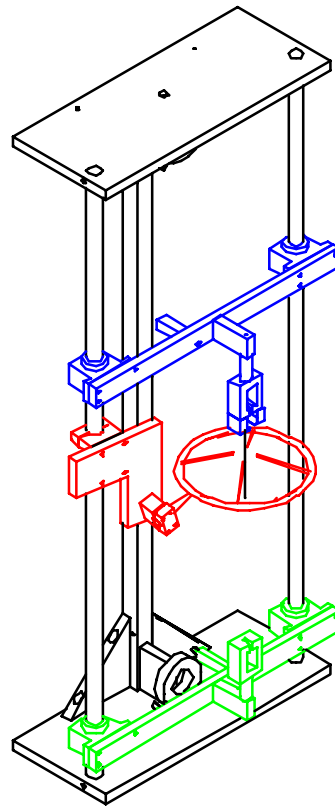
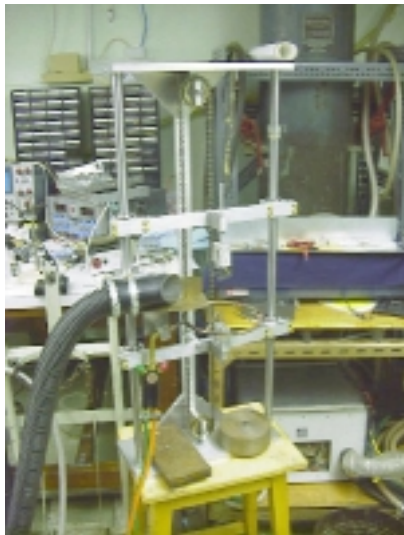
- Not yet implemented into this model from Husman's model (Ph.D. Thesis)
- **Tilt noise most important** - can make good estimate from parameters of last stage
 - $I_{tm} = 0.18$; $I_{int} = 0.36$; $f_{tilt} \sim 0.75$ Hz; $Q \sim 10^6$
 - $\Delta\theta \sim 4 \times 10^{-17}$ rad/ $\sqrt{\text{Hz}}$ at 10 Hz
- **Coupling to horizontal $< 10^{-19}$ m/ $\sqrt{\text{Hz}}$ at 10 Hz if beam offset < 3 mm**



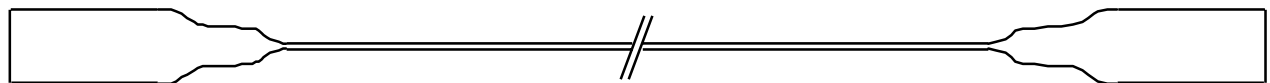
Power Recycling
Mirror in position

Fibre Production and Strength

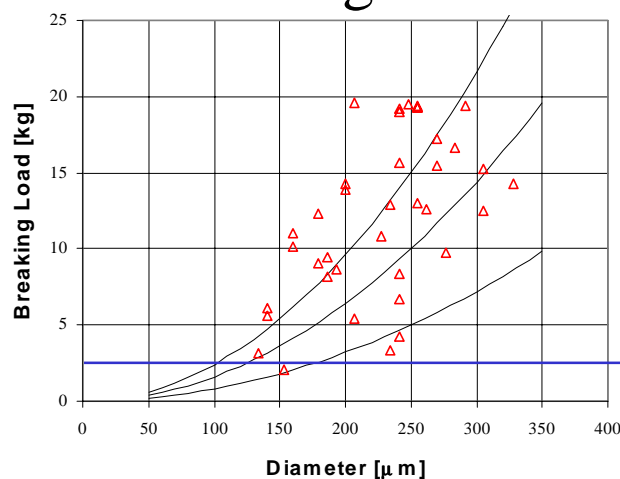
Pulling Machine



The Pulling Machine is being improved to produce fibres even in diameter and length

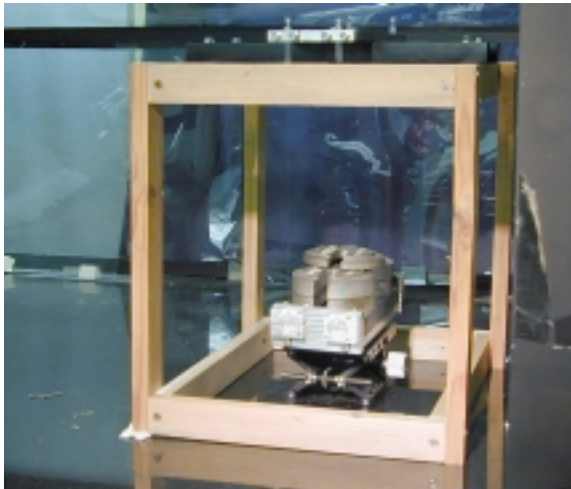
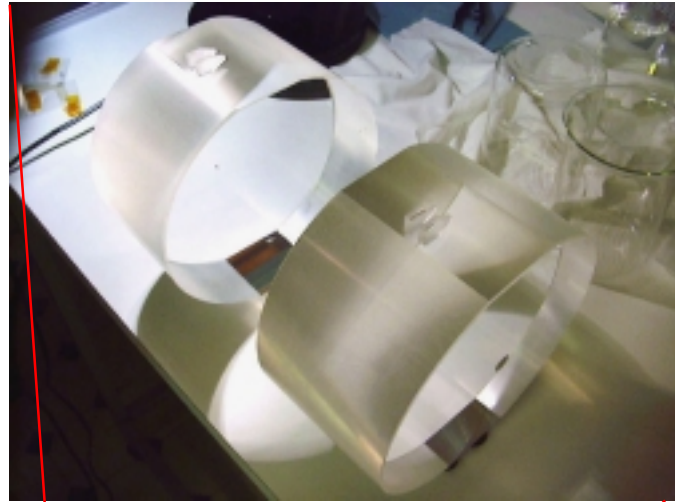


Strength

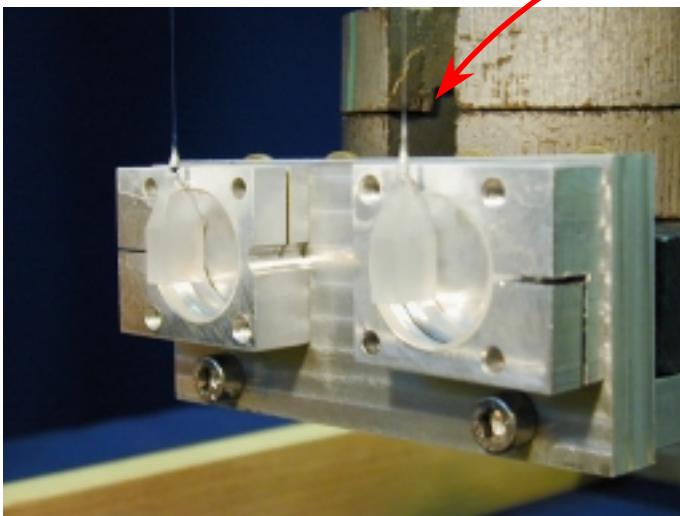
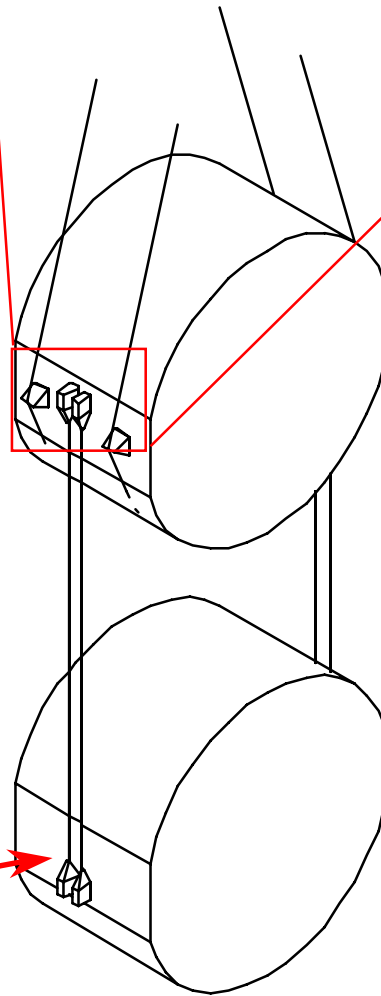


Working load
for GEO

Bonding of the Ears



Since **2nd Nov. 99**
10 kg are suspended
with **4 x 180** micron
diameter **welded** fibres
in air



Welding of the Fibres

Autocad - quadruple suspension

