



### Advanced LIGO PSL Power Stabilisation

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#### • Lots of hard work done by

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 An injection-locked high power stage seeded by a 35-W four-stage MOPA front end with a 2-W NPRO master oscillator.







# The Advanced LIGO Laser (cont.)

#### • Power actuators available:

- » NPRO pump diode current
- » AOM located between master oscillator and power amplifier
- » Power amplifier pump diode current
  - Possibly via a current shunt
- » High power stage pump diode current
  - Possibly via a current shunt



## The Advanced LIGO PSL







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## Intensity Noise Requirements

- Low frequency variations over 24 hours, less than 1% peak to peak
- Control band
  - » 0.1 to 0.4 Hz < 10<sup>-3</sup>
    » 0.4 to 10 Hz < 10<sup>-4</sup>
- software routine to vary pump diode current



free running









Frequency [Hz]	Relative Intensity Noise [1/Sqrt[Hz]
10	2 x 10 <sup>-9</sup>
10 < <i>f</i> < 500	2 x 10 <sup>-10</sup> <i>f</i>
<i>f</i> >= 500	1x10 <sup>-7</sup>

- The requirement at 10 Hz is very tough due to the combination of:
  - Iow noise level
  - Iow frequency specified



### The Challenge



• What limits the power stabilisation performance?

- » Typically more than enough servo gain to suppress the relative intensity noise to the required level.
  - Observe a difference between an in-the-loop photodetector and an out-ofthe-loop photodetector.
- Is there a fundamental limit? Or are there noise mechanisms not found yet?
  - » Photodiode performance?
    - Uniformity of the diode response
    - Temperature effects
  - » Beam pointing?
  - » Acoustics



## **Power Stabilisation Setup**

• Uses an AOM

- » Power actuator independent of laser
- Beam pointing filtered by a pre-modecleaner (*F* ~ 4100)
- Active temperature stabilisation of the photodetector
  - » With 130 mW on photodetector, temperature rises ~ 10 K
- Optimisation of stabilisation loop shape
  - » AC-coupled loop for lowest noise
  - » DC-coupled loop for a stable operating point



















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### **Important Considerations**

- Avoid ground loops, even at RF frequencies
  - » Use battery powered devices
  - » Separate power supplies for components
- Beam pointing
  - » Use pre-modecleaner
  - » Adjustment of photodetectors
- Acoustics

- » Quiet environment
- » Proper mechanical design
- Convection currents
  - » Place components in vacuum



## Photodiode Uniformity

• There is a "sweet spot" on a photodiode.

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- » Not necessarily at the centre!
- » Minimises the coupling between pointing and intensity noise.



#### spatial uniformity measurement



#### **Balanced Detection**



- Is excess noise at low frequencies due to the photodetectors?
- Iaser stabilised below 10-8
- amplification after subtraction of photocurrents





#### **Balanced Detection Results**









- What is the source of the ~1/Sqrt[f] noise at low frequencies?
  - » Beam pointing introduced by the beamsplitter after the pre-modecleaner cavity.
  - » Photodiode material

- Noise when holes and electrons re-combine
- » Resistor current noise







10-6 Johnson noise 100 , 300K Welwyn PCF0805, 0.1%, 5ppm Phycomp TFx13 series, 0.1%, 25ppm Vishay Beyschlag MMA 0204, 1%, 50ppm Vishay SMM0204-MS1, 1%, 50ppm Wirrom ZC 0204, 1%, 50ppm Mira Electronic 2005, 1%, 100ppm Yageo RC 0805, 1%, 100ppm Yageo RC 1206, 1%, 100ppm 1/ f 10 Ξ Έ 10<sup>-8</sup> oltage noise [V/ voltage r 10<sup>-8</sup> 10<sup>-9</sup> 10<sup>-9</sup> 100  $10^{1}$ 10<sup>2</sup> 10<sup>3</sup>  $10^{4}$ 10<sup>0</sup>  $10^{1}$ frequency [Hz]

resistor current noise / 100 / SMD / P<1W / 10V voltage drop











- Further reduction of beam pointing
  - » Elimination of the beamsplitter
  - » Use of modecleaner cavity as the beamsplitter
- Influence of photodetector temperature fluctuations







• Minimise beam pointing

- Careful selection of photodiodes
- Use metal foil resistors for best performance at low frequencies

