

Note on the derivation of the angular momentum and spin precessing equations in SpinTaylor codes.

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This is a technical note meant to accompany the SpinTaylor waveform review to explain how the derivative of the Newtonian angular momentum is computed. A future development would be to include in the code instantaneous spin² terms.

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I. TIME DERIVATIVE OF THE NEWTONIAN ANGULAR MOMENTUM UNIT VECTOR

The evolution equations for precessing spins and orbital angular momentum are obtained by imposing

$$\dot{\hat{L}} = -\dot{\vec{S}}_1 - \dot{\vec{S}}_2, \quad (1)$$

i.e. imposing total angular momentum conservation and neglecting angular momentum emission by radiation, which is given by, see e.g. (4.115) of [1]

$$\frac{dL}{dt} = \frac{32}{5}\eta^2 M v^7 = \frac{32}{5M}\eta v^8 L, \quad (2)$$

with $\eta \equiv m_1 m_2 / M^2$ the symmetric mass ratio, $m_{1,2}$ individual binary constituent masses and $M \equiv m_1 + m_2$.

At leading order in the PN expansion parameter x ($x = v^2 = (M\omega)^{2/3}$ in LAL codes, with ω the orbital phase derivative) one has, see e.g. eqs. (8-10) of [2]:

$$\begin{aligned} \dot{\vec{S}}_1 &= \frac{x^{5/2}}{2M} \left(3 - 2\frac{m_1}{M} - \frac{m_1^2}{M^2} \right) \vec{S}_1 \times \hat{L}, \\ \dot{\hat{L}} &= \frac{x^3}{2M} \left(1 + 3\frac{M}{m_1} \right) \hat{L} \times \vec{S}_1 + 1 \leftrightarrow 2. \end{aligned} \quad (3)$$

At alternate PN orders spin derivatives receive contributions from spin² terms (x^n in the

spin-dot equations) and from $L \times S$ terms ($x^{(2n+1)/2}$), with $n = 2$ for the leading order, and L precession equation can be inferred from (1).

At leading order (and up to v^2 order included with respect to the leading) we can assume that Newtonian angular momentum and \vec{L} are parallel: $\hat{L}_N = \hat{L}$, however at higher order the relationship between \vec{L} and \vec{L}_N is actually, see eq. 4.7 of [3]

$$\begin{aligned} \vec{L} = & \hat{L}_N |\vec{L}_N^{(0)}| \left(1 + v^2 L_{1PN} + v^4 L_{2PN} + v^6 L_{3PN} \right) + \\ & v^2 \left[-\frac{5}{6} \left(1 + 3\frac{M}{m_1} \right) \vec{S}_{1l} - \frac{1}{2} \left(1 - \frac{M}{m_1} \right) \vec{S}_{1n} - \left(1 + \frac{M}{m_1} \right) \vec{S}_{1\lambda} + \right] \\ & + v^4 \left[\vec{S}_{1n} \left(-\frac{11}{8} \left(1 - \frac{M}{m_1} \right) + \frac{\eta}{24} \left(1 - 10\frac{M}{m_1} \right) \right) + \vec{S}_{1\lambda} \left(-\frac{5}{2} \left(1 + \frac{M}{5m_1} \right) + \frac{\eta}{3} \left(1 + 4\frac{M}{m_1} \right) \right) \right. \\ & \left. + \vec{S}_{1L} \left(-\frac{7}{8} \left(5 + 3\frac{M}{5m_1} \right) + 7\frac{\eta}{72} \left(1 + 30\frac{M}{m_1} \right) \right) \right] + 1 \leftrightarrow 2, \end{aligned} \quad (4)$$

where

$$\begin{aligned} |\vec{L}_N^{(0)}| &= \frac{m_1 m_2}{v}, \\ L_{1PN} &= \frac{3}{2} + \frac{\eta}{6}, \\ L_{2PN} &= \frac{27}{8} - \frac{19}{8}\eta + \frac{1}{24}\eta^2, \\ L_{3PN} &= \frac{135}{16} + \left[-\frac{6889}{144} + \frac{41}{24}\pi^2 \right] \eta + \frac{31}{24}\eta^2 + \frac{7}{1296}\eta^3, \end{aligned} \quad (5)$$

and we remind that

$$\vec{L}_N^{(0)} \equiv \frac{m_1 m_2}{v} \hat{L}_N \neq \frac{m_1 m_2}{\omega r} \hat{L}_N, \quad (6)$$

and $\vec{S}_{1n} \equiv \hat{n}^i (\hat{n} \cdot \vec{S}_1)$, $\vec{S}_{1\lambda} \equiv \hat{\lambda}^i (\hat{\lambda} \cdot \vec{S}_1)$, and $\vec{S}_{1l} \equiv \hat{L}_N^i (\hat{L}_N \cdot \vec{S}_1)$, being \hat{n} , $\hat{\lambda}$ the unit vectors in the direction respectively of binary relative separation and velocity.

Note that we may want to average over one orbit, so that

$$\begin{aligned} \langle n^i \rangle &= \langle \lambda^i \rangle = 0, \\ \langle \hat{n}^i \hat{n}^j \rangle &= \langle \hat{\lambda}^i \hat{\lambda}^j \rangle = \frac{1}{2} (\delta_{ij} - \hat{L}_N^i \hat{L}_N^j). \end{aligned} \quad (7)$$

The spin corrections to the orbital angular momentum are $x^{3/2}$ order with respect to the leading contribution to \vec{L} , that comes from the Newtonian angular momentum. Note also that the spins in this formulae are the physical ones related to the LAL convention \vec{S}_{LAL} by $\vec{S}_{iLAL} \equiv \vec{S}_i / M^2$ (we use here units $G_N = c = 1$). The velocity symbol v in [4] (denoted below v_{Kidder}) differs from the one adopted in LAL (and also in this document):

$$v_{Kidder} \equiv \omega r \neq v_{LAL} \equiv (M\omega)^{1/3}. \quad (8)$$

We have thus a simple precession equation for \vec{L} , but \vec{L}_N , or \hat{L}_N is needed to construct the waveform, since \hat{L}_N is the unit vector perpendicular to the instantaneous orbital plane. We can construct the $\dot{\hat{L}}_N$ by short-circuiting eq. (1) and eq. (4), to first obtain

$$\begin{aligned} |L_N| \dot{\hat{L}}_N &= \frac{d}{dt} \left\{ \vec{L} - v^2 \left[-\frac{1}{4} \left(3 + \frac{M}{m_1} \right) \vec{S}_1 - \frac{1}{12} \left(1 + 27 \frac{M}{m_1} \right) (\hat{L}_N \cdot \vec{S}_1) \hat{L}_N + 1 \leftrightarrow 2 \right] \right\} = \\ &= \frac{v}{\eta M} \left(1 - L_{1PN} v^2 + \dots \right) \left\{ -\dot{\vec{S}}_1 - \dot{\vec{S}}_2 - v^2 \left[-\frac{1}{4} \left(3 + \frac{M}{m_1} \right) \dot{\vec{S}}_1 \right. \right. \\ &\quad \left. \left. - \frac{1}{12} \left(1 + 27 \frac{M}{m_1} \right) \frac{d((\hat{L}_N \cdot \vec{S}_1) \hat{L}_N)}{dt} \right] + 1 \leftrightarrow 2 \right\}, \end{aligned} \quad (9)$$

where we averaged over an orbit and the change in L due to GW emission has been neglected. We can then see various effect here at play:

- $\vec{S} \cdot \hat{L}_N$ interaction at v^{2n-1} order in $\dot{\vec{S}}$ equations starting from $n = 2$
- spin² terms appearing at v^{2n} order, coded only for $n=2$ (leading term) in the orbit averaged version
- terms due to S contamination to L , which affect $\dot{\hat{L}}_N$ equations starting from v^7 order can be turned on by the `LALDict` structure via `XLALSimInspiralWaveformParamsInsertLscorr()`.

This is summarized in tab.I.

On the right hand side for the computation of $\dot{\vec{L}}$ we have to consider spin derivatives up to next⁴ leading order v^9 whereas in the rest of the terms we can use spin derivative at next-to-next leading order and angular momentum derivatives at next-to leading order.

To conclude the implementation of precessional equation we define a precession vector

$$\vec{\Omega}_{\hat{L}_N} \equiv \hat{L}_N \times \frac{d\hat{L}_N}{dt}, \quad (10)$$

such that one can define and implement in LAL

$$\frac{d\hat{L}_N^{(LAL)}}{dt} \equiv \vec{\Omega}_{\hat{L}_N} \times \hat{L}_N = \frac{d\hat{L}_N}{dt} - \left(\frac{d\hat{L}_N}{dt} \cdot \hat{L}_N \right) \hat{L}_N, \quad (11)$$

which can be derived by aid of the identity $(\vec{A} \times \vec{B}) \times C = (\vec{A} \cdot \vec{C})\vec{B} - (\vec{B} \cdot \vec{C})\vec{A}$. The pseudo-vector $\vec{\Omega}_{\hat{L}_N}$ is orthogonal to \hat{L}_N and so it takes into account of only the genuine precession of \hat{L}_N .

order	L	NL	N ² L	N ³ L	N ⁴ L
spinO	3	4	5	6	7
v order	v^5	v^6	v^7	v^8	v^9
$\vec{S} \times \hat{L}$	✓		✓		✓
\vec{S}^2		✓ _{avg}		✗	
\vec{S}^3					✗
J_S			✓ _{flag}	✓ _{flag}	✓ _{flag}

TABLE I: Summary of spin precession effects implemented in the *LALSimInspiralSpinTaylor.c* code in the $\dot{S}_{1,2}$ equations.

II. SPINTAYLORT5

The SpinTaylorT5 waveform construction is explained in [5], here we just recall the basic definitions of the main orbital phase:

$$\frac{d\omega}{dt} = \frac{1}{\frac{dE(\omega)/d\omega}{dE/dt}} = \frac{96M_c^{5/3}\omega^{11/3}}{5(1 + 2E_{1PN} - F_{1PN} \dots)}, \quad (12)$$

with the usual identification $v \equiv (M\omega)^{1/3}$, being M the total mass of the binary system and M_c the chirp mass and we assumed $E = -1/2\eta M(M\omega)^{2/3}(1 + E_{1PN} \dots)$ and $dE/dt = 32/5\eta^2(M\omega)^{10/3}(1 + F_{1PN} + \dots)$.

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