



Effect of wire stiffness on pitch modes and correction thereof

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SUS Design Philosophy/Methodology

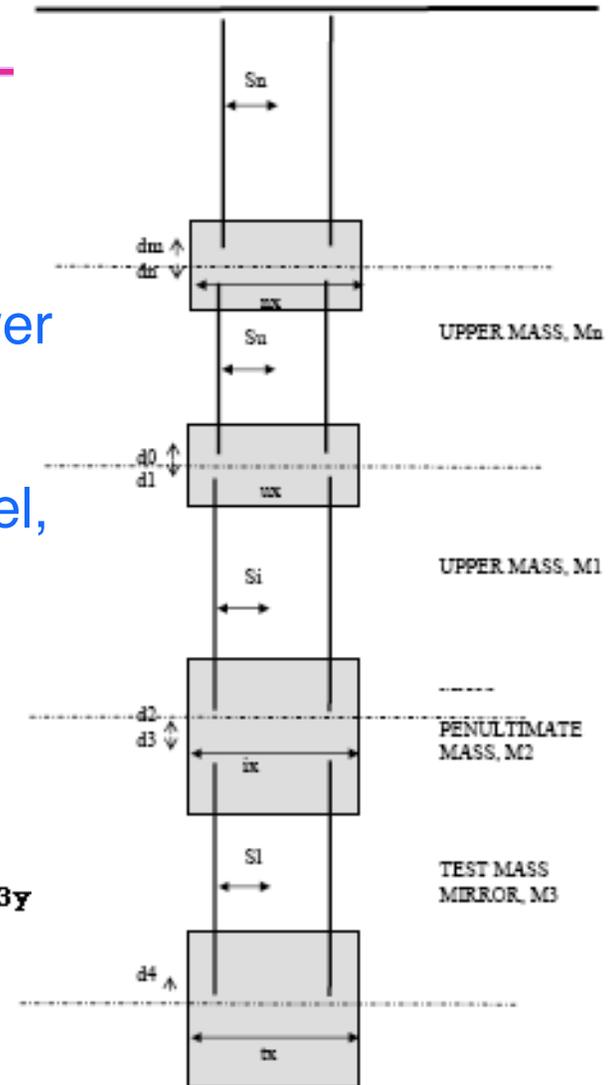
- Quad/triple pendulum has 24/18 rigid body normal modes
 - » Want all frequencies as low as possible
 - All but highest frequency vertical and roll modes in range ≈ 0.4 to ≈ 4 Hz.
 - » Want anti-node at top mass for good local control
- Initial design uses mostly Matlab software by Calum Torrie et al. with improved stiffness matrix elements by Mark Barton
 - » Wire stiffness is neglected
 - » Inaccurate for fundamental pitch mode

Fundamental Pitch Mode

- Only 2 top wires instead of 4 => $s_n=0$
- Fundamental pitch mode has masses moving in phase, ganged together by lower pairs of wires
- For ideally flexible wire as in Matlab model, frequency is set by gravitational restoring torque (weighted sum of d 's) and sum of MOIs:

$$\begin{aligned}
 \mathbf{kk} = (& \\
 & (m_n+m_1+m_2+m_3) g d_n \\
 & +(m_1+m_2+m_3) g (d_n+d_0) \\
 & +(m_2+m_3) g (d_1+d_2) \\
 & +m_3 g (d_3+d_4) \\
 &) \quad \mathbf{II} = I_ny+I_1y+I_2y+I_3y
 \end{aligned}$$

$$ff = \text{Sqrt}[\mathbf{kk}/\mathbf{II}]/2/\text{Pi}$$



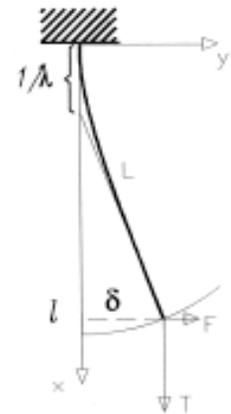
Wire Stiffness - Simple Pendulum Case

G. Cagnoli et al., Physics Letters A 272 (2000): 39 – 45

- The wire can be modeled as an elastic beam under tension (x =longitudinal, y =displacement, T =tension, Y =Young's modulus, I =moment of area, ρ =density):

$$YIy'''' - Ty'' = \rho \frac{\partial^2 y}{\partial t^2}$$

- At low frequency, $y(x) = \frac{F}{T\lambda} [e^{-\lambda x} + \lambda x - 1]$ $\lambda = \sqrt{T/Y_0 I}$
- Pendulum frequency increases due to two effects
 - » Wire is effectively shorter by $0.5/\lambda$ => extra gravitational restoring force
 - » Wire is stiff => elastic restoring force equivalent to another $0.5/\lambda$ of length change



Old Application To Quad

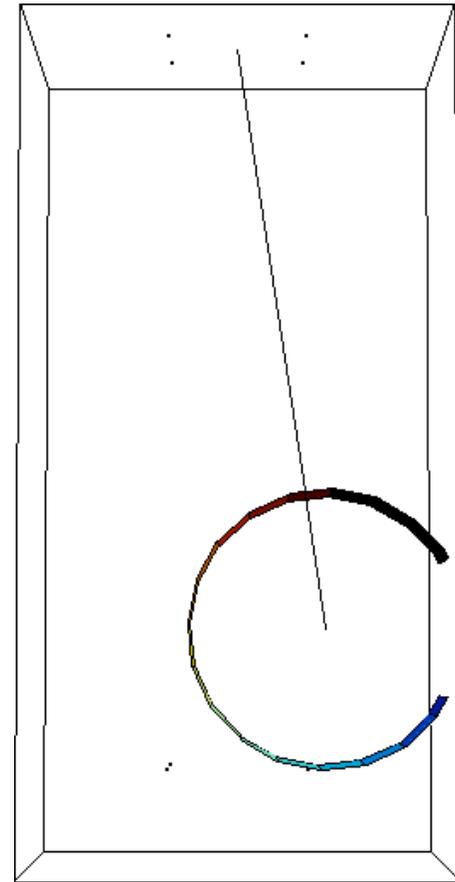
- For the quad pendulum, the d's from the Matlab model were “corrected” by amounts of $1/\lambda$
- But $1/\lambda$ is typically rather larger than the raw d's:

`{4.97277, 3.26511, 2.88802, 0.951584}` $1/\lambda$ in mm
for ETM prototype, T040214-01
cf. all d's = 1 mm

- If the wire stiffness effect is only slightly less than assumed, the pendulum will be unstable!
- As-built pendulum was unstable(!) - is this the problem?

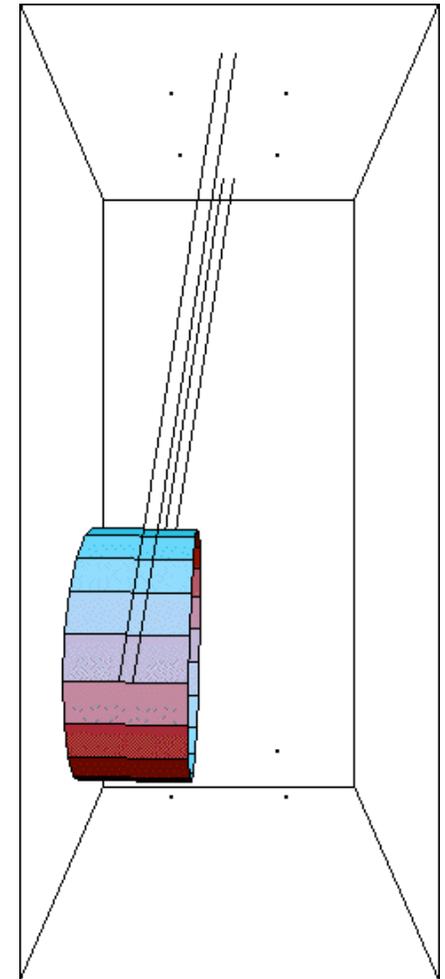
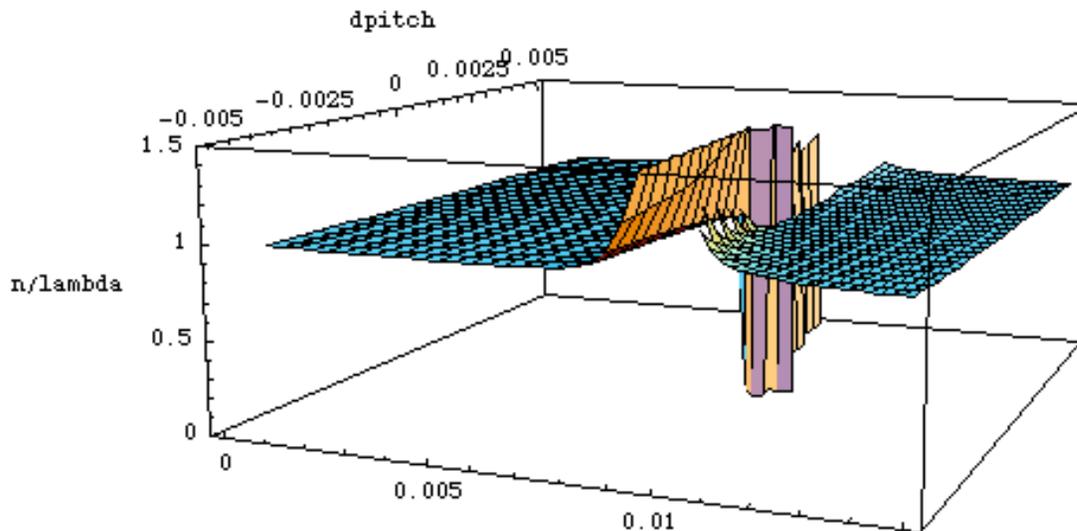
Simple Pendulum With Pitch DOF

- Does a pitch mode need the same correction as a pendulum mode?
- A simple pendulum model was created to check.
- Yes, the pitch flexure correction is exactly $1/\lambda$.



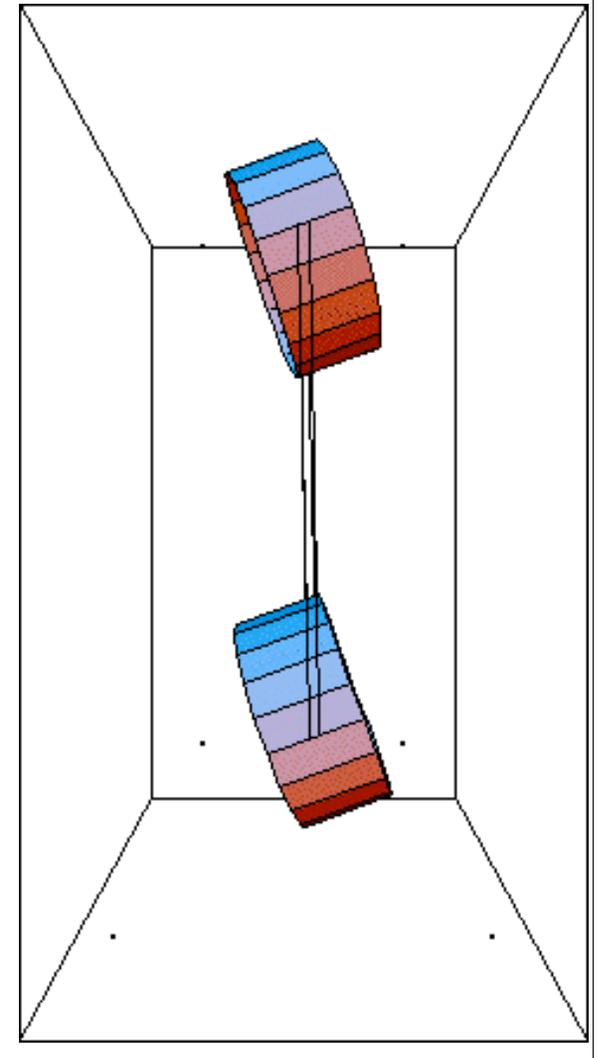
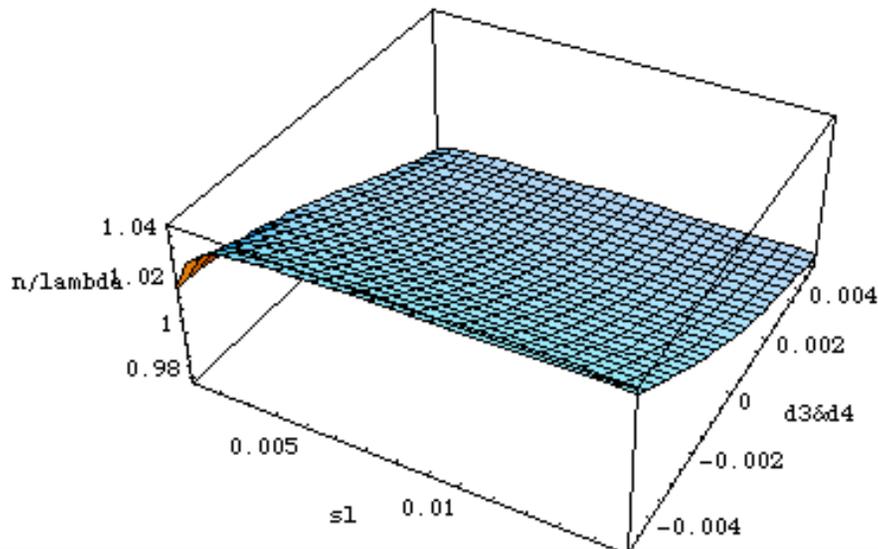
Four-Wire Simple Pendulum

- How about a four-wire pendulum?
- The pitch frequency depends mostly on the wire elasticity, not gravity.
- Yet, the pitch flexure correction is still $1/\lambda$ except where the pitch and pendulum frequencies are nearly equal.



Four-Wire Two-Mass Pendulum

- How about two masses both free to pitch (the upper one hinged)?
- Yes, the flexure correction is still almost exactly $1/\lambda$ (if applied at both top and bottom of each wire).



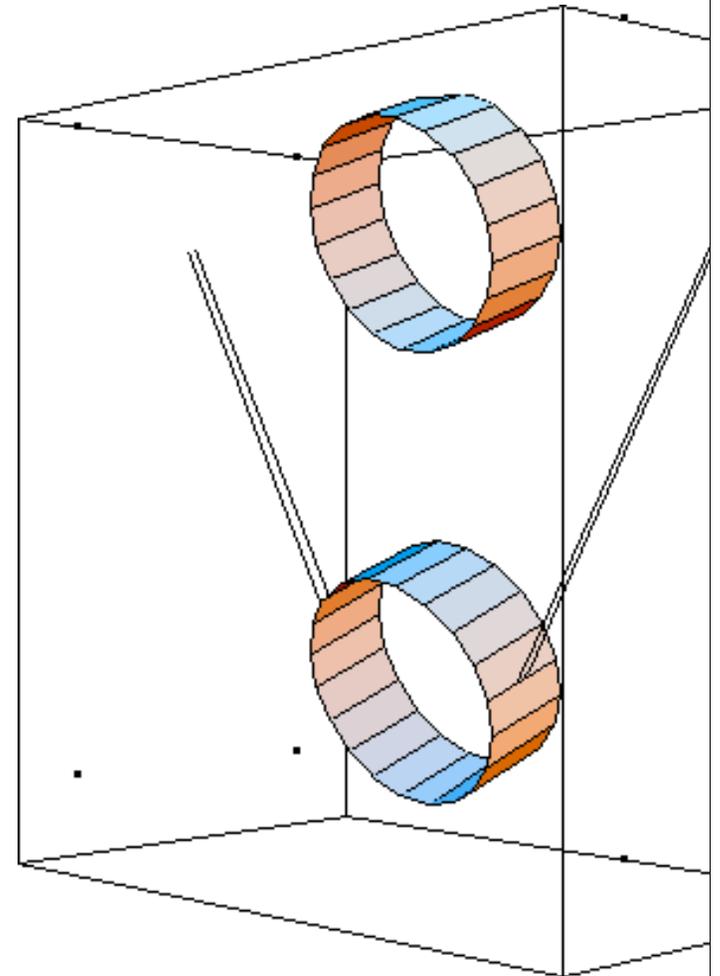
Diagonal Wires

- How about wires further apart in transverse at the top than at the bottom?
- Computation is too slow for a plot to be feasible, but spot checks suggest flexure correction is

$\text{Cos}[\theta]/\lambda$

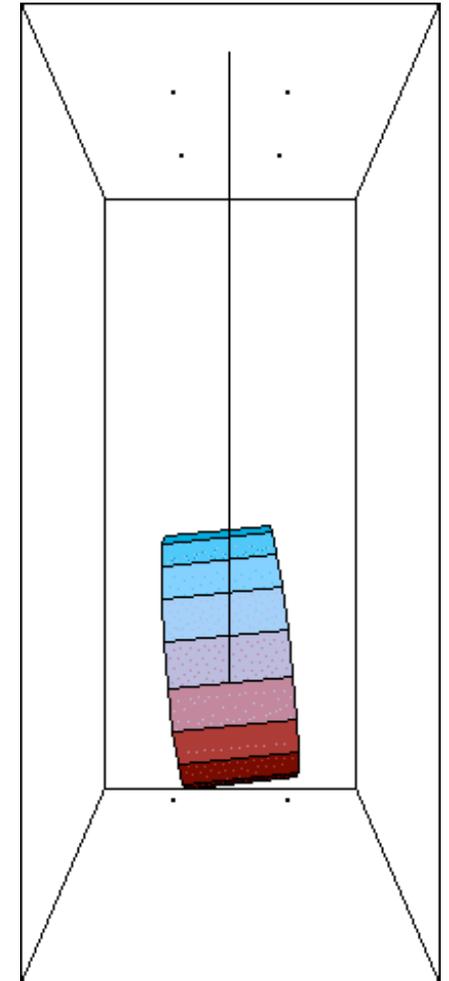
if λ is still calculated in terms of the tension in the wire.

- This is actually a factor of $\text{Cos}[\theta]^{(3/2)}$ smaller than what was used for the quad because the vertical load was used instead of the tension.



Experimental Check

- A two-wire LIGO-I style pendulum was constructed in the lab to check.
- Expected frequency with flexible wire: 0.325 Hz (unstable)
- Expected frequency with stiff wire: 0.359 Hz
- Measured frequency: 0.422 Hz
- Fair agreement.



Check With Quad Model

- Used parameters from ETM Quad Prototype Design (T040214-01) in Mark Barton's Mathematica quad model.
- Corrected d's using new flexure theory.
- Mathematica "Stage2" results (i.e., with wire stiffness) agree very closely with Matlab results (with neither wires stiffness nor correction thereof).

| N | f | type | |
|----|-----------------|--------|--------|
| 1 | <u>0.379244</u> | pitch3 | pitch2 |
| 2 | <u>0.443433</u> | pitch3 | pitch2 |
| 3 | 0.672038 | z3 | z2 |
| 4 | 0.997526 | pitch0 | x2 |
| 5 | 1.27192 | pitch0 | pitch1 |
| 6 | 1.6833 | pitch0 | pitch2 |
| 7 | 2.00385 | x0 | x1 |
| 8 | 2.52876 | z0 | z1 |
| 9 | 2.95722 | pitch1 | |
| 10 | 3.42948 | x1 | x0 |
| 11 | 4.22801 | z1 | z0 |
| 12 | 8.83338 | z2 | z3 |

longpitch1: [0.3797 0.4408 0.9898 1.2736]

longpitch2: [1.6838 1.9753 2.9580 3.3722]

vertical: [0.6602 2.4795 4.1289 8.8326]

Conclusion

- We think we now have a good understanding of how to allow for wire stiffness.
- The old corrections were not quite right.
- The new corrections are not sufficiently different to explain the instability we're seeing.
- More head-scratching required.