



# Advanced Interferometer Sensing & Control (ISC)

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- ➔ Responsible for the GW sensing and overall control systems
- ➔ Addition of signal recycling mirror increases complexity
  - ➔ Permits 'tuning' of response to optimize for noise and astrophysical source characteristics
  - ➔ Requires additional sensing and control for length and alignment
- ➔ Shift to 'DC readout'
  - ➔ Rather than RF mod/demod scheme, shift interferometer slightly away from dark fringe; relaxes laser requirements, needs photodiode develop
- ➔ Requires both proof-of-principle and precision testing (40m)
- ➔ Schedule Highlights:
  - ➔ 2Q01: Design Requirements Review
  - ➔ 2Q02: Tabletop DC readout test results
  - ➔ 2Q03: GEO 10m prototype test results/review
  - ➔ 4Q03: Final design complete



# Advanced Interferometer Sensing & Control (ISC)

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- ➔ Subsystem Scope:
  - ➔ optoelectronic sensors\*
  - ➔ signal conditioning electronics \*
  - ➔ servo-control electronics (analog & digital) \*
  - ➔ control topology & laws \*
  - ➔ locking algorithm
  - ➔ interferometer supervisory controls
  - ➔ interferometer system diagnostics
  - ➔ calibrated strain readout signal

\* except local PSL loops



# Advanced Interferometer Sensing & Control (ISC)

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- ➔ Research Scope:
  - ➔ low noise ADC & DAC research
  - ➔ segmented, high frequency RF, wavefront sensor
  - ➔ high frequency, low noise RF photodiodes
  - ➔ DSP investigation (to allow more computation-intensive filter techniques and enhance control robustness and timing margins)
  - ➔ Control law/topology design
  - ➔ Controls and electronics testing (definition & assist to GEO 10m & LIGO 40m experiments)
  - ➔ Simulation extensions & modeling



# Advanced Interferometer Sensing & Control (ISC)

- ➔ Signal- & power-recycled interferometer has 8 independent optical path lengths, one identical to re-scaling the wavelength
- ➔ independent and significant alignment degrees of freedom:
  - ➔ 12 angular & 2 centering dof for the core optics
  - ➔ 2 angular & 2 centering dof for the input mode cleaner
  - ➔ 2 angular dof for the input mode cleaner
- ➔ 28 'global' degrees of freedom

<i>Symbol</i>	<i>was</i>	<i>Description</i>	<i>Definition</i>
<b><i>D</i></b>	<i>L<sub>-</sub></i>	<i>Arm cavity differential (a strain)</i>	$(ETM_x - ITM_x) - (ETM_y - ITM_y)$
<b><i>C</i></b>	<i>L<sub>+</sub></i>	<i>Arm cavity common mode</i>	$(ETM_x - ITM_x)/2 + (ETM_y - ITM_y)/2$
<b><i>m</i></b>	<i>l<sub>-</sub></i>	<i>Michelson differential</i>	$(ITM_x - PRM) - (ITM_y - PRM)$
<b><i>p</i></b>	<i>l<sub>+</sub></i>	<i>Michelson common mode</i>	$(ITM_x - PRM)/2 + (ITM_y - PRM)/2$
<b><i>s</i></b>	<i>~</i>	<i>Signal recycling cavity length</i>	$(ITM_x - SRM)/2 + (ITM_y - SRM)/2$
<b><i>I</i></b>	<b><i>I</i></b>	<i>Laser wavelength</i>	
<b><i>i</i></b>	<i>l<sub>MC</sub></i>	<i>Input mode cleaner length</i>	
<b><i>o</i></b>	<i>~</i>	<i>Output mode cleaner length</i>	



# Advanced Interferometer Sensing & Control (ISC)

- ➔ Schnupp asymmetry/frontal modulation method (used in initial LIGO) is extended by adding a second set of resonant sidebands
- ➔ The three auxiliary cavity lengths  $p$ ,  $m$  and  $s$  are measured with minimal interaction from the arms, by looking at beat notes between the two sideband systems:
  - ➔ directly at the difference frequency, in the reflected port
  - ➔ by double demodulation, at the antisymmetric port
- ➔ The arm cavity mean length  $C$  is readily derived from interference of the 9 MHz sidebands with the returning carrier at the reflected port
- ➔ 'DC readout' of the gravitational wave signal  $D$ , rather than the traditional RF homodyne detection
- ➔ robust separation is achieved between the internal coordinates

Port	Frequency	$C$	$D$	$p$	$m$	$s$
Reflection	171 MHz	-0.4	0	<b>80</b>	-1	40
PRC Sample	171 MHz	-2	0	72	-63	<b>960</b>
Antisymmetric	171 MHz	0	0	0.1	<b>-1</b>	<b>1.95</b>
Antisymmetric	189 MHz	0	0	-0.3	<b>-1</b>	<b>-1.95</b>





# Advanced Interferometer Sensing & Control (ISC)

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- ➔ preliminary modeling:
  - ➔ with the planned advanced SEI & SUS attenuation
  - ➔ damping and control of the auxiliary  $p$ ,  $m$  and  $s$  lengths ( $< 10^{-10}$  m RMS, adequate to reject optical noise effects) requires only  $\sim 1$  Hz unity-gain loop bandwidths
- ➔ allows a full frequency decade below the noise-critical sensing band for aggressive signal filtering
- ➔ If actuation for auxiliary lengths are applied to the BS, PRM & SRM, contamination of the gravitational wave readout  $D$  will be minimal:
  - ➔ Noise figures in the range of  $10^{-14}$  m/Hz<sup>1/2</sup>, some million times noisier than the strain readout, could be tolerated
  - ➔ depends, on the development of adequate low-noise (e.g., passive eddy-current) damping for the suspension eigenmodes of the cavity mirrors to obviate the need for interferometric damping feedback.



# Servo-Controls Research Tasks

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- ➔ advanced SEI & SUS systems will have radically different controller interfaces
  - ➔ actuation to upper stages which are separated from the mirror position (readout variable) by complex mechanical transfer functions
  - ➔ anticipate significant work required to define pre- and post-conversion signal processing for each of these stages, with the goal of building a composite virtual "super actuator" for each degree of freedom
  - ➔ controllability issues may play a strong role in the suspension actuator selection
- ➔ Software tools for control algorithm construction & maintenance:
  - ➔ initial LIGO control loop software is implemented in compiled C code
  - ➔ successful and efficient, but cumbersome to adapt to new purposes and depends on a high degree of programming expertise
  - ➔ intend to preserve our substantial investment in the EPICS/VxWORKS architecture
  - ➔ propose to develop dynamic libraries, programming tools and user interface layers for our existing realtime operating systems and application environments





# Servo-Controls Research Tasks (continued)

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- ➔ Modeling & Analysis: extend to signal recycled configuration
  - ➔ MELODY
  - ➔ FFT Propagation Code
  - ➔ Modal Model
  - ➔ Matlab IFO Control Model
  - ➔ End-to-End (E2E)
  - ➔ validate models with 10m and 40m experiment results
- ➔ Servo-control topology and control law development
  - ➔ robust control approach, with initial LIGO experience in modeling uncertainties and plant & disturbance variability
  - ➔ define control laws & deliver code to 40m experiment



# Advanced Controls & System Identification (SID)

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- ➔ Programmatic Scope:
  - ➔ Integrated with the ISC design effort
  - ➔ Initial LIGO
  - ➔ Advanced LIGO
  - ➔ interfaces with existing infrastructure
- ➔ Technical Scope:
  - ➔ Robust modern control approach
  - ➔ Optimal controls approach
  - ➔ System identification
  - ➔ Adaptive control



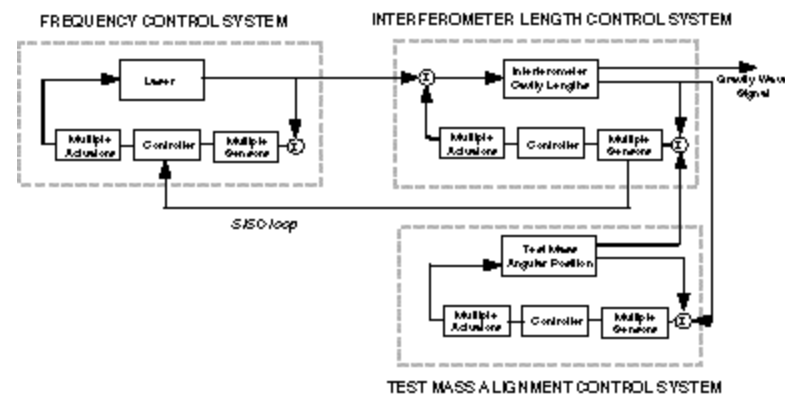
# Advanced Controls & SID Motivation

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- ➔ Challenging LIGO detector availability goals:
  - ➔ Single interferometer operations > 90% of the time with 40 hr. min. continuous lock periods
  - ➔ Double coincidences > 85% time and triple coincidences > 75% time with 100 hr. min. continuous lock periods
- ➔ 40 m prototype experience:
  - ➔ 40m prototype lock durations vary from seconds to a few hours
  - ➔ Control system instabilities caused by drifts in the interferometer system parameters
  - ➔ Displacement noise events which kick the interferometer out of lock
- ➔ Initial LIGO experience:
  - ➔ Lock durations currently limited by tidal drift to ~hours; with tidal actuation may be limited to a few days between earthquakes that knock cavities out of lock
  - ➔ Too early to tell if alignment or parameter drift is a serious problem or not; system is 'maturing' and becoming (or perceived as?) more stable with time

# Advanced Controls & SID

- ➔ LIGO has frequency, length and alignment servo-control loops
  - ➔ The optical model for the core optics length control system is a 4x4 matrix of transfer functions
- ➔ The interferometer optical alignment model is a 10x10 matrix of transfer functions whose elements have a similar form





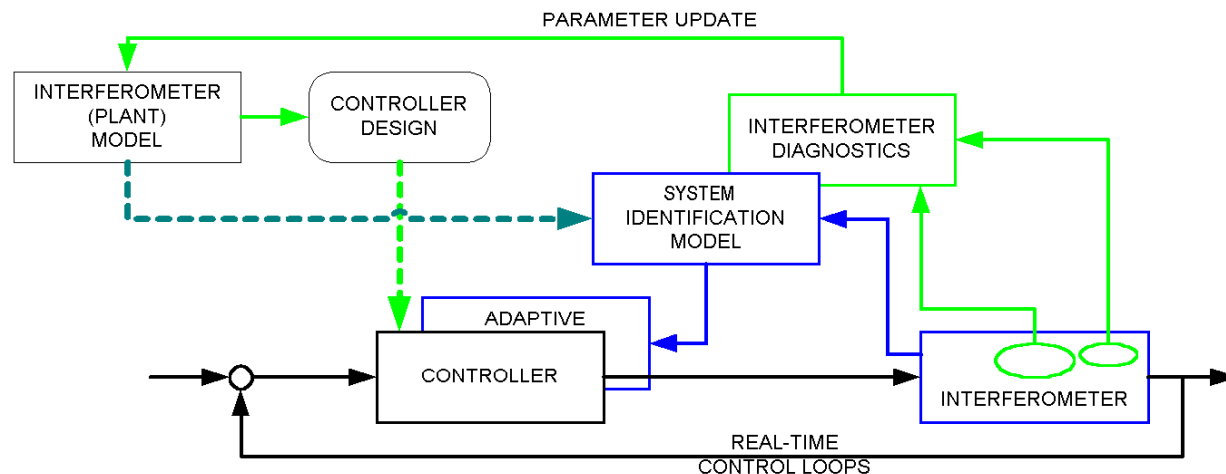
# Advanced Controls & SID

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- ➔ Potential hardware imperfections, model errors, unknowns or parameters subject to drift which could effect control system robustness include:
  - ➔ Beamsplitter reflectivity  $\neq 50\%$
  - ➔ Mixer phase error
  - ➔ Deviations from resonance
  - ➔ Visibility variation
  - ➔ Fabry-Perot cavity input and end test mass absorption (resulting in radius of curvature changes)
  - ➔ Sensor & actuator cross-talk (optical, mechanical & electrical)
  - ➔ Alignment/length Coupling
  - ➔ Modulation depth & phase variation
  - ➔ etc.

# Strategy

- ➔ System identification will be used in conjunction with subsystem diagnostic and measurement techniques to update our understanding of the system and its control
- ➔ Once the system susceptibilities are understood, an adaptive controller can be formulated to compensate
- ➔ SID and Adaptive Control are mature technologies; The application to Interferometry is unique



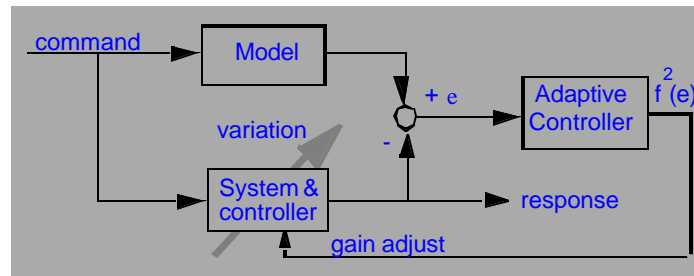


# System Identification

- ➔ System Identification (SID) is an empirical approach to modeling interferometer system dynamics
  - ➔ Non-parametric identification (i.e. frequency response estimation)
  - ➔ Parametric system models (e.g. state space representation)
- ➔ For LIGO we seek a recursive, real-time parameter identification of the multi-input/multi-output optical response of the interferometer in Detection Mode
- ➔ Many techniques are available and will be explored; Potential candidates include:
  - ➔ Generalized Least Squares and Maximum Likelihood Estimators (e.g. the Prediction Error Method) are computationally simple
  - ➔ Observer/Kalman Filter Identification (OKID) -- time domain based, can be extended to identification of closed loop effective controller/observer combination (Observer Controller Identification, OCID)
  - ➔ State-Space Frequency Domain (SSFD) identification -- frequency domain based (can use spectrum analyzers)

# Adaptive Control

- ➔ Adaptive Control can improve sensitivity while maintaining robustness to disturbances and plant variations
- ➔ Adaptive control time scales:
  - milliseconds for the ordinary feedback
  - many minutes for updating the control parameters and performing SID
- ➔ Possible adaptive control algorithm: Model Reference Adaptive Control

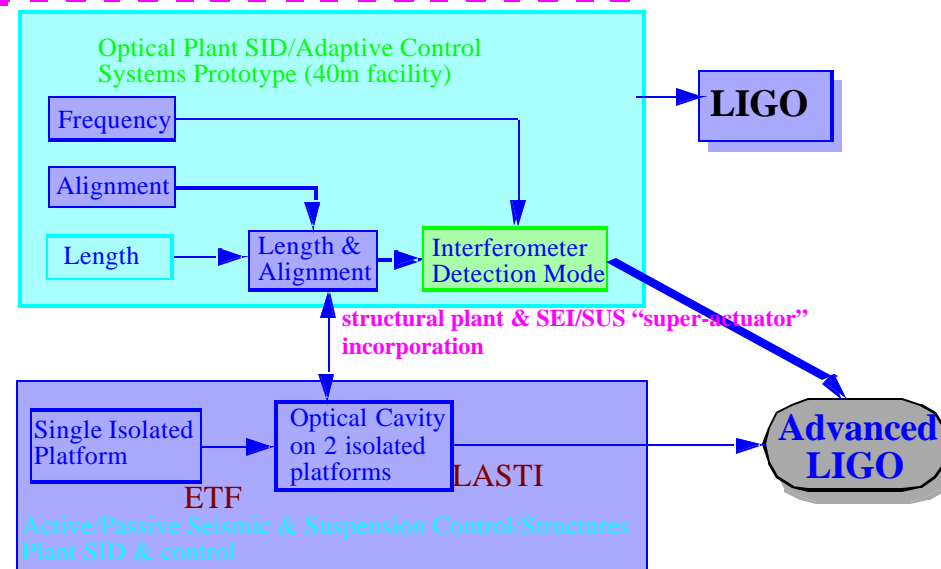






# Collaborators & Responsibilities

- Stanford Univ. plans to explore system identification and adaptive control on advanced seismic isolation and suspension subsystems
- LIGO will concentrate on identification and control (length, alignment and frequency) of the optical plant for a power recycled configuration
- GEO plans to explore adaptive control for autonomous and tele-remote operation





# Advanced Controls & SID

## ➔ Schedule Highlights

- ➔ 4Q02: System identification for the initial LIGO detector
- ➔ 4Q03: Adaptive control for the initial LIGO detector
- ➔ 1Q04: Application to 40m configuration testbed
- ➔ 2Q05: System identification for the advanced LIGO configuration



# Advanced Interferometer Systems, Sensing & Control (ISC, 40m, SID, SYS)

FY02

	Org	Adv. R&D (FTE)	LSC Support R&D	Operations (FTE)		
<b>Advanced Interferometer Systems, Sensing &amp; Control (ISC)</b>						
Sci & PD	MIT	0	0			6.87
	CIT	2	0	3.2	5.2	
UG & Grads	MIT	1	0	1	2	5
	CIT	3	0	0	3	
Eng & Techs	MIT	0	0	0.75	0.75	10.23
	CIT	0	0	9.48	9.48	
Totals (FTE):		6	0	16.1	<b>22.1</b>	
Equip. & Supplies (\$K)		\$275	\$0	\$0	<b>\$275</b>	

N.B.: Does not include LSC research staff.