

Results of the deepest all-sky survey for continuous gravitational waves on LIGO S6 data running on the Einstein@Home volunteer distributed computing project

B. P. Abbott,¹ R. Abbott,¹ T. D. Abbott,² M. R. Abernathy,³ F. Acernese,^{4,5} K. Ackley,⁶ C. Adams,⁷ T. Adams,⁸ P. Addesso,⁹ R. X. Adhikari,¹ V. B. Adya,¹⁰ C. Affeldt,¹⁰ M. Agathos,¹¹ K. Agatsuma,¹¹ N. Aggarwal,¹² O. D. Aguiar,¹³ L. Aiello,^{14,15} A. Ain,¹⁶ P. Ajith,¹⁷ B. Allen,^{10,18,19} A. Allocca,^{20,21} P. A. Altin,²² S. B. Anderson,¹ W. G. Anderson,¹⁸ K. Arai,¹ M. C. Araya,¹ C. C. Arceneaux,²³ J. S. Areeda,²⁴ N. Arnaud,²⁵ K. G. Arun,²⁶ S. Ascenzi,^{27,15} G. Ashton,²⁸ M. Ast,²⁹ S. M. Aston,⁷ P. Astone,³⁰ P. Aufmuth,¹⁹ C. Aulbert,¹⁰ S. Babak,³¹ P. Bacon,³² M. K. M. Bader,¹¹ P. T. Baker,³³ F. Baldaccini,^{34,35} G. Ballardin,³⁶ S. W. Ballmer,³⁷ J. C. Barayoga,¹ S. E. Barclay,³⁸ B. C. Barish,¹ D. Barker,³⁹ F. Barone,^{4,5} B. Barr,³⁸ L. Barsotti,¹² M. Barsuglia,³² D. Barta,⁴⁰ J. Bartlett,³⁹ I. Bartos,⁴¹ R. Bassiri,⁴² A. Basti,^{20,21} J. C. Batch,³⁹ C. Baune,¹⁰ V. Bavigadda,³⁶ M. Bazzan,^{43,44} M. Bejger,⁴⁵ A. S. Bell,³⁸ B. K. Berger,¹ G. Bergmann,¹⁰ C. P. L. Berry,⁴⁶ D. Bersanetti,^{47,48} A. Bertolini,¹¹ J. Betzwieser,⁷ S. Bhagwat,³⁷ R. Bhandare,⁴⁹ I. A. Bilenko,⁵⁰ G. Billingsley,¹ J. Birch,⁷ R. Birney,⁵¹ S. Biscans,¹² A. Bisht,^{10,19} M. Bitossi,³⁶ C. Biwer,³⁷ M. A. Bizouard,²⁵ J. K. Blackburn,¹ C. D. Blair,⁵² D. G. Blair,⁵² R. M. Blair,³⁹ S. Bloemen,⁵³ O. Bock,¹⁰ M. Boer,⁵⁴ G. Bogaert,⁵⁴ C. Bogan,¹⁰ A. Bohe,³¹ C. Bond,⁴⁶ F. Bondu,⁵⁵ R. Bonnand,⁸ B. A. Boom,¹¹ R. Bork,¹ V. Boschi,^{20,21} S. Bose,^{56,16} Y. Bouffanais,³² A. Bozzi,³⁶ C. Bradaschia,²¹ P. R. Brady,¹⁸ V. B. Braginsky*,⁵⁰ M. Branchesi,^{57,58} J. E. Brau,⁵⁹ T. Briant,⁶⁰ A. Brillet,⁵⁴ M. Brinkmann,¹⁰ V. Brisson,²⁵ P. Brockill,¹⁸ J. E. Broida,⁶¹ A. F. Brooks,¹ D. A. Brown,³⁷ D. D. Brown,⁴⁶ N. M. Brown,¹² S. Brunett,¹ C. C. Buchanan,² A. Buikema,¹² T. Bulik,⁶² H. J. Bulten,^{63,11} A. Buonanno,^{31,64} D. Buskalic,⁸ C. Buy,³² R. L. Byer,⁴² M. Cabero,¹⁰ L. Cadonati,⁶⁵ G. Cagnoli,^{66,67} C. Cahillane,¹ J. Calderón Bustillo,⁶⁵ T. Callister,¹ E. Calloni,^{68,5} J. B. Camp,⁶⁹ K. C. Cannon,⁷⁰ J. Cao,⁷¹ C. D. Capano,¹⁰ E. Capocasa,³² F. Carbognani,³⁶ S. Caride,⁷² J. Casanueva Diaz,²⁵ C. Casentini,^{27,15} S. Caudill,¹⁸ M. Cavaglià,²³ F. Cavalier,²⁵ R. Cavalieri,³⁶ G. Cella,²¹ C. B. Cepeda,¹ L. Cerboni Baiardi,^{57,58} G. Cerretani,^{20,21} E. Cesarini,^{27,15} S. J. Chamberlin,⁷³ M. Chan,³⁸ S. Chao,⁷⁴ P. Charlton,⁷⁵ E. Chassande-Mottin,³² B. D. Cheeseboro,⁷⁶ H. Y. Chen,⁷⁷ Y. Chen,⁷⁸ C. Cheng,⁷⁴ A. Chincarini,⁴⁸ A. Chiummo,³⁶ H. S. Cho,⁷⁹ M. Cho,⁶⁴ J. H. Chow,²² N. Christensen,⁶¹ Q. Chu,⁵² S. Chua,⁶⁰ S. Chung,⁵² G. Ciani,⁶ F. Clara,³⁹ J. A. Clark,⁶⁵ F. Cleva,⁵⁴ E. Coccia,^{27,14} P.-F. Cohadon,⁶⁰ A. Colla,^{80,30} C. G. Collette,⁸¹ L. Cominsky,⁸² M. Constancio Jr.,¹³ A. Conte,^{80,30} L. Conti,⁴⁴ D. Cook,³⁹ T. R. Corbitt,² N. Cornish,³³ A. Corsi,⁷² S. Cortese,³⁶ C. A. Costa,¹³ M. W. Coughlin,⁶¹ S. B. Coughlin,⁸³ J.-P. Coulon,⁵⁴ S. T. Countryman,⁴¹ P. Couvares,¹ E. E. Cowan,⁶⁵ D. M. Coward,⁵² M. J. Cowart,⁷ D. C. Coyne,¹ R. Coyne,⁷² K. Craig,³⁸ J. D. E. Creighton,¹⁸ T. D. Creighton,⁸⁸ J. Cripe,² S. G. Crowder,⁸⁴ A. Cumming,³⁸ L. Cunningham,³⁸ E. Cuoco,³⁶ T. Dal Canton,¹⁰ S. L. Danilishin,³⁸ S. D'Antonio,¹⁵ K. Danzmann,^{19,10} N. S. Darman,⁸⁵ A. Dasgupta,⁸⁶ C. F. Da Silva Costa,⁶ V. Dattilo,³⁶ I. Dave,⁴⁹ M. Davier,²⁵ G. S. Davies,³⁸ E. J. Daw,⁸⁷ R. Day,³⁶ S. De,³⁷ D. DeBra,⁴² G. Debreczeni,⁴⁰ J. Degallaix,⁶⁶ M. De Laurentis,^{68,5} S. Deléglise,⁶⁰ W. Del Pozzo,⁴⁶ T. Denker,¹⁰ T. Dent,¹⁰ V. Dergachev,¹ R. De Rosa,^{68,5} R. T. DeRosa,⁷ R. DeSalvo,⁹ R. C. Devine,⁷⁶ S. Dhurandhar,¹⁶ M. C. Díaz,⁸⁸ L. Di Fiore,⁵ M. Di Giovanni,^{89,90} T. Di Girolamo,^{68,5} A. Di Lieto,^{20,21} S. Di Pace,^{80,30} I. Di Palma,^{31,80,30} A. Di Virgilio,²¹ V. Dolique,⁶⁶ F. Donovan,¹² K. L. Dooley,²³ S. Doravari,¹⁰ R. Douglas,³⁸ T. P. Downes,¹⁸ M. Drago,¹⁰ R. W. P. Drever,¹ J. C. Driggers,³⁹ M. Ducrot,⁸ S. E. Dwyer,³⁹ T. B. Edo,⁸⁷ M. C. Edwards,⁶¹ A. Effler,⁷ H.-B. Eggenstein,¹⁰ P. Ehrens,¹ J. Eichholz,^{6,1} S. S. Eikenberry,⁶ W. Engels,⁷⁸ R. C. Essick,¹² T. Etzel,¹ M. Evans,¹² T. M. Evans,⁷ R. Everett,⁷³ M. Factourovich,⁴¹ V. Fafone,^{27,15} H. Fair,³⁷ S. Fairhurst,⁹¹ X. Fan,⁷¹ Q. Fang,⁵² S. Farinon,⁴⁸ B. Farr,⁷⁷ W. M. Farr,⁴⁶ M. Favata,⁹² M. Fays,⁹¹ H. Fehrmann,¹⁰ M. M. Fejer,⁴² E. Fenyvesi,⁹³ I. Ferrante,^{20,21} E. C. Ferreira,¹³ F. Ferrini,³⁶ F. Fidecaro,^{20,21} I. Fiori,³⁶ D. Fiorucci,³² R. P. Fisher,³⁷ R. Flamini,^{66,94} M. Fletcher,³⁸ J.-D. Fournier,⁵⁴ S. Frasca,^{80,30} F. Frasconi,²¹ Z. Frei,⁹³ A. Freise,⁴⁶ R. Frey,⁵⁹ V. Frey,²⁵ P. Fritschel,¹² V. V. Frolov,⁷ P. Fulda,⁶ M. Fyffe,⁷ H. A. G. Gabbard,²³ J. R. Gair,⁹⁵ L. Gammaitoni,³⁴ S. G. Gaonkar,¹⁶ F. Garufi,^{68,5} G. Gaur,^{96,86} N. Gehrels,⁶⁹ G. Gemme,⁴⁸ P. Geng,⁸⁸ E. Genin,³⁶ A. Gennai,²¹ J. George,⁴⁹ L. Gergely,⁹⁷ V. Germain,⁸ Abhirup Ghosh,¹⁷ Archisman Ghosh,¹⁷ S. Ghosh,^{53,11} J. A. Giaime,^{2,7} K. D. Giardina,⁷ A. Giazotto,²¹ K. Gill,⁹⁸ A. Glaefke,³⁸ E. Goetz,³⁹ R. Goetz,⁶ L. Gondan,⁹³ G. González,² J. M. Gonzalez Castro,^{20,21} A. Gopakumar,⁹⁹ N. A. Gordon,³⁸ M. L. Gorodetsky,⁵⁰ S. E. Gossan,¹ M. Gosselin,³⁶ R. Gouaty,⁸ A. Grado,^{100,5} C. Graef,³⁸ P. B. Graff,⁶⁴ M. Granata,⁶⁶ A. Grant,³⁸ S. Gras,¹² C. Gray,³⁹ G. Greco,^{57,58} A. C. Green,⁴⁶ P. Groot,⁵³ H. Grote,¹⁰ S. Grunewald,³¹ G. M. Guidi,^{57,58} X. Guo,⁷¹ A. Gupta,¹⁶ M. K. Gupta,⁸⁶ K. E. Gushwa,¹ E. K. Gustafson,¹ R. Gustafson,¹⁰¹ J. J. Hacker,²⁴ B. R. Hall,⁵⁶ E. D. Hall,¹ G. Hammond,³⁸ M. Haney,⁹⁹ M. M. Hanke,¹⁰ J. Hanks,³⁹ C. Hanna,⁷³ M. D. Hannam,⁹¹ J. Hanson,⁷ T. Hardwick,² J. Harms,^{57,58} G. M. Harry,³ I. W. Harry,³¹ M. J. Hart,³⁸ M. T. Hartman,⁶ C.-J. Haster,⁴⁶ K. Haughian,³⁸ A. Heidmann,⁶⁰

M. C. Heintze,⁷ H. Heitmann,⁵⁴ P. Hello,²⁵ G. Hemming,³⁶ M. Hendry,³⁸ I. S. Heng,³⁸ J. Hennig,³⁸ J. Henry,¹⁰²
 A. W. Heptonstall,¹ M. Heurs,^{10,19} S. Hild,³⁸ D. Hoak,³⁶ D. Hofman,⁶⁶ K. Holt,⁷ D. E. Holz,⁷⁷ P. Hopkins,⁹¹
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 K. Kawabe,³⁹ F. Kéfélian,⁵⁴ M. S. Kehl,¹⁰⁸ D. Keitel,¹⁰⁴ D. B. Kelley,³⁷ W. Kells,¹ R. Kennedy,⁸⁷ J. S. Key,⁸⁸
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 Chunglee Kim,⁷⁹ J. Kim,¹¹⁰ K. Kim,¹¹¹ N. Kim,⁴² W. Kim,¹¹² Y.-M. Kim,¹¹⁰ S. J. Kimbrell,⁶⁵ E. J. King,¹¹²
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 P. Leaci,^{80,30} S. Leavey,³⁸ E. O. Lebigot,^{32,71} C. H. Lee,¹¹⁰ H. K. Lee,¹¹¹ H. M. Lee,¹¹⁶ K. Lee,³⁸ A. Lenon,³⁷
 M. Leonardi,^{89,90} J. R. Leong,¹⁰ N. Leroy,²⁵ N. Letendre,⁸ Y. Levin,¹¹⁵ J. B. Lewis,¹ T. G. F. Li,¹¹⁷ A. Libson,¹²
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 A. S. Markosyan,⁴² E. Maros,¹ F. Martelli,^{57,58} L. Martellini,⁵⁴ I. W. Martin,³⁸ D. V. Martynov,¹² J. N. Marx,¹
 K. Mason,¹² A. Masserot,⁸ T. J. Massinger,³⁷ M. Masso-Reid,³⁸ S. Mastrogiovanni,^{80,30} F. Matichard,¹²
 L. Matone,⁴¹ N. Mavalvala,¹² N. Mazumder,⁵⁶ R. McCarthy,³⁹ D. E. McClelland,²² S. McCormick,⁷
 S. C. McGuire,¹²² G. McIntyre,¹ J. McIver,¹ D. J. McManus,²² T. McRae,²² S. T. McWilliams,⁷⁶ D. Meacher,⁷³
 G. D. Meadors,^{31,10} J. Meidam,¹¹ A. Melatos,⁸⁵ G. Mendell,³⁹ R. A. Mercer,¹⁸ E. L. Merilh,³⁹ M. Merzougui,⁵⁴
 S. Meshkov,¹ C. Messenger,³⁸ C. Messick,⁷³ R. Metzдорff,⁶⁰ P. M. Meyers,⁸⁴ F. Mezzani,^{30,80} H. Miao,⁴⁶
 C. Michel,⁶⁶ H. Middleton,⁴⁶ E. E. Mikhailov,¹²³ L. Milano,^{68,5} A. L. Miller,^{6,80,30} A. Miller,⁸³ B. B. Miller,⁸³
 J. Miller,¹² M. Millhouse,³³ Y. Minenkov,¹⁵ J. Ming,³¹ S. Mirshekari,¹²⁴ C. Mishra,¹⁷ S. Mitra,¹⁶ V. P. Mitrofanov,⁵⁰
 G. Mitselmakher,⁶ R. Mittleman,¹² A. Moggi,²¹ M. Mohan,³⁶ S. R. P. Mohapatra,¹² M. Montani,^{57,58} B. C. Moore,⁹²
 C. J. Moore,¹²⁵ D. Moraru,³⁹ G. Moreno,³⁹ S. R. Morris,⁸⁸ K. Mossavi,¹⁰ B. Mours,⁸ C. M. Mow-Lowry,⁴⁶
 G. Mueller,⁶ A. W. Muir,⁹¹ Arunava Mukherjee,¹⁷ D. Mukherjee,¹⁸ S. Mukherjee,⁸⁸ N. Mukund,¹⁶ A. Mullavey,⁷
 J. Munch,¹¹² D. J. Murphy,⁴¹ P. G. Murray,³⁸ A. Mytidis,⁶ I. Nardecchia,^{27,15} L. Naticchioni,^{80,30} R. K. Nayak,¹²⁶
 K. Nedkova,¹¹⁹ G. Nelemans,^{53,11} T. J. N. Nelson,⁷ M. Neri,^{47,48} A. Neunzert,¹⁰¹ G. Newton,³⁸ T. T. Nguyen,²²
 A. B. Nielsen,¹⁰ S. Nissanke,^{53,11} A. Nitz,¹⁰ F. Nocera,³⁶ D. Nolting,⁷ M. E. N. Normandin,⁸⁸ L. K. Nuttall,³⁷
 J. Oberling,³⁹ E. Ochsner,¹⁸ J. O'Dell,¹²⁷ E. Oelker,¹² G. H. Ogini,¹²⁸ J. J. Oh,¹²⁹ S. H. Oh,¹²⁹ F. Ohme,⁹¹
 M. Oliver,¹⁰⁴ P. Oppermann,¹⁰ Richard J. Oram,⁷ B. O'Reilly,⁷ R. O'Shaughnessy,¹⁰² D. J. Ottaway,¹¹²
 H. Overmier,⁷ B. J. Owen,⁷² A. Pai,¹⁰⁷ S. A. Pai,⁴⁹ J. R. Palamos,⁵⁹ O. Palashov,¹⁰⁹ C. Palomba,³⁰ A. Pal-Singh,²⁹
 H. Pan,⁷⁴ C. Pankow,⁸³ F. Pannarale,⁹¹ B. C. Pant,⁴⁹ F. Paoletti,^{36,21} A. Paoli,³⁶ M. A. Papa,^{31,18,10} H. R. Paris,⁴²
 W. Parker,⁷ D. Pascucci,³⁸ A. Pasqualetti,³⁶ R. Passaquieti,^{20,21} D. Passuello,²¹ B. Patricelli,^{20,21} Z. Patrick,⁴²
 B. L. Pearlstone,³⁸ M. Pedraza,¹ R. Pedurand,^{66,130} L. Pekowsky,³⁷ A. Pele,⁷ S. Penn,¹³¹ A. Perreca,¹ L. M. Perri,⁸³
 M. Phelps,³⁸ O. J. Piccini,^{80,30} M. Pichot,⁵⁴ F. Piergiovanni,^{57,58} V. Pierro,⁹ G. Pillant,³⁶ L. Pinard,⁶⁶
 I. M. Pinto,⁹ M. Pitkin,³⁸ M. Poe,¹⁸ R. Poggiani,^{20,21} P. Popolizio,³⁶ A. Post,¹⁰ J. Powell,³⁸ J. Prasad,¹⁶
 V. Predoi,⁹¹ T. Prestegard,⁸⁴ L. R. Price,¹ M. Prijatelj,^{10,36} M. Principe,⁹ S. Privitera,³¹ R. Prix,¹⁰
 G. A. Prodi,^{89,90} L. Prokhorov,⁵⁰ O. Puncken,¹⁰ M. Punturo,³⁵ P. Puppo,³⁰ M. Pürner,³¹ H. Qi,¹⁸ J. Qin,⁵²
 S. Qiu,¹¹⁵ V. Quetschke,⁸⁸ E. A. Quintero,¹ R. Quitzow-James,⁵⁹ F. J. Raab,³⁹ D. S. Rabeling,²² H. Radkins,³⁹
 P. Raffai,⁹³ S. Raja,⁴⁹ C. Rajan,⁴⁹ M. Rakhmanov,⁸⁸ P. Rapagnani,^{80,30} V. Raymond,³¹ M. Razzano,^{20,21} V. Re,²⁷
 J. Read,²⁴ C. M. Reed,³⁹ T. Regimbau,⁵⁴ L. Rei,⁴⁸ S. Reid,⁵¹ D. H. Reitze,^{1,6} H. Rew,¹²³ S. D. Reyes,³⁷
 F. Ricci,^{80,30} K. Riles,¹⁰¹ M. Rizzo,¹⁰² N. A. Robertson,^{1,38} R. Robie,³⁸ F. Robinet,²⁵ A. Rocchi,¹⁵ L. Rolland,⁸
 J. G. Rollins,¹ V. J. Roma,⁵⁹ J. D. Romano,⁸⁸ R. Romano,^{4,5} G. Romanov,¹²³ J. H. Romie,⁷ D. Rosińska,^{132,45}
 S. Rowan,³⁸ A. Rüdiger,¹⁰ P. Ruggi,³⁶ K. Ryan,³⁹ S. Sachdev,¹ T. Sadecki,³⁹ L. Sadeghian,¹⁸ M. Sakellariadou,¹³³
 L. Salconi,³⁶ M. Saleem,¹⁰⁷ F. Salemi,¹⁰ A. Samajdar,¹²⁶ L. Sammut,¹¹⁵ E. J. Sanchez,¹ V. Sandberg,³⁹

B. Sandeen,⁸³ J. R. Sanders,³⁷ B. Sassolas,⁶⁶ B. S. Sathyaprakash,⁹¹ P. R. Saulson,³⁷ O. E. S. Sauter,¹⁰¹ R. L. Savage,³⁹ A. Sawadsky,¹⁹ P. Schale,⁵⁹ R. Schilling[†],¹⁰ J. Schmidt,¹⁰ P. Schmidt,^{1,78} R. Schnabel,²⁹ R. M. S. Schofield,⁵⁹ A. Schönbeck,²⁹ E. Schreiber,¹⁰ D. Schuette,^{10,19} B. F. Schutz,^{91,31} J. Scott,³⁸ S. M. Scott,²² D. Sellers,⁷ A. S. Sengupta,⁹⁶ D. Sentenac,³⁶ V. Sequino,^{27,15} A. Sergeev,¹⁰⁹ Y. Setyawati,^{53,11} D. A. Shaddock,²² T. Shaffer,³⁹ M. S. Shahrari,⁸³ M. Shaltev,¹⁰ B. Shapiro,⁴² P. Shawhan,⁶⁴ A. Sheperd,¹⁸ D. H. Shoemaker,¹² D. M. Shoemaker,⁶⁵ K. Siellez,⁶⁵ X. Siemens,¹⁸ M. Sieniawska,⁴⁵ D. Sigg,³⁹ A. D. Silva,¹³ A. Singer,¹ L. P. Singer,⁶⁹ A. Singh,^{31,10,19} R. Singh,² A. Singhal,¹⁴ A. M. Sintès,¹⁰⁴ B. J. J. Slagmolen,²² J. R. Smith,²⁴ N. D. Smith,¹ R. J. E. Smith,¹ E. J. Son,¹²⁹ B. Sorazu,³⁸ F. Sorrentino,⁴⁸ T. Souradeep,¹⁶ A. K. Srivastava,⁸⁶ A. Staley,⁴¹ M. Steinke,¹⁰ J. Steinlechner,³⁸ S. Steinlechner,³⁸ D. Steinmeyer,^{10,19} B. C. Stephens,¹⁸ R. Stone,⁸⁸ K. A. Strain,³⁸ N. Straniero,⁶⁶ G. Stratta,^{57,58} N. A. Strauss,⁶¹ S. Strigin,⁵⁰ R. Sturani,¹²⁴ A. L. Stuver,⁷ T. Z. Summerscales,¹³⁴ L. Sun,⁸⁵ S. Sunil,⁸⁶ P. J. Sutton,⁹¹ B. L. Swinkels,³⁶ M. J. Szczepańczyk,⁹⁸ M. Tacca,³² D. Talukder,⁵⁹ D. B. Tanner,⁶ M. Tápai,⁹⁷ S. P. Tarabrin,¹⁰ A. Taracchini,³¹ R. Taylor,¹ T. Theeg,¹⁰ M. P. Thirugnanasambandam,¹ E. G. Thomas,⁴⁶ M. Thomas,⁷ P. Thomas,³⁹ K. A. Thorne,⁷ E. Thrane,¹¹⁵ S. Tiwari,^{14,90} V. Tiwari,⁹¹ K. V. Tokmakov,¹⁰⁶ K. Toland,³⁸ C. Tomlinson,⁸⁷ M. Tonelli,^{20,21} Z. Tornasi,³⁸ C. V. Torres[‡],⁸⁸ C. I. Torrie,¹ D. Töyrä,⁴⁶ F. Travasso,^{34,35} G. Traylor,⁷ D. Trifirò,²³ M. C. Tringali,^{89,90} L. Trozzo,^{135,21} M. Tse,¹² M. Turconi,⁵⁴ D. Tuyenbayev,⁸⁸ D. Ugolini,¹³⁶ C. S. Unnikrishnan,⁹⁹ A. L. Urban,¹⁸ S. A. Usman,³⁷ H. Vahlbruch,¹⁹ G. Vajente,¹ G. Valdes,⁸⁸ N. van Bakel,¹¹ M. van Beuzekom,¹¹ J. F. J. van den Brand,^{63,11} C. Van Den Broeck,¹¹ D. C. Vander-Hyde,³⁷ L. van der Schaaf,¹¹ J. V. van Heijningen,¹¹ A. A. van Veggel,³⁸ M. Vardaro,^{43,44} S. Vass,¹ M. Vasúth,⁴⁰ R. Vaulin,¹² A. Vecchio,⁴⁶ G. Vedovato,⁴⁴ J. Veitch,⁴⁶ P. J. Veitch,¹¹² K. Venkateswara,¹³⁷ D. Verkindt,⁸ F. Vetrano,^{57,58} A. Viceré,^{57,58} S. Vinciguerra,⁴⁶ D. J. Vine,⁵¹ J.-Y. Vinet,⁵⁴ S. Vitale,¹² T. Vo,³⁷ H. Vocca,^{34,35} C. Vorvick,³⁹ D. V. Voss,⁶ W. D. Voudsen,⁴⁶ S. P. Vyatchanin,⁵⁰ A. R. Wade,²² L. E. Wade,¹³⁸ M. Wade,¹³⁸ M. Walker,² L. Wallace,¹ S. Walsh,^{31,10} G. Wang,^{14,58} H. Wang,⁴⁶ M. Wang,⁴⁶ X. Wang,⁷¹ Y. Wang,⁵² R. L. Ward,²² J. Warner,³⁹ M. Was,⁸ B. Weaver,³⁹ L.-W. Wei,⁵⁴ M. Weinert,¹⁰ A. J. Weinstein,¹ R. Weiss,¹² L. Wen,⁵² P. Weßels,¹⁰ T. Westphal,¹⁰ K. Wette,¹⁰ J. T. Whelan,¹⁰² B. F. Whiting,⁶ R. D. Williams,¹ A. R. Williamson,⁹¹ J. L. Willis,¹³⁹ B. Willke,^{19,10} M. H. Wimmer,^{10,19} W. Winkler,¹⁰ C. C. Wipf,¹ H. Wittel,^{10,19} G. Woan,³⁸ J. Woehler,¹⁰ J. Worden,³⁹ J. L. Wright,³⁸ D. S. Wu,¹⁰ G. Wu,⁷ J. Yablon,⁸³ W. Yam,¹² H. Yamamoto,¹ C. C. Yancey,⁶⁴ H. Yu,¹² M. Yvert,⁸ A. Zadrożny,¹¹³ L. Zangrando,⁴⁴ M. Zanolin,⁹⁸ J.-P. Zendri,⁴⁴ M. Zevin,⁸³ L. Zhang,¹ M. Zhang,¹²³ Y. Zhang,¹⁰² C. Zhao,⁵² M. Zhou,⁸³ Z. Zhou,⁸³ S. Zhu,^{31,10} X. J. Zhu,⁵² M. E. Zucker,^{1,12} S. E. Zuraw,¹¹⁹ and J. Zweigig¹

(LIGO Scientific Collaboration and Virgo Collaboration)

*Deceased, March 2016. †Deceased, May 2015. ‡Deceased, March 2015.

¹LIGO, California Institute of Technology, Pasadena, CA 91125, USA

²Louisiana State University, Baton Rouge, LA 70803, USA

³American University, Washington, D.C. 20016, USA

⁴Università di Salerno, Fisciano, I-84084 Salerno, Italy

⁵INFN, Sezione di Napoli, Complesso Universitario di Monte S. Angelo, I-80126 Napoli, Italy

⁶University of Florida, Gainesville, FL 32611, USA

⁷LIGO Livingston Observatory, Livingston, LA 70754, USA

⁸Laboratoire d'Annecy-le-Vieux de Physique des Particules (LAPP), Université Savoie Mont Blanc, CNRS/IN2P3, F-74941 Annecy-le-Vieux, France

⁹University of Sannio at Benevento, I-82100 Benevento, Italy and INFN, Sezione di Napoli, I-80100 Napoli, Italy

¹⁰Albert-Einstein-Institut, Max-Planck-Institut für Gravitationsphysik, D-30167 Hannover, Germany

¹¹Nikhef, Science Park, 1098 XG Amsterdam, The Netherlands

¹²LIGO, Massachusetts Institute of Technology, Cambridge, MA 02139, USA

¹³Instituto Nacional de Pesquisas Espaciais, 12227-010 São José dos Campos, São Paulo, Brazil

¹⁴INFN, Gran Sasso Science Institute, I-67100 L'Aquila, Italy

¹⁵INFN, Sezione di Roma Tor Vergata, I-00133 Roma, Italy

¹⁶Inter-University Centre for Astronomy and Astrophysics, Pune 411007, India

¹⁷International Centre for Theoretical Sciences, Tata Institute of Fundamental Research, Bangalore 560012, India

¹⁸University of Wisconsin-Milwaukee, Milwaukee, WI 53201, USA

¹⁹Leibniz Universität Hannover, D-30167 Hannover, Germany

²⁰Università di Pisa, I-56127 Pisa, Italy

²¹INFN, Sezione di Pisa, I-56127 Pisa, Italy

²²Australian National University, Canberra, Australian Capital Territory 0200, Australia

²³The University of Mississippi, University, MS 38677, USA

- ²⁴ *California State University Fullerton, Fullerton, CA 92831, USA*
- ²⁵ *LAL, Univ. Paris-Sud, CNRS/IN2P3, Université Paris-Saclay, Orsay, France*
- ²⁶ *Chennai Mathematical Institute, Chennai 603103, India*
- ²⁷ *Università di Roma Tor Vergata, I-00133 Roma, Italy*
- ²⁸ *University of Southampton, Southampton SO17 1BJ, United Kingdom*
- ²⁹ *Universität Hamburg, D-22761 Hamburg, Germany*
- ³⁰ *INFN, Sezione di Roma, I-00185 Roma, Italy*
- ³¹ *Albert-Einstein-Institut, Max-Planck-Institut für Gravitationsphysik, D-14476 Potsdam-Golm, Germany*
- ³² *APC, AstroParticule et Cosmologie, Université Paris Diderot, CNRS/IN2P3, CEA/Irfu, Observatoire de Paris, Sorbonne Paris Cité, F-75205 Paris Cedex 13, France*
- ³³ *Montana State University, Bozeman, MT 59717, USA*
- ³⁴ *Università di Perugia, I-06123 Perugia, Italy*
- ³⁵ *INFN, Sezione di Perugia, I-06123 Perugia, Italy*
- ³⁶ *European Gravitational Observatory (EGO), I-56021 Cascina, Pisa, Italy*
- ³⁷ *Syracuse University, Syracuse, NY 13244, USA*
- ³⁸ *SUPA, University of Glasgow, Glasgow G12 8QQ, United Kingdom*
- ³⁹ *LIGO Hanford Observatory, Richland, WA 99352, USA*
- ⁴⁰ *Wigner RCP, RMKI, H-1121 Budapest, Konkoly Thege Miklós út 29-33, Hungary*
- ⁴¹ *Columbia University, New York, NY 10027, USA*
- ⁴² *Stanford University, Stanford, CA 94305, USA*
- ⁴³ *Università di Padova, Dipartimento di Fisica e Astronomia, I-35131 Padova, Italy*
- ⁴⁴ *INFN, Sezione di Padova, I-35131 Padova, Italy*
- ⁴⁵ *CAMK-PAN, 00-716 Warsaw, Poland*
- ⁴⁶ *University of Birmingham, Birmingham B15 2TT, United Kingdom*
- ⁴⁷ *Università degli Studi di Genova, I-16146 Genova, Italy*
- ⁴⁸ *INFN, Sezione di Genova, I-16146 Genova, Italy*
- ⁴⁹ *RRCAT, Indore MP 452013, India*
- ⁵⁰ *Faculty of Physics, Lomonosov Moscow State University, Moscow 119991, Russia*
- ⁵¹ *SUPA, University of the West of Scotland, Paisley PA1 2BE, United Kingdom*
- ⁵² *University of Western Australia, Crawley, Western Australia 6009, Australia*
- ⁵³ *Department of Astrophysics/IMAPP, Radboud University Nijmegen, P.O. Box 9010, 6500 GL Nijmegen, The Netherlands*
- ⁵⁴ *Artemis, Université Côte d'Azur, CNRS, Observatoire Côte d'Azur, CS 34229, Nice cedex 4, France*
- ⁵⁵ *Institut de Physique de Rennes, CNRS, Université de Rennes 1, F-35042 Rennes, France*
- ⁵⁶ *Washington State University, Pullman, WA 99164, USA*
- ⁵⁷ *Università degli Studi di Urbino "Carlo Bo," I-61029 Urbino, Italy*
- ⁵⁸ *INFN, Sezione di Firenze, I-50019 Sesto Fiorentino, Firenze, Italy*
- ⁵⁹ *University of Oregon, Eugene, OR 97403, USA*
- ⁶⁰ *Laboratoire Kastler Brossel, UPMC-Sorbonne Universités, CNRS, ENS-PSL Research University, Collège de France, F-75005 Paris, France*
- ⁶¹ *Carleton College, Northfield, MN 55057, USA*
- ⁶² *Astronomical Observatory Warsaw University, 00-478 Warsaw, Poland*
- ⁶³ *VU University Amsterdam, 1081 HV Amsterdam, The Netherlands*
- ⁶⁴ *University of Maryland, College Park, MD 20742, USA*
- ⁶⁵ *Center for Relativistic Astrophysics and School of Physics, Georgia Institute of Technology, Atlanta, GA 30332, USA*
- ⁶⁶ *Laboratoire des Matériaux Avancés (LMA), CNRS/IN2P3, F-69622 Villeurbanne, France*
- ⁶⁷ *Université Claude Bernard Lyon 1, F-69622 Villeurbanne, France*
- ⁶⁸ *Università di Napoli "Federico II," Complesso Universitario di Monte S. Angelo, I-80126 Napoli, Italy*
- ⁶⁹ *NASA/Goddard Space Flight Center, Greenbelt, MD 20771, USA*
- ⁷⁰ *RESCEU, University of Tokyo, Tokyo, 113-0033, Japan.*
- ⁷¹ *Tsinghua University, Beijing 100084, China*
- ⁷² *Texas Tech University, Lubbock, TX 79409, USA*
- ⁷³ *The Pennsylvania State University, University Park, PA 16802, USA*
- ⁷⁴ *National Tsing Hua University, Hsinchu City, 30013 Taiwan, Republic of China*
- ⁷⁵ *Charles Sturt University, Wagga Wagga, New South Wales 2678, Australia*
- ⁷⁶ *West Virginia University, Morgantown, WV 26506, USA*
- ⁷⁷ *University of Chicago, Chicago, IL 60637, USA*
- ⁷⁸ *Caltech CaRT, Pasadena, CA 91125, USA*
- ⁷⁹ *Korea Institute of Science and Technology Information, Daejeon 305-806, Korea*
- ⁸⁰ *Università di Roma "La Sapienza," I-00185 Roma, Italy*
- ⁸¹ *University of Brussels, Brussels 1050, Belgium*
- ⁸² *Sonoma State University, Rohnert Park, CA 94928, USA*

- ⁸³Center for Interdisciplinary Exploration & Research in Astrophysics (CIERA),
Northwestern University, Evanston, IL 60208, USA
- ⁸⁴University of Minnesota, Minneapolis, MN 55455, USA
- ⁸⁵The University of Melbourne, Parkville, Victoria 3010, Australia
- ⁸⁶Institute for Plasma Research, Bhat, Gandhinagar 382428, India
- ⁸⁷The University of Sheffield, Sheffield S10 2TN, United Kingdom
- ⁸⁸The University of Texas Rio Grande Valley, Brownsville, TX 78520, USA
- ⁸⁹Università di Trento, Dipartimento di Fisica, I-38123 Povo, Trento, Italy
- ⁹⁰INFN, Trento Institute for Fundamental Physics and Applications, I-38123 Povo, Trento, Italy
- ⁹¹Cardiff University, Cardiff CF24 3AA, United Kingdom
- ⁹²Montclair State University, Montclair, NJ 07043, USA
- ⁹³MTA Eötvös University, “Lendulet” Astrophysics Research Group, Budapest 1117, Hungary
- ⁹⁴National Astronomical Observatory of Japan, 2-21-1 Osawa, Mitaka, Tokyo 181-8588, Japan
- ⁹⁵School of Mathematics, University of Edinburgh, Edinburgh EH9 3FD, United Kingdom
- ⁹⁶Indian Institute of Technology, Gandhinagar Ahmedabad Gujarat 382424, India
- ⁹⁷University of Szeged, Dóm tér 9, Szeged 6720, Hungary
- ⁹⁸Embry-Riddle Aeronautical University, Prescott, AZ 86301, USA
- ⁹⁹Tata Institute of Fundamental Research, Mumbai 400005, India
- ¹⁰⁰INAF, Osservatorio Astronomico di Capodimonte, I-80131, Napoli, Italy
- ¹⁰¹University of Michigan, Ann Arbor, MI 48109, USA
- ¹⁰²Rochester Institute of Technology, Rochester, NY 14623, USA
- ¹⁰³NCSA, University of Illinois at Urbana-Champaign, Urbana, Illinois 61801, USA
- ¹⁰⁴Universitat de les Illes Balears, IAC3—IEEC, E-07122 Palma de Mallorca, Spain
- ¹⁰⁵University of Białystok, 15-424 Białystok, Poland
- ¹⁰⁶SUPA, University of Strathclyde, Glasgow G1 1XQ, United Kingdom
- ¹⁰⁷IISER-TVM, CET Campus, Trivandrum Kerala 695016, India
- ¹⁰⁸Canadian Institute for Theoretical Astrophysics,
University of Toronto, Toronto, Ontario M5S 3H8, Canada
- ¹⁰⁹Institute of Applied Physics, Nizhny Novgorod, 603950, Russia
- ¹¹⁰Pusan National University, Busan 609-735, Korea
- ¹¹¹Hanyang University, Seoul 133-791, Korea
- ¹¹²University of Adelaide, Adelaide, South Australia 5005, Australia
- ¹¹³NCBJ, 05-400 Świerk-Otwock, Poland
- ¹¹⁴IM-PAN, 00-956 Warsaw, Poland
- ¹¹⁵Monash University, Victoria 3800, Australia
- ¹¹⁶Seoul National University, Seoul 151-742, Korea
- ¹¹⁷The Chinese University of Hong Kong, Shatin, NT, Hong Kong SAR, China
- ¹¹⁸University of Alabama in Huntsville, Huntsville, AL 35899, USA
- ¹¹⁹University of Massachusetts-Amherst, Amherst, MA 01003, USA
- ¹²⁰ESPCI, CNRS, F-75005 Paris, France
- ¹²¹Università di Camerino, Dipartimento di Fisica, I-62032 Camerino, Italy
- ¹²²Southern University and A&M College, Baton Rouge, LA 70813, USA
- ¹²³College of William and Mary, Williamsburg, VA 23187, USA
- ¹²⁴Instituto de Física Teórica, University Estadual Paulista/ICTP South
American Institute for Fundamental Research, São Paulo SP 01140-070, Brazil
- ¹²⁵University of Cambridge, Cambridge CB2 1TN, United Kingdom
- ¹²⁶IISER-Kolkata, Mohanpur, West Bengal 741252, India
- ¹²⁷Rutherford Appleton Laboratory, HSIC, Chilton, Didcot, Oxon OX11 0QX, United Kingdom
- ¹²⁸Whitman College, 345 Boyer Avenue, Walla Walla, WA 99362 USA
- ¹²⁹National Institute for Mathematical Sciences, Daejeon 305-390, Korea
- ¹³⁰Université de Lyon, F-69361 Lyon, France
- ¹³¹Hobart and William Smith Colleges, Geneva, NY 14456, USA
- ¹³²Janusz Gil Institute of Astronomy, University of Zielona Góra, 65-265 Zielona Góra, Poland
- ¹³³King’s College London, University of London, London WC2R 2LS, United Kingdom
- ¹³⁴Andrews University, Berrien Springs, MI 49104, USA
- ¹³⁵Università di Siena, I-53100 Siena, Italy
- ¹³⁶Trinity University, San Antonio, TX 78212, USA
- ¹³⁷University of Washington, Seattle, WA 98195, USA
- ¹³⁸Kenyon College, Gambier, OH 43022, USA
- ¹³⁹Abilene Christian University, Abilene, TX 79699, USA

We report results of a deep all-sky search for periodic gravitational waves from isolated neutron stars in data from the S6 LIGO science run. The search was possible thanks to the computing power provided by the volunteers of the Einstein@Home distributed computing project. We find

no significant signal candidate and set the most stringent upper limits to date on the amplitude of gravitational wave signals from the target population. At the frequency of best strain sensitivity, between 170.5 and 171 Hz we set a 90% confidence upper limit of 5.5×10^{-25} , while at the high end of our frequency range, around 505 Hz, we achieve upper limits $\simeq 10^{-24}$. At 230 Hz we can exclude sources with ellipticities greater than 10^{-6} within 100 pc of Earth with fiducial value of the principal moment of inertia of 10^{38}kg m^2 . If we assume a higher (lower) gravitational wave spindown we constrain farther (closer) objects to higher (lower) ellipticities.

I. INTRODUCTION

In this paper we report the results of a deep all-sky Einstein@Home [1] search for continuous, nearly monochromatic gravitational waves (GWs) in data from LIGO’s sixth science (S6) run. A number of all-sky searches have been carried out on LIGO data, [2–11], of which [5, 7, 10] also ran on Einstein@Home. The search presented here covers frequencies from 50 Hz through 510 Hz and frequency derivatives from 3.39×10^{-10} Hz/s through -2.67×10^{-9} Hz/s. In this range we establish the most constraining gravitational wave amplitude upper limits to date for the target signal population.

II. LIGO INTERFEROMETERS AND THE DATA USED

The LIGO gravitational wave network consists of two observatories, one in Hanford (WA) and the other in Livingston (LA) separated by a 3000-km baseline [12]. The last science run (S6) [13] of this network before the upgrade towards the advanced LIGO configuration [14] took place between July 2009 and October 2010. The analysis in this paper uses a subset of this data: from GPS 949469977 (2010 Feb 6 05:39:22 UTC) through GPS 971529850 (2010 Oct 19 13:23:55 UTC), selected for good strain sensitivity [15]. Since interferometers sporadically fall out of operation (“lose lock”) due to environmental or instrumental disturbances or for scheduled maintenance periods, the data set is not contiguous and each detector has a duty factor of about 50% [16].

As done in [7], frequency bands known to contain spectral disturbances have been removed from the analysis. Actually, the data has been substituted with Gaussian noise with the same average power as that in the neighbouring and undisturbed bands. Table A 2 identifies these bands.

III. THE SEARCH

The search described in this paper targets nearly monochromatic gravitational wave signals as described for example by Eqs. 1-4 of [7]. Various emission mechanisms could generate such a signal as reviewed in Section IIA of [11]. In interpreting our results we will consider a spinning compact object with a fixed, non-axisymmetric mass quadrupole, described by an ellipticity ϵ .

We perform a stack-slide type of search using the GCT method [17, 18]. In a stack-slide search the data is partitioned in segments and each segment is searched with a matched-filter method [19]. The results from these coherent searches are combined by summing (stacking) the detection statistic values from the segments (sliding), one per segment (\mathcal{F}_i), and this determines the value of the core detection statistic:

$$\overline{\mathcal{F}} := \frac{1}{N_{\text{seg}}} \sum_{i=1}^{N_{\text{seg}}} \mathcal{F}_i. \quad (1)$$

There are different ways to combine the single-segment \mathcal{F}_i values, but independently of the way that this is done, this type of search is usually referred to as a “semi-coherent search”. So stack-slide searches are a type of semi-coherent search. Important variables for this type of search are: the coherent time baseline of the segments T_{coh} , the number of segments used N_{seg} , the total time spanned by the data T_{obs} , the grids in parameter space and the detection statistic used to rank the parameter space cells. For a stack-slide search in Gaussian noise, $N_{\text{seg}} \times 2\overline{\mathcal{F}}$ follows a $\chi^2_{4N_{\text{seg}}}$ chi-squared distribution with $4N_{\text{seg}}$ degrees of freedom. These parameters are summarised in Table I. The grids in frequency and spindown are each described by a single parameter, the grid spacing, which is constant over the search range. The same frequency grid spacings are used for the coherent searches over the segments and for the incoherent summing. The spindown spacing for the incoherent summing, $\delta\dot{f}$, is finer than that used for the coherent searches, $\delta\dot{f}_c$, by a factor γ . The notation used here is consistent with that used in previous observational papers [20] and in the GCT methods papers cited above.

The sky grid is the union of two grids: one is uniform over the projection of the celestial sphere onto the equatorial plane, and the tiling (in the equatorial plane) is approximately square with sides of length

$$d(m_{\text{sky}}) = \frac{1}{f} \frac{\sqrt{m_{\text{sky}}}}{\pi\tau_E}, \quad (2)$$

with $m_{\text{sky}} = 0.3$ and $\tau_E \simeq 0.021$ s being half of the light travel time across the Earth. As was done in [7], the sky-grids are constant over 10 Hz bands and the spacings are the ones associated through Eq. 2 to the highest frequency f in the range. The other grid is limited to the equatorial region ($0 \leq \alpha \leq 2\pi$ and $-0.5 \leq \delta \leq 0.5$), with constant right ascension α and declination δ spacings equal to $d(0.3)$ – see Fig.1. The reason for the equatorial “patching” with a denser sky grid is to improve the

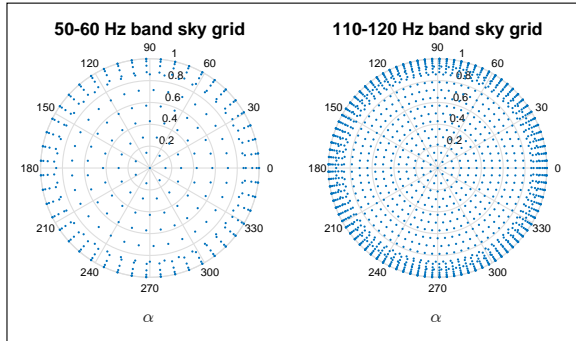


FIG. 1. Polar plots (r, θ plots with $\theta = \alpha$ and $r = \cos \delta$) of the grid points in the northern equatorial hemisphere sky for the band 50-60Hz (left panel) and for the band 110-120Hz (right panel). α is the right ascension coordinate and δ the declination coordinate. One can clearly see the higher density in the $-0.5 \leq \delta \leq 0.5$ equatorial region and the higher density ($\propto f^2$) of grid points at higher frequencies. The southern hemispheres looks practically identical to the respective northern ones.

sensitivity of the search: the sky resolution actually depends on the ecliptic latitude and the uniform equatorial grid under-resolves particularly in the equatorial region. The resulting number of templates used to search 50-mHz bands as a function of frequency is shown in Fig. 2.

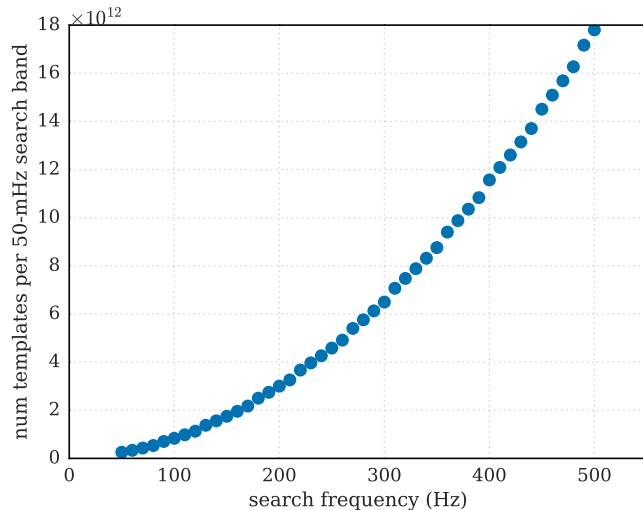


FIG. 2. Number of searched templates in 50-mHz bands. The variation with frequency is due to the increasing sky resolution. $N_f \times N_{\hat{f}} \sim 3.7 \times 10^8$, where N_f and $N_{\hat{f}}$ are the number of f and \hat{f} templates searched in 50-mHz bands. The total number of templates searched between 50 and 510 Hz is 6.3×10^{16} .

The search is split into work-units (WUs) sized to keep

the average Einstein@Home volunteer computer busy for about 6 hours. Each WU searches a 50 mHz band, the entire spindown range and 13 points in the sky, corresponding to 4.9×10^9 templates out of which it returns only the top 3000. A total of 12.7 million WUs are necessary to cover the entire parameter space. The total number of templates searched is 6.3×10^{16} .

1. The ranking statistic

The search was actually carried out in separate Einstein@Home runs that used different ranking statistics to define the top-candidate-list, reflecting different stages in the development of a detection statistic robust with respect to spectral lines in the data [21]. In particular, three ranking statistics were used: the average $2\mathcal{F}$ statistic over the segments, $2\bar{\mathcal{F}}$, which in essence at every template point is the likelihood of having a signal with the shape given by the template versus having Gaussian noise; the line-veto statistic \hat{O}_{SL} which is the odds ratio of having a signal versus having a spectral line; and a general line-robust statistic, \hat{O}_{SGL} , that tests the signal hypothesis against a Gaussian noise + spectral line noise model. Such a statistic can match the performance of both the standard average $2\bar{\mathcal{F}}$ statistic in Gaussian noise and the line-veto statistic in presence of single-detector spectral disturbances and statistically outperforms them when the noise is a mixture of both [21].

We combine the $2\bar{\mathcal{F}}$ -ranked results with the \hat{O}_{SL} -ranked results to produce a single list of candidates ranked according to the general line-robust statistic \hat{O}_{SGL} . We now explain how this is achieved. Alongside the detection statistic value and the parameter space cell coordinates of each candidate, the Einstein@Home application also returns the single-detector $2\bar{\mathcal{F}}^X$ values (“X” indicates the detector). These are used to compute, for every candidate of any run, the \hat{O}_{SGL} through Eq. 61 of [21]:

$$\ln \hat{O}_{\text{SGL}} = \ln \hat{o}_{\text{SL}} + \hat{\mathcal{F}} - \hat{\mathcal{F}}''_{\text{max}} - \ln \left(e^{\hat{\mathcal{F}}_* - \hat{\mathcal{F}}''_{\text{max}}} + \left\langle \hat{r}^X e^{\hat{\mathcal{F}}^X - \hat{\mathcal{F}}''_{\text{max}}} \right\rangle \right), \quad (3)$$

with the angle-brackets indicating the average with re-

T_{coh}	60 hrs
T_{ref}	960499913.5 GPS sec
N_{seg}	90
δf	1.6×10^{-6} Hz
$\delta \dot{f}_c$	5.8×10^{-11} Hz/s
γ	230
m_{sky}	0.3 + equatorial patch

TABLE I. Search parameters rounded to the first decimal figure. T_{ref} is the reference time that defines the frequency and frequency derivative values.

spect to detectors (X) and

$$\begin{aligned}\widehat{\mathcal{F}} &= N_{\text{seg}} \overline{\mathcal{F}} \\ \widehat{\mathcal{F}}^X &= N_{\text{seg}} \overline{\mathcal{F}}^X\end{aligned}\quad (4)$$

$$\widehat{\mathcal{F}}''_{\text{max}} \equiv \max \left(\widehat{\mathcal{F}}_*, \widehat{\mathcal{F}}^X + \ln \widehat{r}^X \right) \quad (5)$$

$$\widehat{\mathcal{F}}_* \equiv \widehat{\mathcal{F}}_*^{(0)} - \ln \widehat{o}_{\text{LG}} \quad (6)$$

$$\widehat{\mathcal{F}}_*^{(0)} \equiv \ln c_*^{N_{\text{seg}}} \quad \text{with } c_* \text{ set to } 20.64 \quad (7)$$

$$\widehat{o}_{\text{LG}} = \sum_X \widehat{o}_{\text{LG}}^X \quad (8)$$

$$\widehat{r}^X \equiv \frac{\widehat{o}_{\text{LG}}^X}{\widehat{o}_{\text{LG}}/N_{\text{det}}} \quad (9)$$

$$\widehat{p}_{\text{L}} \equiv \frac{\widehat{o}_{\text{LG}}}{1 + \widehat{o}_{\text{LG}}} \quad (10)$$

where $\widehat{o}_{\text{LG}}^X$ is the assumed prior probability of a spectral line occurring in any frequency bin of detector X , \widehat{p}_{L} is the line prior estimated from the data, $N_{\text{det}} = 2$ is the number of detectors, and \widehat{o}_{SL} is an assumed prior probability of a line being a signal (set arbitrarily to 1; its specific value does not affect the ranking statistic). Following the reasoning of Eq. 67 of [21], with $N_{\text{seg}} = 90$ we set $c_* = 20.64$ corresponding to a Gaussian false-alarm probability of 10^{-9} and an average $2\mathcal{F}$ transition scale of ~ 6 ($\mathcal{F}_*^{(0)} \sim 3$). The $\widehat{o}_{\text{LG}}^X$ values are estimated from the data as described in Section VI.A of [21] in 50-mHz bands with a normalized-SFT-power threshold $\mathcal{P}_{\text{thr}}^X = \mathcal{P}_{\text{thr}}(p_{\text{FA}} = 10^{-9}, N_{\text{SFT}}^X \sim 6000) \approx 1.08$. For every 50-mHz band the list of candidates from the $2\mathcal{F}$ -ranked run is merged with the list from the \widehat{O}_{SL} -ranked run and duplicate candidates are considered only once. The resulting list is ranked by the newly-computed \widehat{O}_{SGL} and the top 3000 candidates are kept. This is our result-set and it is treated in a manner that is very similar to [3].

2. Identification of undisturbed bands

Even after the removal of disturbed data caused by spectral artefacts of known origin, the statistical properties of the results are not uniform across the search band. In what follows we concentrate on the subset of the

signal-frequency bands having reasonably uniform statistical properties. This still leaves us with the majority of the search parameter space while allowing us to use methods that rely on theoretical modelling of the significance in the statistical analysis of the results. Our classification of “clean” vs. “disturbed” bands has no pretence of being rigorous. It only serves the practical purpose of discarding from the analysis regions in parameter space with evident disturbances. The classification is carried out in two steps: a visual inspection and a refinement on the visual inspection.

The visual inspection is performed by three scientists who each look at various distributions of the detection statistics over the entire sky and spindown parameter space in 50-mHz bands. They rank each band with an integer score 0,1,2,3 ranging from “undisturbed” (0) to “disturbed” (3). A band is considered “undisturbed” if all three rankings are 0. The criteria agreed upon for ranking are that the distribution of detection statistic values should not show a visible trend affecting a large portion of the $f - \dot{f}$ plane and, if outliers exist in a small region, outside this region the detection statistic values should be within the expected ranges. Fig. 3 shows the \widehat{O}_{SGL} for three bands: two were marked as undisturbed and the other as disturbed. One of the bands contains the $f - \dot{f}$ parameter space that harbours a fake signal injected in the data to verify the detection pipelines. The detection statistic is elevated in a small region around the signal parameters. The visual inspection procedure does not mark as disturbed bands with such features.

Based on this visual inspection 13% of the bands between 50 and 510 Hz are marked as “disturbed”. Of these, 34% were given by all visual inspectors rankings smaller than 3, i.e. they were only marginally disturbed. Further inspection “rehabilitated” 42% of these. As a result of this refinement in the selection procedure we exclude from the current analysis 11% of the searched frequencies.

Fig. 4 shows the highest values of the detection statistic in half-Hz signal-frequency bands compared to the expectations. The set of candidates that the highest detection statistic values are picked from, does not include the 50mHz signal-frequency bands that stem entirely from fake data, from the cleaning procedure, or that were marked as disturbed. In this paper we refer to the candidates with the highest value of the detection

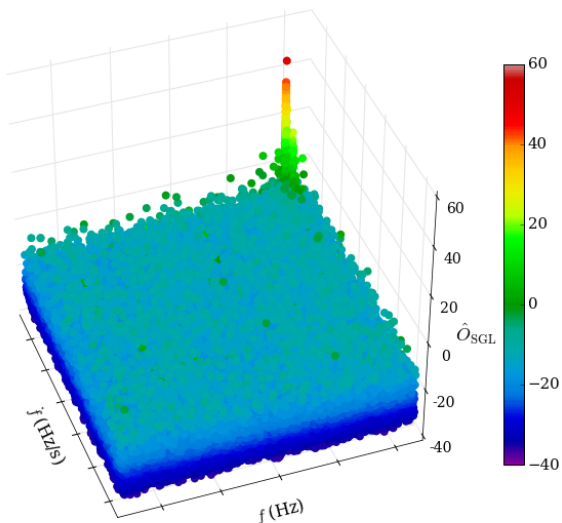
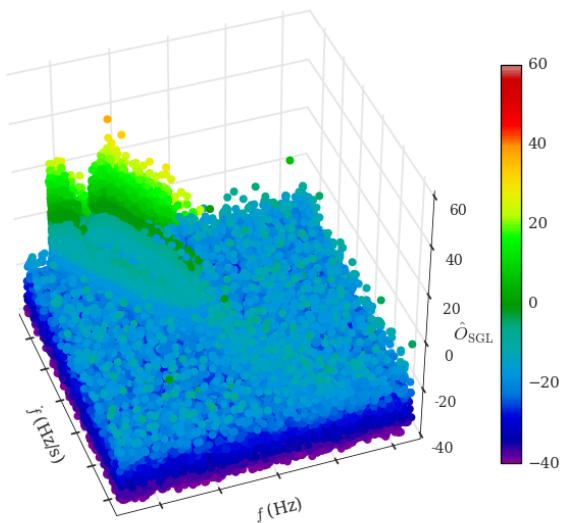
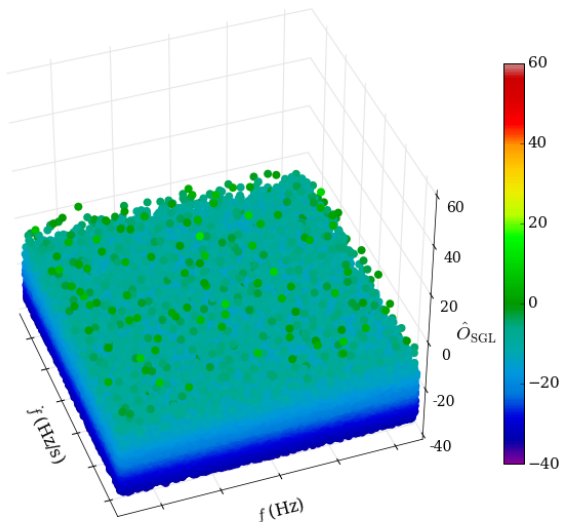


FIG. 3. On the z-axis and color-coded is the \hat{O}_{SGL} in three 50-mHz bands. The top band was marked as “undisturbed”. The middle band is an example of a “disturbed band”. The bottom band is an example of an “undisturbed band” but containing a signal, a fake one, in this case.

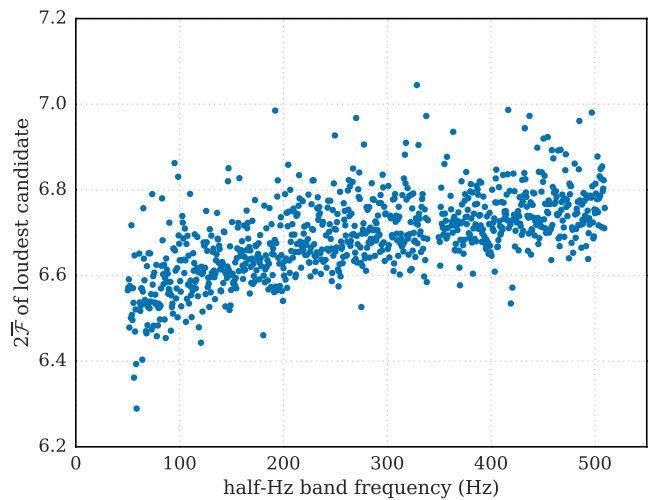


FIG. 4. Highest values of $2\bar{\mathcal{F}}$ in every half-Hz band as a function of band frequency. Since the number of templates increases with frequency so does the loudest $2\bar{\mathcal{F}}$.

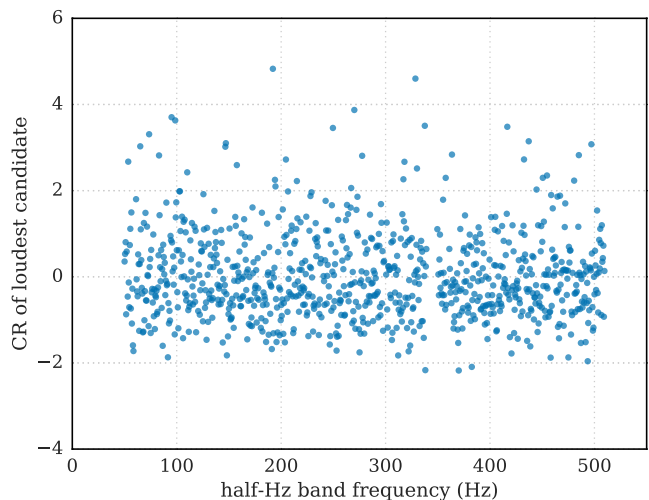


FIG. 5. Highest values of the significance (CR) in every half-Hz band as a function of band frequency. Since the significance folds in the expected value for the loudest $2\bar{\mathcal{F}}$ and its standard deviation, the significance of the loudest in noise does not increase with frequency. Our results are consistent with this expectation.

statistic as the *loudest* candidates.

The loudest expected value over N_{trials} independent trials of $2\bar{\mathcal{F}}$ is determined¹ by numerical integration of the probability density function given, for example, by Eq. 7 of [20]. For this search, we estimate that $N_{\text{trials}} \simeq 0.87 N_{\text{templ}}$, with N_{templ} being the number of templates searched.

As a uniform measure of significance of the highest $2\bar{\mathcal{F}}$

¹ After a simple change of variable from $2\bar{\mathcal{F}}$ to $N_{\text{seg}} \times 2\bar{\mathcal{F}}$.

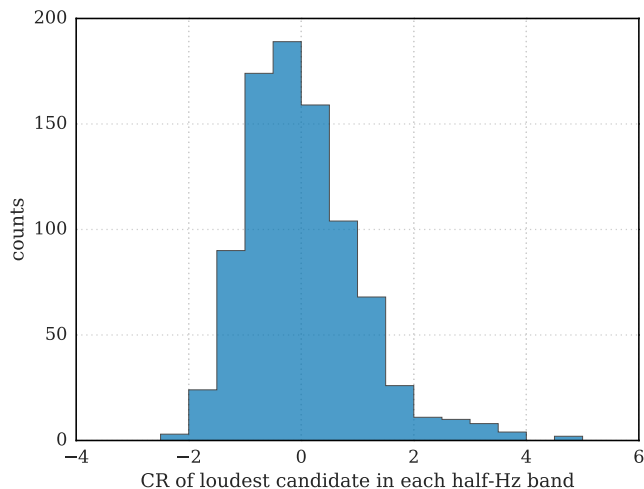


FIG. 6. Histogram of the highest values of the significance CR in every half-Hz band.

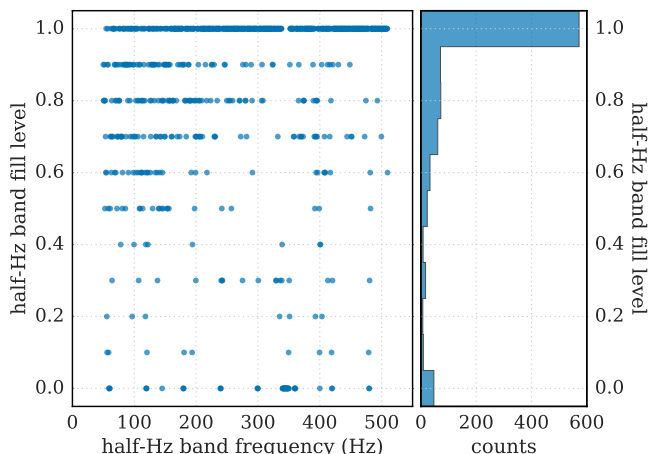


FIG. 7. The fraction of 50mHz bands (in signal frequency) which contribute to the results in every half-Hz band. As explained in the text, some bands are excluded because they are all from fake data or because they are marked as disturbed by the visual inspection. The list of excluded bands is given in Table A 3.

value across bands that were searched with different values of N_{trials} we introduce the critical ratio CR defined as the deviation of the measured highest $2\bar{\mathcal{F}}$ from the expected value, measured in units of the standard deviation:

$$\text{CR} := \frac{2\bar{\mathcal{F}}_{\text{meas}} - 2\bar{\mathcal{F}}_{\text{exped}}}{\sigma_{\text{exped}}}. \quad (11)$$

The highest and most significant detection statistic value from our search is $2\bar{\mathcal{F}} = 8.6$ at a frequency of about 52.76 Hz with a CR=29. This is due to a fake signal. The second highest value of the detection statistic is 7.04 at a frequency of about 329.01 Hz corresponding to a CR of 4.6. The second highest-CR candidate has a $2\bar{\mathcal{F}}$ of 6.99,

is at 192.16 Hz and has a CR=4.8.

Sorting loudest candidates from half-Hz bands according to detection statistic values is not the same as sorting them according to CR. The reason for this is that the number of templates is not the same for all half-Hz bands. This is due to the grid spacings decreasing with frequency (Eq. 2) and to the fact that, as previously explained, some 50-mHz bands have been excluded from the current analysis and hence some half-Hz bands comprise results from fewer than ten 50mHz bands. Fig.7 gives the fill-level of each half-Hz band, i.e. how many 50mHz bands have contributed candidates to the analysis out of ten. We use the CR as a measure of the significance because it folds in correctly the effect of varying number of templates in the half-Hz bands.

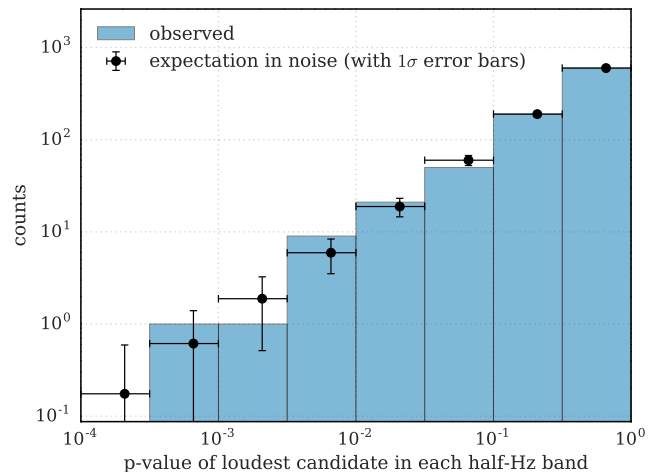


FIG. 8. p-values for the loudest in half-Hz bands of our data (histogram bars) and expected distribution of pure noise data for reference (black markers).

After excluding the candidate due to the fake signal, in this data we see no evidence of a signal: the distribution of p-values associated with every measured half-Hz band loudest is consistent with what we expect from noise-only across the measured range (Fig.8). In particular we note two things: 1) the two candidates at CR=4.6 and CR=4.8 are not significant when we consider how many half-Hz bands we have searched and 2) there is no population of low significance candidates deviating from the expectation of the noise-only case. We recall that the p-value for the loudest measured in any half-Hz band searched with an effective number of independent trials $N_{\text{trials}} = 0.87 N_{\text{trials}}$ is obtained by integrating Eq. 6 of [20] between the observed value and infinity.

IV. UPPER LIMITS

The search did not reveal any continuous gravitational wave signal in the parameter volume that was searched. We hence set frequentist upper limits on the maximum

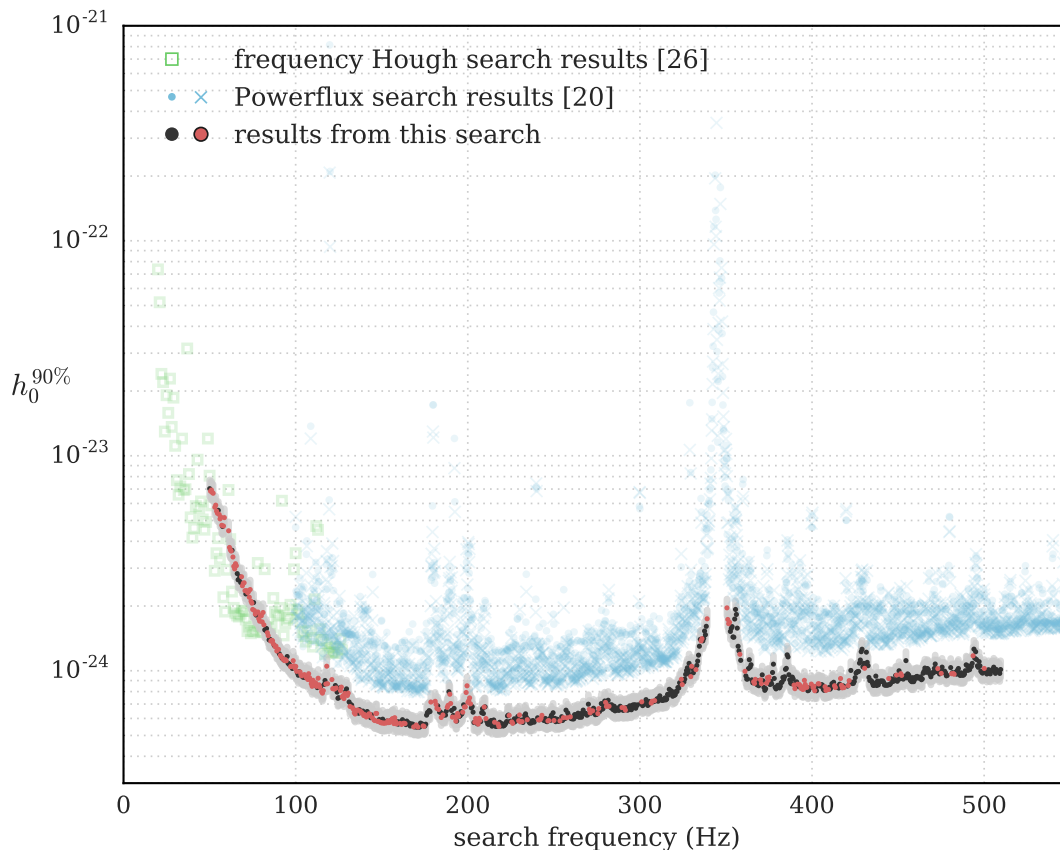


FIG. 9. 90% confidence upper limits on the gravitational wave amplitude of signals with frequency within half-Hz bands, from the entire sky and within the spindown range of the search. The light red markers denote half-Hz bands where the upper limit value does not hold for all frequencies in that interval. A list of the excluded frequencies is given in the Appendix. Although not obvious from the figure, due to the quality of the data we were not able to analyse the data in some half-Hz bands, so there are some points missing in the plot. For reference we also plot the upper limit results from two searches: one on the same data (Powerflux) [2] and on contemporary data from the Virgo detector (frequency Hough) [4]. The Powerflux points are obtained by rescaling the best (crosses) and worst-case (dots) upper limit values as explained in the text. It should be noted that the Powerflux upper limits are set at 95% rather than 90% but refer to 0.25 Hz bands rather than half-Hz.

gravitational wave amplitude consistent with this null result in half-Hz bands : $h_0^{90\%}(f)$. $h_0^{90\%}(f)$ is the GW amplitude such that 90% of a population of signals with parameter values in our search range would have produced a candidate louder than what was observed by our search. This is the criterion hereafter referred to as “detection”.

Evaluating these upper limits with injection-and-recovery Monte Carlo simulations in every half-Hz band is too computationally intensive. So we perform them in a subset of 50 bands and infer the upper limit values in the other bands from these. The 50 bands are evenly spaced in the search frequency range. For each band $j = 1 \dots 50$, we measure the 90% upper limit value corresponding to different detection criteria. The different detection criteria are defined by different CR values for the measured loudest. The first CR bin, CR_0 , is for CR values equal to or smaller than 0, the next bins are for $i < CR_i \leq (i + 1)$ with $i=1\dots 5$. Correspondingly we have $h_{0,CR_i}^{90\%,j}$ for each band. For every detection criteria

and every band we determine the sensitivity depth [22], and by averaging these sensitivity depths over the bands we derive a sensitivity depth for every detection criteria: $\mathcal{D}_{CR_i}^{90\%} = 1/50 \sum_j \mathcal{D}_{CR_i}^{90\%,j}$. We use these to set upper limits in the bands k where we have not performed injection-and-recovery simulations as

$$h_0^{90\%}(f_k) = \frac{\sqrt{S_h(f_k)}}{\mathcal{D}_{CR_i(k)}^{90\%}}, \quad (12)$$

where $CR_i(k)$ is the significance bin of the loudest candidate of the k^{th} band and $S_h(f_k)$ the power spectral density of the data (measured in $1/\sqrt{\text{Hz}}$). The values of the sensitivity depths range between $\mathcal{D}_{CR_6}^{90\%} \simeq 33 (1/\sqrt{\text{Hz}})$ and $\mathcal{D}_{CR_0}^{90\%} \simeq 37 (1/\sqrt{\text{Hz}})$. The uncertainties on the upper limit values introduced by this procedure are $\simeq 10\%$ of the nominal upper limit value. We represent this uncertainty as a shaded region around the upper limit values in Fig.9. The upper limit values are also provided in tabular form in the Appendix in Table IV. We do not set

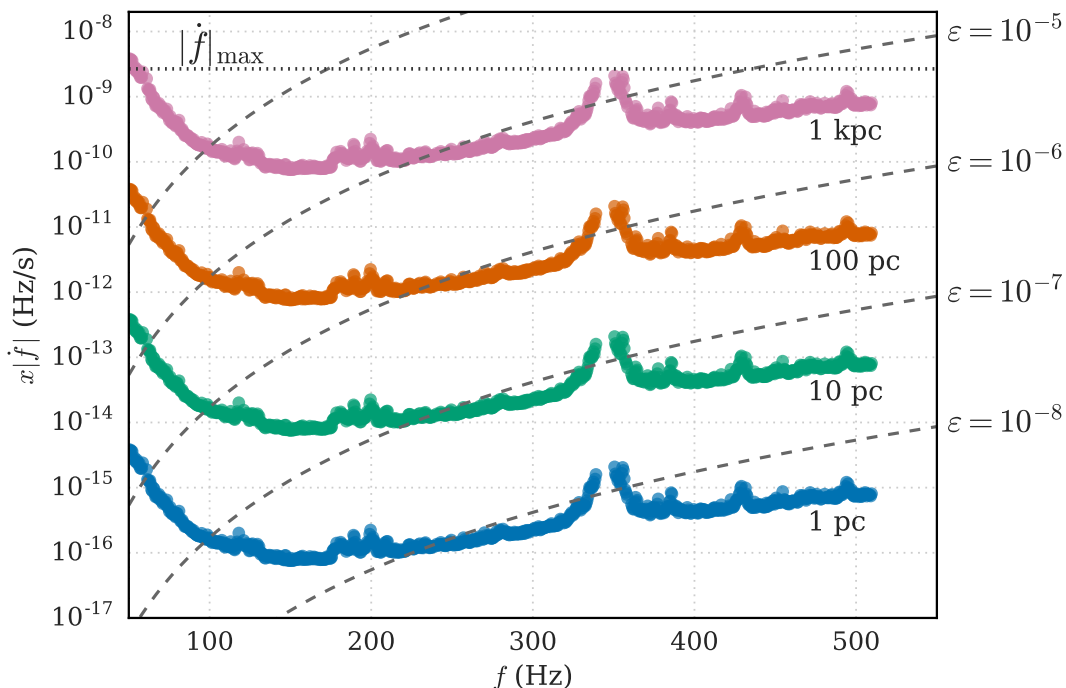


FIG. 10. Gravitational wave amplitude upper limits recast as curves in the $f - x|\dot{f}|$ plane for sources at given distances and having assumed $I = 10^{38}$ kg m². f is the signal frequency and $x|\dot{f}|$ is the gravitational-wave spindown, i.e. the fraction of the actual spindown that accounts for the rotational energy loss due to GW emission. Superimposed are curves of constant ellipticity $\epsilon(f, \dot{f}|I = 10^{38}$ kg m²). The dotted line at $|\dot{f}|_{\max}$ indicates the maximum magnitude of searched spindown.

upper limits in half-Hz bands where the results are entirely produced with fake data inserted by the cleaning procedure described in Section II. Upper limits for such bands will not appear in Table A 1 nor in Fig. 9. There also exist 50-mHz bands that include contributions from fake data as a result of the cleaning procedure or that have been excluded from the analysis because they were marked as disturbed by the visual inspection procedure described in Section III 2. We mark the half-Hz bands which host these 50mHz bands with a different colour (light red) in Fig.9. In Table A 3 in the Appendix we provide a complete list of such 50-mHz bands because it is important to note that the upper limit values do not apply to those 50-mHz bands. Finally we note that, due to the cleaning procedure, there exist signal frequency bands where the search results *might* have contributions from fake data. We list these signal-frequency ranges in Table A 4. For completeness this table also contains the cleaned bands of Table A 3, under the column header “all fake data”.

V. CONCLUSIONS

Our upper limits are the tightest ever placed for this set of target signals. The smallest value of the GW amplitude upper limit is 5.5×10^{-25} in the band 170.5-171 Hz. Fig. 9 shows the upper limit values as a function of

search frequency. We also show the upper limits from [2], another all-sky search on S6 data, rescaled according to [23] to enable a direct comparison with ours. Under the assumption that the sources are uniformly distributed in space, our search probes a volume in space a few times larger than that of [2]. It should however be noted that [2] examines a much broader parameter space than the one presented here. The Virgo VSR2 and VSR4 science runs were contemporary to the S6 run and more sensitive at low frequency with respect to LIGO. The Virgo data were analysed in search of continuous signals from the whole sky in the frequency range 20 Hz - 128 Hz and a narrower spindown range than that covered here, with $|\dot{f}| \leq 10^{-10}$ Hz/s [4]. Our sensitivity is comparable to that achieved by that search and improves on it above 80 Hz.

Following [24], we define the fraction x of the spindown rotational energy emitted in gravitational waves. The star’s ellipticity necessary to sustain such emission is

$$\epsilon(f, x\dot{f}) = \sqrt{\frac{5c^5}{32\pi^4 G} \frac{x\dot{f}}{I f^5}}, \quad (13)$$

where c is the speed of light, G is the gravitational constant, f is the GW frequency and I the principal moment of inertia of the star. Correspondingly, $x\dot{f}$ is the spindown rate that accounts for the emission of GWs and this is why we refer to it as the GW spindown. The gravitational wave amplitude h_0 at the detector coming from

a GW source like that of Eq.13, at a distance D from Earth is

$$h_0(f, x\dot{f}, D) = \frac{1}{D} \sqrt{\frac{5GI}{2c^3} \frac{x\dot{f}}{f}}. \quad (14)$$

Based on this last equation, we can use our GW amplitude upper limits to bound the minimum distance for compact objects emitting continuous gravitational waves under different assumptions on the object's ellipticity (i.e. gravitational wave spindown). This is shown in Fig. 10. We find that for most frequencies above 230 Hz our upper limits exclude compact objects with ellipticities of $10^{-6} \sqrt{\frac{10^{38} \text{kg m}^2}{I}}$ (corresponding to GW spindowns between 10^{-12} Hz/s and 10^{-11} Hz/s) within 100 pc of Earth. Both the ellipticity and the distance ranges span absolutely plausible values and could not have been excluded with other measurements.

We expect the methodology used in this search to serve as a template for the assessment of Einstein@Home run results in the future, for example the next Einstein@Home run, using advanced LIGO data that is being processed as this paper is written. Results of searches for continuous wave signals could also be mined further, probing sub-threshold candidates with a hierarchical series of follow-up searches. This is not the topic of this paper and might be pursued in a forthcoming publication.

VI. ACKNOWLEDGMENTS

The authors gratefully acknowledge the support of the Einstein@Home volunteers, of the United States National Science Foundation for the construction and operation of the LIGO Laboratory, the Science and Technology Facilities Council of the United Kingdom, the Max-Planck-Society, and the State of Niedersachsen/Germany for support of the construction and operation of the GEO600 detector, and the Italian Istituto Nazionale di Fisica Nucleare and the French Centre National de la Recherche Scientifique for the construction and operation of the Virgo detector. The authors also gratefully acknowledge the support of the research by these agencies and by the Australian Research Council, the International Science Linkages program of the Commonwealth of Australia, the Council of Scientific and Industrial Research of India, the Istituto Nazionale di Fisica Nucleare of Italy, the Spanish Ministerio de Educación y Ciencia, the Conselleria d'Economia Hisenda i Innovació of the Govern de les Illes Balears, the Foundation for Fundamental Research on Matter supported by the Netherlands Organisation for Scientific Research, the Polish Ministry of Science and Higher Education, the FOCUS Programme of Foundation for Polish Science, the Royal Society, the Scottish Funding Council, the Scottish Universities Physics Alliance, The National Aeronautics and Space Administration, the Carnegie Trust, the Leverhulme Trust, the

David and Lucile Packard Foundation, the Research Corporation, and the Alfred P. Sloan Foundation.

This document has been assigned LIGO Laboratory document number LIGO-P1600156-v20.

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Appendix A: Tabular data

1. Upper limit values

f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$
50.063	70.3 ± 12.8	50.563	68.4 ± 12.5	51.063	69.3 ± 12.6	51.563	67.5 ± 12.4
52.063	66.9 ± 12.2	53.063	57.6 ± 10.5	53.563	58.9 ± 10.9	54.063	55.3 ± 10.1
54.563	54.0 ± 9.9	55.063	55.7 ± 10.2	55.563	53.3 ± 9.8	56.063	50.9 ± 9.3
56.563	51.8 ± 9.5	57.063	47.5 ± 8.7	57.563	46.9 ± 8.6	58.063	47.1 ± 8.6
58.563	51.5 ± 9.4	61.063	44.8 ± 8.2	61.563	37.4 ± 6.9	62.063	36.5 ± 6.7
62.563	36.0 ± 6.6	63.063	36.3 ± 6.6	63.563	33.8 ± 6.2	64.063	30.6 ± 5.6
64.563	29.8 ± 5.4	65.063	31.5 ± 5.9	65.563	30.8 ± 5.7	66.063	28.3 ± 5.2
66.563	26.5 ± 4.8	67.063	26.5 ± 4.9	67.563	27.3 ± 5.0	68.063	25.7 ± 4.7
68.563	27.4 ± 5.0	69.063	24.8 ± 4.5	69.563	25.5 ± 4.7	70.063	25.7 ± 4.7
70.563	23.6 ± 4.3	71.063	22.8 ± 4.2	71.563	23.6 ± 4.3	72.063	23.1 ± 4.2
72.563	23.3 ± 4.2	73.063	22.0 ± 4.0	73.563	23.9 ± 4.5	74.063	21.1 ± 3.8
74.563	20.6 ± 3.8	75.063	19.3 ± 3.5	75.563	20.8 ± 3.8	76.063	19.0 ± 3.5
76.563	18.3 ± 3.4	77.063	18.1 ± 3.3	77.563	18.5 ± 3.4	78.063	18.8 ± 3.4
78.563	17.4 ± 3.2	79.063	17.0 ± 3.1	79.563	18.1 ± 3.3	80.063	18.0 ± 3.3
80.563	16.9 ± 3.1	81.063	18.7 ± 3.4	81.563	16.3 ± 3.0	82.063	15.5 ± 2.8
82.563	15.4 ± 2.8	83.063	15.7 ± 2.9	83.563	15.0 ± 2.8	84.063	14.6 ± 2.7
84.563	13.9 ± 2.5	85.063	14.0 ± 2.6	85.563	13.7 ± 2.5	86.063	13.9 ± 2.5
86.563	13.8 ± 2.5	87.063	13.3 ± 2.4	87.563	13.1 ± 2.4	88.063	12.9 ± 2.4
88.563	13.0 ± 2.4	89.063	12.4 ± 2.3	89.563	12.3 ± 2.3	90.063	12.6 ± 2.3
90.563	12.0 ± 2.2	91.063	11.8 ± 2.2	91.563	11.6 ± 2.1	92.063	11.4 ± 2.1
92.563	11.3 ± 2.1	93.063	11.2 ± 2.1	93.563	11.1 ± 2.0	94.063	11.3 ± 2.1
94.563	11.1 ± 2.0	95.063	11.6 ± 2.2	95.563	10.8 ± 2.0	96.063	10.8 ± 2.0
96.563	10.6 ± 1.9	97.063	10.4 ± 1.9	97.563	10.5 ± 1.9	98.063	10.2 ± 1.9
98.563	11.1 ± 2.1	99.063	10.5 ± 1.9	99.563	10.3 ± 1.9	100.063	10.5 ± 1.9
100.563	9.9 ± 1.8	101.063	9.8 ± 1.8	101.563	9.5 ± 1.7	102.063	9.9 ± 1.8
102.563	9.9 ± 1.8	103.063	9.6 ± 1.8	103.563	9.5 ± 1.7	104.063	9.4 ± 1.7
104.563	9.3 ± 1.7	105.063	9.6 ± 1.8	105.563	9.3 ± 1.7	106.063	9.3 ± 1.7
106.563	9.4 ± 1.7	107.063	9.1 ± 1.7	107.563	9.7 ± 1.8	108.063	9.3 ± 1.7
108.563	9.0 ± 1.7	109.063	8.7 ± 1.6	109.563	8.5 ± 1.5	110.063	9.0 ± 1.7
110.563	8.6 ± 1.6	111.063	8.6 ± 1.6	111.563	8.8 ± 1.6	112.063	8.5 ± 1.5
112.563	8.3 ± 1.5	113.063	9.2 ± 1.7	113.563	8.6 ± 1.6	114.063	8.4 ± 1.5
114.563	8.4 ± 1.6	115.063	8.0 ± 1.5	115.563	7.9 ± 1.4	116.063	8.1 ± 1.5
116.563	8.6 ± 1.6	117.063	9.0 ± 1.7	117.563	8.7 ± 1.6	118.063	10.5 ± 1.9
118.563	8.7 ± 1.6	121.063	9.1 ± 1.7	121.563	8.2 ± 1.5	122.063	8.3 ± 1.5
122.563	8.2 ± 1.5	123.063	8.5 ± 1.6	123.563	8.3 ± 1.5	124.063	8.0 ± 1.4
124.563	7.4 ± 1.4	125.063	7.5 ± 1.4	125.563	8.3 ± 1.5	126.063	8.1 ± 1.5
126.563	8.4 ± 1.5	127.063	7.6 ± 1.4	127.563	7.7 ± 1.4	128.063	7.4 ± 1.4
128.563	7.8 ± 1.4	129.063	8.0 ± 1.5	129.563	8.2 ± 1.5	130.063	7.7 ± 1.4
130.563	7.9 ± 1.4	131.063	7.2 ± 1.3	131.563	6.8 ± 1.2	132.063	7.0 ± 1.3
132.563	6.9 ± 1.3	133.063	6.7 ± 1.2	133.563	6.6 ± 1.2	134.063	6.4 ± 1.2
134.563	6.3 ± 1.2	135.063	6.5 ± 1.2	135.563	6.5 ± 1.2	136.063	6.6 ± 1.2
136.563	6.3 ± 1.2	137.063	6.6 ± 1.2	137.563	6.5 ± 1.2	138.063	6.4 ± 1.2
138.563	6.4 ± 1.2	139.063	6.5 ± 1.2	139.563	6.2 ± 1.1	140.063	6.3 ± 1.1
140.563	6.2 ± 1.1	141.063	6.1 ± 1.1	141.563	6.5 ± 1.2	142.063	6.2 ± 1.1
142.563	6.3 ± 1.2	143.063	6.3 ± 1.1	143.563	6.0 ± 1.1	144.063	6.2 ± 1.1
144.563	6.0 ± 1.1	145.563	5.9 ± 1.1	146.063	5.9 ± 1.1	146.563	6.3 ± 1.2
147.063	6.3 ± 1.2	147.563	5.8 ± 1.1	148.063	5.8 ± 1.1	148.563	5.9 ± 1.1
149.063	5.8 ± 1.1	149.563	5.7 ± 1.0	150.063	5.7 ± 1.0	150.563	6.0 ± 1.1
151.063	5.7 ± 1.0	151.563	5.7 ± 1.0	152.063	5.7 ± 1.1	152.563	5.7 ± 1.0
153.063	5.8 ± 1.1	153.563	5.8 ± 1.1	154.063	5.7 ± 1.0	154.563	5.7 ± 1.1
155.063	5.9 ± 1.1	155.563	5.9 ± 1.1	156.063	6.0 ± 1.1	156.563	6.0 ± 1.1
157.063	5.7 ± 1.0	157.563	6.0 ± 1.1	158.063	5.8 ± 1.1	158.563	5.7 ± 1.0
159.063	5.8 ± 1.1	159.563	5.6 ± 1.0	160.063	5.8 ± 1.1	160.563	5.7 ± 1.0
161.063	5.7 ± 1.0	161.563	5.6 ± 1.0	162.063	5.9 ± 1.1	162.563	5.7 ± 1.0
163.063	5.7 ± 1.0	163.563	5.7 ± 1.0	164.063	5.6 ± 1.0	164.563	5.8 ± 1.1
165.063	5.7 ± 1.0	165.563	5.7 ± 1.0	166.063	5.7 ± 1.0	166.563	5.5 ± 1.0
167.063	5.7 ± 1.0	167.563	5.6 ± 1.0	168.063	5.6 ± 1.0	168.563	5.5 ± 1.0

f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$
169.063	5.5 ± 1.0	169.563	5.5 ± 1.0	170.063	5.6 ± 1.0	170.563	5.5 ± 1.0
171.063	5.5 ± 1.0	171.563	5.5 ± 1.0	172.063	5.5 ± 1.0	172.563	5.7 ± 1.0
173.063	5.6 ± 1.0	173.563	5.7 ± 1.0	174.063	5.5 ± 1.0	174.563	5.5 ± 1.0
175.063	5.5 ± 1.0	175.563	5.6 ± 1.0	176.063	6.2 ± 1.1	176.563	6.4 ± 1.2
177.063	6.4 ± 1.2	177.563	6.5 ± 1.2	178.063	6.5 ± 1.2	178.563	7.2 ± 1.3
181.063	7.2 ± 1.3	181.563	7.0 ± 1.3	182.063	6.7 ± 1.2	182.563	6.9 ± 1.3
183.063	6.6 ± 1.2	183.563	6.4 ± 1.2	184.063	6.4 ± 1.2	184.563	6.1 ± 1.1
185.063	6.3 ± 1.2	185.563	6.2 ± 1.1	186.063	6.2 ± 1.1	186.563	6.3 ± 1.2
187.063	6.2 ± 1.1	187.563	6.5 ± 1.2	188.063	6.8 ± 1.2	188.563	6.9 ± 1.3
189.063	8.0 ± 1.5	189.563	7.8 ± 1.4	190.063	7.0 ± 1.3	190.563	6.5 ± 1.2
191.063	6.1 ± 1.1	191.563	6.2 ± 1.1	192.063	6.7 ± 1.3	192.563	6.1 ± 1.1
193.063	5.8 ± 1.1	193.563	5.8 ± 1.1	194.063	6.3 ± 1.2	194.563	6.1 ± 1.1
195.063	6.1 ± 1.1	195.563	6.2 ± 1.1	196.063	6.5 ± 1.2	196.563	6.3 ± 1.2
197.063	6.4 ± 1.2	197.563	6.9 ± 1.3	198.063	6.8 ± 1.2	198.563	6.8 ± 1.2
199.063	7.9 ± 1.4	199.563	8.5 ± 1.6	200.063	7.1 ± 1.3	200.563	7.3 ± 1.3
201.063	7.5 ± 1.4	201.563	7.0 ± 1.3	202.063	6.7 ± 1.2	202.563	6.8 ± 1.2
203.063	6.4 ± 1.2	203.563	5.7 ± 1.1	204.063	5.8 ± 1.1	204.563	6.0 ± 1.1
205.063	5.8 ± 1.1	205.563	5.7 ± 1.0	206.063	5.6 ± 1.0	206.563	6.0 ± 1.1
207.063	5.9 ± 1.1	207.563	5.8 ± 1.1	208.063	6.4 ± 1.2	208.563	6.7 ± 1.2
209.063	6.3 ± 1.2	209.563	6.8 ± 1.2	210.063	6.8 ± 1.2	210.563	6.0 ± 1.1
211.063	5.8 ± 1.1	211.563	5.7 ± 1.0	212.063	5.6 ± 1.0	212.563	5.8 ± 1.1
213.063	5.7 ± 1.0	213.563	5.9 ± 1.1	214.063	5.5 ± 1.0	214.563	5.8 ± 1.1
215.063	5.9 ± 1.1	215.563	5.8 ± 1.1	216.063	5.5 ± 1.0	216.563	5.5 ± 1.0
217.063	5.5 ± 1.0	217.563	5.7 ± 1.0	218.063	5.5 ± 1.0	218.563	5.8 ± 1.1
219.063	5.5 ± 1.0	219.563	5.7 ± 1.0	220.063	5.7 ± 1.0	220.563	5.5 ± 1.0
221.063	5.6 ± 1.0	221.563	5.6 ± 1.0	222.063	5.7 ± 1.0	222.563	5.8 ± 1.1
223.063	6.2 ± 1.1	223.563	6.2 ± 1.1	224.063	6.2 ± 1.1	224.563	5.8 ± 1.1
225.063	5.8 ± 1.1	225.563	5.8 ± 1.1	226.063	5.7 ± 1.0	226.563	5.7 ± 1.0
227.063	6.0 ± 1.1	227.563	5.8 ± 1.1	228.063	5.9 ± 1.1	228.563	5.9 ± 1.1
229.063	6.1 ± 1.1	229.563	5.9 ± 1.1	230.063	6.2 ± 1.1	230.563	5.8 ± 1.1
231.063	5.9 ± 1.1	231.563	5.8 ± 1.1	232.063	5.7 ± 1.1	232.563	5.9 ± 1.1
233.063	6.2 ± 1.1	233.563	6.3 ± 1.1	234.063	6.1 ± 1.1	234.563	5.9 ± 1.1
235.063	5.9 ± 1.1	235.563	5.8 ± 1.1	236.063	5.7 ± 1.0	236.563	5.7 ± 1.0
237.063	5.7 ± 1.0	237.563	5.9 ± 1.1	238.063	5.9 ± 1.1	238.563	5.8 ± 1.1
240.563	6.0 ± 1.1	241.063	5.9 ± 1.1	241.563	5.9 ± 1.1	242.063	5.9 ± 1.1
242.563	6.0 ± 1.1	243.063	6.2 ± 1.1	243.563	6.0 ± 1.1	244.063	5.9 ± 1.1
244.563	5.9 ± 1.1	245.063	6.0 ± 1.1	245.563	5.8 ± 1.1	246.063	5.8 ± 1.1
246.563	5.8 ± 1.1	247.063	5.9 ± 1.1	247.563	6.0 ± 1.1	248.063	5.9 ± 1.1
248.563	6.2 ± 1.1	249.063	6.1 ± 1.1	249.563	6.4 ± 1.2	250.063	5.9 ± 1.1
250.563	6.0 ± 1.1	251.063	5.8 ± 1.1	251.563	5.9 ± 1.1	252.063	5.9 ± 1.1
252.563	5.8 ± 1.1	253.063	5.8 ± 1.1	253.563	5.8 ± 1.1	254.063	5.9 ± 1.1
254.563	6.1 ± 1.1	255.063	5.9 ± 1.1	255.563	6.1 ± 1.1	256.063	6.0 ± 1.1
256.563	6.0 ± 1.1	257.063	6.6 ± 1.2	257.563	6.0 ± 1.1	258.063	6.4 ± 1.2
258.563	6.2 ± 1.1	259.063	6.1 ± 1.1	259.563	6.1 ± 1.1	260.063	6.0 ± 1.1
260.563	6.0 ± 1.1	261.063	6.0 ± 1.1	261.563	6.0 ± 1.1	262.063	6.3 ± 1.1
262.563	6.1 ± 1.1	263.063	6.2 ± 1.1	263.563	6.2 ± 1.1	264.063	6.3 ± 1.2
264.563	6.1 ± 1.1	265.063	6.1 ± 1.1	265.563	6.3 ± 1.1	266.063	6.1 ± 1.1
266.563	6.4 ± 1.2	267.063	6.6 ± 1.2	267.563	6.3 ± 1.2	268.063	6.4 ± 1.2
268.563	6.3 ± 1.2	269.063	6.2 ± 1.1	269.563	6.2 ± 1.1	270.063	7.0 ± 1.3
270.563	6.6 ± 1.2	271.063	6.4 ± 1.2	271.563	6.3 ± 1.2	272.063	6.6 ± 1.2
272.563	6.5 ± 1.2	273.063	6.7 ± 1.2	273.563	6.5 ± 1.2	274.063	6.2 ± 1.1
274.563	6.3 ± 1.1	275.063	6.3 ± 1.1	275.563	6.3 ± 1.2	276.063	6.7 ± 1.2
276.563	6.5 ± 1.2	277.063	6.6 ± 1.2	277.563	7.0 ± 1.3	278.063	6.6 ± 1.2
278.563	6.7 ± 1.2	279.063	6.8 ± 1.3	279.563	7.2 ± 1.3	280.063	7.1 ± 1.3
280.563	6.8 ± 1.2	281.063	6.9 ± 1.3	281.563	7.3 ± 1.3	282.063	6.8 ± 1.3
282.563	6.9 ± 1.3	283.063	6.7 ± 1.2	283.563	6.9 ± 1.3	284.063	6.6 ± 1.2
284.563	6.6 ± 1.2	285.063	6.8 ± 1.3	285.563	6.5 ± 1.2	286.063	6.7 ± 1.2
286.563	6.6 ± 1.2	287.063	6.7 ± 1.2	287.563	6.5 ± 1.2	288.063	6.6 ± 1.2
288.563	6.8 ± 1.2	289.063	6.6 ± 1.2	289.563	6.7 ± 1.2	290.063	6.6 ± 1.2
290.563	6.6 ± 1.2	291.063	6.7 ± 1.2	291.563	6.6 ± 1.2	292.063	6.7 ± 1.2
292.563	6.6 ± 1.2	293.063	6.6 ± 1.2	293.563	6.8 ± 1.2	294.063	6.9 ± 1.3
294.563	6.6 ± 1.2	295.063	6.6 ± 1.2	295.563	6.9 ± 1.3	296.063	6.9 ± 1.3
296.563	6.7 ± 1.2	297.063	6.9 ± 1.3	297.563	6.7 ± 1.2	298.063	6.9 ± 1.3

f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$
298.563	6.9 ± 1.3	300.563	7.1 ± 1.3	301.063	7.2 ± 1.3	301.563	6.9 ± 1.3
302.063	6.9 ± 1.3	302.563	7.1 ± 1.3	303.063	7.1 ± 1.3	303.563	7.3 ± 1.3
304.063	7.2 ± 1.3	304.563	6.9 ± 1.3	305.063	7.0 ± 1.3	305.563	7.2 ± 1.3
306.063	7.1 ± 1.3	306.563	7.1 ± 1.3	307.063	7.2 ± 1.3	307.563	7.2 ± 1.3
308.063	7.2 ± 1.3	308.563	7.3 ± 1.3	309.063	7.2 ± 1.3	309.563	7.3 ± 1.3
310.063	7.4 ± 1.4	310.563	7.2 ± 1.3	311.063	7.5 ± 1.4	311.563	7.6 ± 1.4
312.063	7.4 ± 1.4	312.563	7.3 ± 1.3	313.063	7.3 ± 1.3	313.563	7.3 ± 1.3
314.063	7.3 ± 1.3	314.563	7.5 ± 1.4	315.063	7.3 ± 1.3	315.563	7.4 ± 1.4
316.063	7.8 ± 1.4	316.563	7.7 ± 1.4	317.063	8.2 ± 1.5	317.563	7.8 ± 1.4
318.063	8.1 ± 1.5	318.563	7.8 ± 1.4	319.063	7.6 ± 1.4	319.563	8.0 ± 1.5
320.063	7.7 ± 1.4	320.563	7.7 ± 1.4	321.063	8.0 ± 1.5	321.563	8.0 ± 1.5
322.063	8.4 ± 1.5	322.563	8.3 ± 1.5	323.063	8.8 ± 1.6	323.563	8.7 ± 1.6
324.063	9.1 ± 1.7	324.563	8.6 ± 1.6	325.063	9.0 ± 1.6	325.563	8.9 ± 1.6
326.063	9.1 ± 1.7	326.563	9.6 ± 1.8	327.063	10.0 ± 1.8	327.563	10.3 ± 1.9
328.063	10.0 ± 1.8	328.563	10.8 ± 2.0	329.063	9.6 ± 1.8	329.563	9.4 ± 1.7
330.063	10.5 ± 1.9	330.563	10.2 ± 1.9	331.063	9.8 ± 1.8	331.563	10.2 ± 1.9
332.063	10.2 ± 1.9	332.563	10.1 ± 1.9	333.063	10.6 ± 1.9	333.563	11.1 ± 2.0
334.063	11.8 ± 2.2	334.563	13.0 ± 2.4	335.063	14.0 ± 2.6	335.563	13.8 ± 2.5
336.063	14.1 ± 2.6	336.563	13.8 ± 2.5	337.063	14.1 ± 2.6	337.563	15.3 ± 2.9
338.063	14.7 ± 2.7	338.563	16.1 ± 2.9	339.063	17.4 ± 3.2	350.563	19.6 ± 3.6
351.063	17.3 ± 3.2	351.563	16.6 ± 3.0	352.063	16.8 ± 3.1	352.563	15.2 ± 2.8
353.063	15.7 ± 2.9	353.563	16.0 ± 2.9	354.063	14.4 ± 2.6	354.563	14.3 ± 2.6
355.063	17.4 ± 3.2	355.563	19.3 ± 3.5	356.063	18.3 ± 3.3	356.563	15.8 ± 2.9
357.063	13.0 ± 2.4	357.563	12.4 ± 2.3	358.063	11.9 ± 2.2	358.563	11.2 ± 2.0
361.063	9.9 ± 1.8	361.563	9.5 ± 1.7	362.063	9.1 ± 1.7	362.563	9.2 ± 1.7
363.063	10.2 ± 1.9	363.563	11.3 ± 2.1	364.063	10.4 ± 1.9	364.563	10.7 ± 2.0
365.063	9.1 ± 1.7	365.563	8.8 ± 1.6	366.063	8.9 ± 1.6	366.563	8.7 ± 1.6
367.063	9.1 ± 1.7	367.563	9.0 ± 1.6	368.063	8.6 ± 1.6	368.563	9.0 ± 1.6
369.063	8.5 ± 1.6	369.563	8.9 ± 1.6	370.063	9.1 ± 1.7	370.563	8.7 ± 1.6
371.063	9.6 ± 1.8	371.563	9.0 ± 1.6	372.063	8.4 ± 1.5	372.563	8.1 ± 1.5
373.063	8.3 ± 1.5	373.563	8.7 ± 1.6	374.063	9.3 ± 1.7	374.563	9.0 ± 1.6
375.063	9.3 ± 1.7	375.563	8.6 ± 1.6	376.063	8.9 ± 1.6	376.563	8.7 ± 1.6
377.063	9.8 ± 1.8	377.563	10.7 ± 2.0	378.063	9.2 ± 1.7	378.563	8.4 ± 1.5
379.063	8.2 ± 1.5	379.563	8.4 ± 1.5	380.063	8.6 ± 1.6	380.563	8.5 ± 1.5
381.063	8.3 ± 1.5	381.563	8.5 ± 1.6	382.063	8.8 ± 1.6	382.563	8.9 ± 1.6
383.063	9.3 ± 1.7	383.563	9.1 ± 1.7	384.063	9.4 ± 1.7	384.563	10.2 ± 1.9
385.063	10.3 ± 1.9	385.563	11.9 ± 2.2	386.063	11.6 ± 2.1	386.563	9.6 ± 1.7
387.063	9.1 ± 1.7	387.563	8.8 ± 1.6	388.063	8.7 ± 1.6	388.563	9.3 ± 1.7
389.063	9.2 ± 1.7	389.563	8.6 ± 1.6	390.063	8.3 ± 1.5	390.563	8.8 ± 1.6
391.063	8.9 ± 1.6	391.563	8.7 ± 1.6	392.063	8.4 ± 1.5	392.563	8.6 ± 1.6
393.063	8.5 ± 1.6	393.563	8.3 ± 1.5	394.063	8.4 ± 1.5	394.563	8.2 ± 1.5
395.063	8.2 ± 1.5	395.563	9.0 ± 1.7	396.063	8.6 ± 1.6	396.563	8.4 ± 1.5
397.063	8.4 ± 1.5	397.563	8.1 ± 1.5	398.063	8.1 ± 1.5	398.563	8.3 ± 1.5
399.063	8.4 ± 1.5	399.563	8.7 ± 1.6	400.563	8.3 ± 1.5	401.063	8.5 ± 1.6
401.563	8.1 ± 1.5	402.063	8.1 ± 1.5	402.563	8.1 ± 1.5	403.063	8.5 ± 1.6
403.563	8.7 ± 1.6	404.063	8.7 ± 1.6	404.563	8.6 ± 1.6	405.063	8.5 ± 1.6
405.563	8.6 ± 1.6	406.063	8.6 ± 1.6	406.563	8.2 ± 1.5	407.063	8.1 ± 1.5
407.563	8.4 ± 1.5	408.063	8.1 ± 1.5	408.563	8.2 ± 1.5	409.063	8.2 ± 1.5
409.563	8.2 ± 1.5	410.063	8.4 ± 1.5	410.563	8.2 ± 1.5	411.063	8.4 ± 1.5
411.563	8.7 ± 1.6	412.063	8.7 ± 1.6	412.563	8.8 ± 1.6	413.063	8.5 ± 1.6
413.563	8.4 ± 1.5	414.063	8.4 ± 1.5	414.563	8.5 ± 1.5	415.063	8.5 ± 1.5
415.563	8.3 ± 1.5	416.063	8.7 ± 1.6	416.563	9.2 ± 1.7	417.063	8.6 ± 1.6
417.563	8.3 ± 1.5	418.063	8.5 ± 1.6	418.563	8.3 ± 1.5	420.563	8.5 ± 1.6
421.063	8.5 ± 1.6	421.563	9.0 ± 1.7	422.063	8.8 ± 1.6	422.563	10.0 ± 1.8
423.063	8.8 ± 1.6	423.563	8.7 ± 1.6	424.063	8.7 ± 1.6	424.563	8.9 ± 1.6
425.063	9.3 ± 1.7	425.563	9.7 ± 1.8	426.063	9.8 ± 1.8	426.563	9.9 ± 1.8
427.063	9.9 ± 1.8	427.563	10.9 ± 2.0	428.063	11.2 ± 2.1	428.563	12.3 ± 2.2
429.063	12.6 ± 2.3	429.563	10.4 ± 1.9	430.063	10.8 ± 2.0	430.563	10.3 ± 1.9
431.063	10.5 ± 1.9	431.563	12.2 ± 2.2	432.063	10.9 ± 2.0	432.563	10.6 ± 1.9
433.063	9.3 ± 1.7	433.563	9.0 ± 1.6	434.063	9.0 ± 1.6	434.563	9.0 ± 1.6
435.063	8.8 ± 1.6	435.563	8.6 ± 1.6	436.063	8.6 ± 1.6	436.563	8.8 ± 1.6
437.063	9.4 ± 1.8	437.563	8.5 ± 1.6	438.063	9.0 ± 1.6	438.563	8.6 ± 1.6
439.063	8.8 ± 1.6	439.563	8.9 ± 1.6	440.063	9.0 ± 1.6	440.563	8.9 ± 1.6

f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$	f (in Hz)	$h_0^{90\%} \times 10^{25}$
441.063	9.0 ± 1.6	441.563	8.8 ± 1.6	442.063	8.6 ± 1.6	442.563	8.6 ± 1.6
443.063	8.6 ± 1.6	443.563	8.6 ± 1.6	444.063	8.6 ± 1.6	444.563	9.2 ± 1.7
445.063	8.6 ± 1.6	445.563	8.7 ± 1.6	446.063	9.2 ± 1.7	446.563	9.1 ± 1.7
447.063	8.9 ± 1.6	447.563	9.0 ± 1.7	448.063	9.0 ± 1.6	448.563	9.5 ± 1.7
449.063	9.5 ± 1.8	449.563	8.9 ± 1.6	450.063	9.1 ± 1.7	450.563	10.0 ± 1.8
451.063	9.2 ± 1.7	451.563	9.7 ± 1.8	452.063	9.5 ± 1.7	452.563	9.2 ± 1.7
453.063	9.1 ± 1.7	453.563	9.4 ± 1.7	454.063	9.5 ± 1.7	454.563	11.1 ± 2.1
455.063	9.3 ± 1.7	455.563	9.7 ± 1.8	456.063	9.6 ± 1.8	456.563	9.4 ± 1.7
457.063	9.0 ± 1.7	457.563	8.9 ± 1.6	458.063	8.9 ± 1.6	458.563	9.3 ± 1.7
459.063	8.9 ± 1.6	459.563	9.1 ± 1.7	460.063	9.3 ± 1.7	460.563	9.4 ± 1.7
461.063	9.4 ± 1.7	461.563	9.3 ± 1.7	462.063	9.3 ± 1.7	462.563	9.3 ± 1.7
463.063	9.4 ± 1.7	463.563	9.1 ± 1.7	464.063	9.2 ± 1.7	464.563	9.7 ± 1.8
465.063	9.9 ± 1.8	465.563	10.3 ± 1.9	466.063	9.9 ± 1.8	466.563	9.8 ± 1.8
467.063	10.2 ± 1.9	467.563	10.1 ± 1.9	468.063	9.8 ± 1.8	468.563	9.6 ± 1.8
469.063	9.4 ± 1.7	469.563	9.7 ± 1.8	470.063	9.8 ± 1.8	470.563	9.8 ± 1.8
471.063	10.3 ± 1.9	471.563	10.7 ± 2.0	472.063	10.2 ± 1.9	472.563	9.9 ± 1.8
473.063	10.2 ± 1.9	473.563	9.9 ± 1.8	474.063	9.7 ± 1.8	474.563	10.0 ± 1.8
475.063	9.7 ± 1.8	475.563	10.4 ± 1.9	476.063	10.0 ± 1.8	476.563	9.8 ± 1.8
477.063	10.0 ± 1.8	477.563	9.8 ± 1.8	478.063	9.5 ± 1.7	478.563	9.5 ± 1.7
480.563	10.3 ± 1.9	481.063	9.7 ± 1.8	481.563	9.8 ± 1.8	482.063	9.7 ± 1.8
482.563	9.6 ± 1.8	483.063	9.7 ± 1.8	483.563	9.9 ± 1.8	484.063	9.6 ± 1.8
484.563	10.1 ± 1.8	485.063	10.2 ± 1.9	485.563	9.7 ± 1.8	486.063	9.5 ± 1.7
486.563	9.8 ± 1.8	487.063	9.5 ± 1.7	487.563	9.5 ± 1.7	488.063	9.5 ± 1.7
488.563	9.7 ± 1.8	489.063	10.0 ± 1.8	489.563	10.7 ± 1.9	490.063	10.6 ± 1.9
490.563	10.0 ± 1.8	491.063	10.3 ± 1.9	491.563	10.1 ± 1.9	492.063	10.5 ± 1.9
492.563	10.5 ± 1.9	493.063	10.8 ± 2.0	493.563	11.7 ± 2.1	494.063	12.6 ± 2.3
494.563	11.4 ± 2.1	495.063	12.3 ± 2.2	495.563	11.3 ± 2.1	496.063	10.5 ± 1.9
496.563	10.4 ± 1.9	497.063	11.0 ± 2.1	497.563	10.5 ± 1.9	498.063	10.0 ± 1.8
498.563	9.8 ± 1.8	499.063	9.7 ± 1.8	499.563	9.9 ± 1.8	500.063	10.2 ± 1.9
500.563	10.0 ± 1.8	501.063	9.9 ± 1.8	501.563	9.7 ± 1.8	502.063	9.9 ± 1.8
502.563	10.1 ± 1.9	503.063	9.7 ± 1.8	503.563	9.7 ± 1.8	504.063	10.0 ± 1.8
504.563	10.1 ± 1.8	505.063	10.2 ± 1.9	505.563	10.4 ± 1.9	506.063	10.0 ± 1.8
506.563	9.7 ± 1.8	507.063	10.1 ± 1.9	507.563	9.9 ± 1.8	508.063	9.9 ± 1.8

TABLE II: First frequency of each half Hz signal frequency band in which we set upper limits and upper limit value for that band.

2. Cleaned-out frequency bins

Cause	f_L (Hz)	Harmonics	LFS (Hz)	HFS (Hz)	IFO	Cause	f_L (Hz)	Harmonics	LFS (Hz)	HFS (Hz)	IFO
Mains	60	8	1	1	L,H	2Hz Comb	132	1	0.0006	0.0006	L,H
Wire	345	1	5	5	L	2Hz Comb	138	1	0.0006	0.0006	L,H
Wire	346	1	4	4	H	2Hz Comb	140	1	0.0006	0.0006	L,H
Electronic	85.8	1	0.01	0.01	H	2Hz Comb	142	1	0.0006	0.0006	L,H
Electronic	89.9	1	0.06	0.06	H	2Hz Comb	144	1	0.0006	0.0006	L,H
Electronic	93.29	1	0.015	0.015	L	2Hz Comb	150	1	0.0006	0.0006	L,H
Electronic	93.05	1	0.01	0.01	H	2Hz Comb	158	1	0.0006	0.0006	L,H
Electronic	93.25	1	0.01	0.01	H	2Hz Comb	154	1	0.0006	0.0006	L,H
Electronic	96.71	1	0.015	0.015	L	2Hz Comb	162	1	0.0006	0.0006	L,H
Electronic	139.94	1	0.02	0.02	L	2Hz Comb	166	1	0.0006	0.0006	L,H
Electronic	139.95	1	0.01	0.01	H	2Hz Comb	168	1	0.0006	0.0006	L,H
Electronic	145.06	1	0.02	0.02	L	2Hz Comb	170	1	0.0006	0.0006	L,H
Electronic	164.52	1	0.01	0.01	H	2Hz Comb	172	1	0.0006	0.0006	L,H
Electronic	186.59	1	0.025	0.025	L	2Hz Comb	174	1	0.0006	0.0006	L,H
Electronic	193.42	1	0.025	0.025	L	2Hz Comb	176	1	0.0006	0.0006	L,H
Electronic	233.23	1	0.05	0.05	L	2Hz Comb	178	1	0.0006	0.0006	L,H
Electronic	241.78	1	0.07	0.07	L	2Hz Comb	184	1	0.0006	0.0006	L,H
Electronic	329.58	1	0.02	0.01	H	2Hz Comb	188	1	0.0006	0.0006	L,H
Electronic	329.86	1	0.01	0.02	H	2Hz Comb	192	1	0.0006	0.0006	L,H
Violin Mode	329.32	1	0.11	0.11	L	2Hz Comb	196	1	0.0006	0.0006	L,H
Violin Mode	329.70	1	0.3	0.3	H	2Hz Comb	204	1	0.0006	0.0006	L,H
Violin Mode	335.53	1	0.28	0.28	L	2Hz Comb	206	1	0.0006	0.0006	L,H
CPU line	54.496	1	0.0006	0.0006	L,H	2Hz Comb	214	1	0.0006	0.0006	L,H
CPU line	108.992	1	0.0006	0.0006	L,H	2Hz Comb	216	1	0.0006	0.0006	L,H
Sideband Comb	140.4100	1	0.0006	0.0006	H	2Hz Comb	218	1	0.0006	0.0006	L,H
Sideband Comb	166.1205	1	0.0006	0.0006	H	2Hz Comb	221	1	0.0006	0.0006	L,H
Sideband Comb	191.8322	1	0.0006	0.0006	H	2Hz Comb	222	1	0.0006	0.0006	L,H
Sideband Comb	217.5428	1	0.0006	0.0006	H	2Hz Comb	226	1	0.0006	0.0006	L,H
Sideband Comb	243.2539	1	0.0006	0.0006	H	2Hz Comb	234	1	0.0006	0.0006	L,H
Sideband Comb	268.9650	1	0.0006	0.0006	H	2Hz Comb	236	1	0.0006	0.0006	L,H
Sideband Comb	294.6756	1	0.0006	0.0006	H	2Hz Comb	242	1	0.0006	0.0006	L,H
Sideband Comb	320.3867	1	0.0006	0.0006	H	2Hz Comb	244	1	0.0006	0.0006	L,H
Sideband Comb	346.0972	1	0.0006	0.0006	H	2Hz Comb	248	1	0.0006	0.0006	L,H
Sideband Comb	371.8077	1	0.0006	0.0006	H	2Hz Comb	252	1	0.0006	0.0006	L,H
Sideband Comb	383.6639	1	0.0006	0.0006	H	2Hz Comb	254	1	0.0006	0.0006	L,H
Sideband Comb	397.5194	1	0.0006	0.0006	H	2Hz Comb	256	1	0.0006	0.0006	L,H
Sideband Comb	409.3705	1	0.0006	0.0006	H	2Hz Comb	260	1	0.0006	0.0006	L,H
Sideband Comb	423.2306	1	0.0006	0.0006	H	2Hz Comb	262	1	0.0006	0.0006	L,H
Sideband Comb	435.0861	1	0.0006	0.0006	H	2Hz Comb	264	1	0.0006	0.0006	L,H
Sideband Comb	460.7967	1	0.0006	0.0006	H	2Hz Comb	266	1	0.0006	0.0006	L,H
Sideband Comb	486.5078	1	0.0006	0.0006	H	2Hz Comb	268	1	0.0006	0.0006	L,H
1Hz Comb	1	2000	0.0006	0.0006	L,H	2Hz Comb	270	1	0.0006	0.0006	L,H
2Hz Comb	52	1	0.0006	0.0006	L,H	2Hz Comb	274	1	0.0006	0.0006	L,H
2Hz Comb	64	1	0.0006	0.0006	L,H	2Hz Comb	278	1	0.0006	0.0006	L,H
2Hz Comb	68	1	0.0006	0.0006	L,H	2Hz Comb	280	1	0.0006	0.0006	L,H
2Hz Comb	76	1	0.0006	0.0006	L,H	2Hz Comb	282	1	0.0006	0.0006	L,H
2Hz Comb	80	1	0.0006	0.0006	L,H	2Hz Comb	286	1	0.0006	0.0006	L,H
2Hz Comb	82	1	0.0006	0.0006	L,H	2Hz Comb	290	1	0.0006	0.0006	L,H
2Hz Comb	90	1	0.0006	0.0006	L,H	2Hz Comb	298	1	0.0006	0.0006	L,H
2Hz Comb	96	1	0.0006	0.0006	L,H	2Hz Comb	308	1	0.0006	0.0006	L,H
2Hz Comb	98	1	0.0006	0.0006	L,H	2Hz Comb	312	1	0.0006	0.0006	L,H
2Hz Comb	102	1	0.0006	0.0006	L,H	2Hz Comb	316	1	0.0006	0.0006	L,H
2Hz Comb	109	1	0.0006	0.0006	L,H	2Hz Comb	320	1	0.0006	0.0006	L,H
2Hz Comb	110	1	0.0006	0.0006	L,H	2Hz Comb	334	1	0.0006	0.0006	L,H
2Hz Comb	111	1	0.0006	0.0006	L,H	2Hz Comb	372	1	0.0006	0.0006	L,H
2Hz Comb	112	1	0.0006	0.0006	L,H	2Hz Comb	376	1	0.0006	0.0006	L,H
2Hz Comb	116	1	0.0006	0.0006	L,H	2Hz Comb	380	1	0.0006	0.0006	L,H
2Hz Comb	120	1	0.0006	0.0006	L,H	2Hz Comb	384	1	0.0006	0.0006	L,H
2Hz Comb	124	1	0.0006	0.0006	L,H	2Hz Comb	394	1	0.0006	0.0006	L,H
2Hz Comb	128	1	0.0006	0.0006	L,H	2Hz Comb	402	1	0.0006	0.0006	L,H

Cause	f_L (Hz)	Harmonics	LFS (Hz)	HFS (Hz)	IFO
2Hz Comb	410	1	0.0006	0.0006	L,H
2Hz Comb	414	1	0.0006	0.0006	L,H
2Hz Comb	418	1	0.0006	0.0006	L,H
2Hz Comb	422	1	0.0006	0.0006	L,H
2Hz Comb	430	1	0.0006	0.0006	L,H
2Hz Comb	432	1	0.0006	0.0006	L,H
2Hz Comb	435	1	0.0006	0.0006	L,H
2Hz Comb	440	1	0.0006	0.0006	L,H
2Hz Comb	448	1	0.0006	0.0006	L,H
2Hz Comb	462	1	0.0006	0.0006	L,H
2Hz Comb	466	1	0.0006	0.0006	L,H
2Hz Comb	468	1	0.0006	0.0006	L,H
2Hz Comb	470	1	0.0006	0.0006	L,H
2Hz Comb	474	1	0.0006	0.0006	L,H
2Hz Comb	482	1	0.0006	0.0006	L,H
2Hz Comb	488	1	0.0006	0.0006	L,H
2Hz Comb	496	1	0.0006	0.0006	L,H
2Hz Comb	500	1	0.0006	0.0006	L,H
2Hz Comb	504	1	0.0006	0.0006	L,H
2Hz Comb	508	1	0.0006	0.0006	L,H
Digital	55.8	1	0.05	0.05	H
Digital	56.875	1	0.005	0.005	H
Digital	58.625	1	0.005	0.005	H
Digital	69.	1	0.05	0.05	H
Digital	85.375	1	0.005	0.005	H
Digital	113.75	1	0.01	0.01	H
Digital	140.24	1	0.01	0.01	H
Digital	153.75	1	0.05	0.05	H
Digital	158.0	1	0.05	0.05	H
Digital	199.57	1	0.01	0.01	H
Digital	210.36	1	0.01	0.01	H
Digital	373.5	1	0.05	0.05	H
Digital	392.2	1	0.0006	0.0006	L,H
Digital	399.3	1	0.0006	0.0006	L
Digital	401.5	1	0.05	0.05	H

TABLE III: Instrumental lines identified and “cleaned” before the Einstein@Home runs. The different columns represent: (I) the source of the line; (II) the central frequency of the instrumental line; (III) the number of harmonics; (IV) Low-Frequency-Side (LFS) of the knockout band; (V) High-Frequency-Side (HFS) of the knockout band; (VI) the interferometer where the instrumental lines were identified. Note that when there are higher harmonics, the knockout band width remains constant.

3. 50mHz signal-frequency bands that did not contribute to results

start band	stop band	disturbance type	start band	stop band	disturbance type
50.113		D	80.413	80.463	D
50.563		D	80.563	80.663	D
51.013		D	80.913		D
51.113	51.163	D	81.013	81.213	D
51.963		D	83.463		D
52.413	52.463	D	83.863		D
52.613		D	85.413		D
52.863	53.113	D	85.563		D
53.663		D	85.713	85.813	D
53.863	53.913	D	85.963		D
54.363	54.513	D	86.513		D
55.063	55.113	D	86.713	86.813	D
55.463	55.613	D	87.763		D
55.713	55.963	D	88.513		D
56.113	56.513	D	88.963		D
56.613		D	89.963	90.013	D
57.563		D	90.563	90.713	D
58.163		D	91.513		D
58.363	58.613	D	92.113		D
58.713	59.013	D	93.063	93.113	D
59.063		C	93.913	94.013	D
59.113		C D	94.213		D
59.163	60.863	C	96.663	97.163	D
60.913		C D	98.263		D
60.963	61.013	D	98.863	99.063	D
61.313	61.613	D	99.713	99.763	D
61.963		D	99.863	100.013	D
62.213	62.263	D	100.213	100.263	D
62.363		D	100.463		D
63.163	63.213	D	102.163	102.263	D
63.463	63.513	D	102.663		D
63.713		D	103.013	103.113	D
64.013	64.113	D	103.413	103.463	D
64.313	64.513	D	104.863		D
64.713	64.813	D	105.663	105.713	D
65.313	65.413	D	106.413	106.663	D
68.513		D	107.013	107.213	D
68.763	68.913	D	107.313	107.413	D
69.263		D	107.663		D
69.713	69.763	D	108.013	108.063	D
70.063	70.113	D	108.813	109.113	D
70.463	70.513	D	109.413	109.513	D
71.063		D	109.963		D
71.513		D	110.613		D
72.013	72.113	D	110.863	110.913	D
72.313	72.413	D	111.013	111.113	D
72.913	73.013	D	111.713	111.863	D
73.313	73.413	D	112.663	112.713	D
73.763	73.863	D	113.063		D
74.463	74.513	D	113.213	113.313	D
74.713		D	113.713	113.913	D
75.763		D	114.663	114.713	D
76.013	76.113	D	115.313	115.413	D
77.563	77.663	D	115.763		D
78.213	78.313	D	117.463	117.713	D
78.413	78.563	D	118.063		D
78.963	79.013	D	118.213	118.563	D
79.263		D	118.813	119.013	D
79.913	80.063	D	119.063	120.863	C

start band	stop band	disturbance type
120.963	121.013	D
121.163	121.313	D
121.613	121.763	D
122.063	122.313	D
123.113		D
125.613	125.663	D
126.213	126.313	D
126.413		D
126.713	126.813	D
127.063		D
127.963	128.013	D
128.363		D
129.713	129.763	D
129.863	129.963	D
130.513		D
131.263		D
132.713	132.763	D
133.413		D
134.013	134.063	D
134.413	134.513	D
135.063	135.163	D
135.613	135.713	D
137.063	137.113	D
137.463	137.513	D
137.613	137.913	D
138.163		D
139.463	139.513	D
139.613	139.813	D
140.113	140.213	D
140.363	140.413	D
140.963		D
141.613	141.663	D
141.813	141.863	D
142.213	142.313	D
142.613	142.713	D
144.313	144.363	D
144.613	144.763	D
145.013	145.713	D
146.313	146.363	D
146.663	146.813	D
146.913		D
147.113	147.163	D
147.713		D
148.763		D
149.113	149.213	D
149.563		D
149.963	150.013	D
150.863		D
151.263		D
152.063		D
153.163	153.313	D
153.413		D
153.613	153.713	D
153.863	153.913	D
154.213	154.263	D
155.263		D
155.763		D
156.113		D
156.213	156.263	D
156.363		D
156.513		D

start band	stop band	disturbance type
156.813	156.863	D
157.363	157.413	D
157.763		D
158.163		D
158.363		D
160.213	160.313	D
161.413	161.513	D
162.313	162.363	D
162.913	162.963	D
163.463	163.513	D
168.063	168.113	D
169.613	169.713	D
170.813		D
173.713	173.813	D
174.163		D
178.513		D
178.963		D
179.063	180.863	C
180.963	181.013	D
181.363		D
181.813	181.863	D
182.763	182.813	D
184.363	184.463	D
185.363	185.413	D
187.963		D
188.463		D
189.363	189.413	D
189.813	189.863	D
190.763	190.813	D
192.363	192.613	D
193.613	194.313	D
196.963	197.013	D
197.713	197.763	D
197.863	197.963	D
198.113	198.163	D
198.563	198.663	D
199.213	199.313	D
199.513	199.613	D
199.813	200.013	D
200.413	200.513	D
200.913	201.013	D
201.313	201.363	D
203.663		D
204.113	204.213	D
204.863	204.913	D
205.663		D
205.863		D
206.413	206.663	D
209.213	209.263	D
210.213	210.313	D
215.513		D
217.463	217.563	D
217.913	218.013	D
223.563	223.613	D
225.513	225.563	D
229.363		D
229.813	229.913	D
230.213	230.313	D
231.313	231.413	D
234.113	234.163	D
239.063	240.863	C

start band	stop band	disturbance type
241.613	241.713	D
241.813	241.863	D
242.113	242.163	D
242.313	242.863	D
246.513	246.563	D
249.963	250.013	D
253.063	253.113	D
255.063	255.113	D
257.063	257.113	D
257.263	257.363	D
259.063	259.113	D
270.163	270.213	D
270.613	270.663	D
272.413	272.513	D
275.213	275.563	D
279.763	279.813	D
280.313	280.363	D
280.813		D
281.913	282.013	D
289.363		D
290.963	291.013	D
291.213		D
291.313	291.413	D
299.063	300.863	C
306.463	306.563	D
308.463	308.513	D
324.013	324.063	D
329.113	329.263	D
329.313		C
329.463	329.863	C
332.163	332.263	D
335.163	335.263	D
335.313	335.663	C
335.713		C D
335.763		C D
335.813		C D
335.863		C
338.613	338.863	D
339.013	339.213	D
339.463	340.013	D
340.063		C D
340.113	349.863	C
349.963	350.563	D
350.663	350.763	D
350.913	351.213	D
351.363	351.563	D
357.863	357.963	D
358.913	359.063	D
359.113	360.863	C
360.913	361.013	D
365.563	365.613	D
366.513	366.613	D
366.863		D
369.763	369.813	D
370.013	370.163	D
373.263	373.313	D
373.513	373.613	D
374.163		D
374.513	374.613	D
389.513	389.613	D
391.213	391.313	D

start band	stop band	disturbance type
392.063	392.213	D
392.513	392.613	D
393.013	393.263	D
393.413	393.513	D
393.913		D
394.013	394.213	D
394.813	394.913	D
395.463	395.513	D
395.863		D
395.963	396.063	D
396.513	396.713	D
399.063	399.113	D
399.213	399.313	D
399.613	400.613	D
400.713	400.813	D
401.013	401.313	D
403.513	403.913	D
407.213	407.363	D
407.813	407.913	D
408.213	408.363	D
409.263	409.413	D
413.013	413.363	D
416.113	416.213	D
417.013	417.213	D
418.163	418.213	D
419.113	420.863	C
421.213		D
430.313		D
444.413	444.513	D
448.913		D
451.413	451.663	D
472.563	472.663	D
474.563	474.613	D
479.113	480.863	C

TABLE IV: 50-mHz search-frequency bands that were identified as disturbed based on visual inspection (D) or where the results were produced from entirely fake data as detailed in Table I (C). Both sets of bands (D and C) were excluded from the analysis. The first two columns list the first frequency of the first and last 50-mHz band in a contiguous range of excluded bands.

4. Signal-frequency ranges where the results might have contributions from fake data

line type	mixed, isolated		mixed, left		all fake data		mixed, right		detector
1Hz	50.9648	51.0352							L,H
1Hz, 2Hz	51.9647	52.0353							L,H
1Hz	52.9646	53.0354							L,H
1Hz	53.9645	54.0355							L,H
CPU	54.4605	54.5315							L,H
1Hz	54.9644	55.0356							L,H
D			55.715	55.785	55.785	55.815	55.815	55.885	H
1Hz	55.9643	56.0357							L,H
D	56.8348	56.9152							H
1Hz	56.9642	57.0358							L,H
1Hz	57.9641	58.0359							L,H
D	58.5847	58.6653							H
1Hz, M			58.964	59.0348	59.0348	60.965	60.965	61.0362	L,H
1Hz	61.9637	62.0363							L,H
1Hz	62.9636	63.0364							L,H
1Hz, 2Hz	63.9635	64.0365							L,H
1Hz	64.9634	65.0366							L,H
1Hz	65.9633	66.0367							L,H
1Hz	66.9632	67.0368							L,H
1Hz, 2Hz	67.9631	68.0369							L,H
1Hz, D			68.9136	68.9864	68.9864	69.0136	69.0136	69.0864	H
1Hz	68.963	69.037							L
1Hz	69.9629	70.0371							L,H
1Hz	70.9628	71.0372							L,H
1Hz	71.9627	72.0373							L,H
1Hz	72.9626	73.0374							L,H
1Hz	73.9625	74.0375							L,H
1Hz	74.9624	75.0376							L,H
1Hz, 2Hz	75.9623	76.0377							L,H
1Hz	76.9622	77.0378							L,H
1Hz	77.9621	78.0379							L,H
1Hz	78.962	79.038							L,H
1Hz, 2Hz	79.9619	80.0381							L,H
1Hz	80.9618	81.0382							L,H
1Hz, 2Hz	81.9617	82.0383							L,H
1Hz	82.9616	83.0384							L,H
1Hz	83.9615	84.0385							L,H
1Hz	84.9614	85.0386							L,H
D	85.332	85.418							H
E	85.752	85.848							H
1Hz	85.9613	86.0387							L,H
1Hz	86.9612	87.0388							L,H
1Hz	87.9611	88.0389							L,H
1Hz	88.961	89.039							L,H
E			89.8016	89.8784	89.8784	89.9215	89.9215	89.9985	H
1Hz, 2Hz	89.9609	90.0391							L,H
1Hz	90.9608	91.0392							L,H
1Hz	91.9607	92.0393							L,H
1Hz	92.9606	93.0394							L,H
E	93.0012	93.0988							H
E	93.2012	93.2988							H
E	93.2362	93.3438							L
1Hz	93.9605	94.0395							L,H
1Hz	94.9604	95.0396							L,H
1Hz, 2Hz	95.9603	96.0397							L,H
E	96.6559	96.7641							L
1Hz	96.9602	97.0398							L,H
1Hz, 2Hz	97.9601	98.0399							L,H

line type	mixed, isolated		mixed, left		all fake data		mixed, right		detector
1Hz	98.96	99.04							L,H
1Hz	99.9599	100.0401							L,H
1Hz	100.9598	101.0402							L,H
1Hz, 2Hz	101.9597	102.0403							L,H
1Hz	102.9596	103.0404							L,H
1Hz	103.9595	104.0405							L,H
1Hz	104.9594	105.0406							L,H
1Hz	105.9593	106.0407							L,H
1Hz	106.9592	107.0408							L,H
1Hz	107.9591	108.0409							L,H
CPU	108.951	109.033							L,H
1Hz, 2Hz	108.959	109.041							L,H
1Hz, 2Hz	109.9589	110.0411							L,H
1Hz, 2Hz	110.9588	111.0412							L,H
1Hz, 2Hz	111.9587	112.0413							L,H
1Hz	112.9586	113.0414							L,H
D	113.6992	113.8008							H
1Hz	113.9585	114.0415							L,H
1Hz	114.9584	115.0416							L,H
1Hz, 2Hz	115.9583	116.0417							L,H
1Hz	116.9582	117.0418							L,H
1Hz	117.9581	118.0419							L,H
1Hz, 2Hz, M			118.958	119.0408	119.0408	120.959	120.959	121.0422	L,H
1Hz	121.9577	122.0423							L,H
1Hz	122.9576	123.0424							L,H
1Hz, 2Hz	123.9575	124.0425							L,H
1Hz	124.9574	125.0426							L,H
1Hz	125.9573	126.0427							L,H
1Hz	126.9572	127.0428							L,H
1Hz, 2Hz	127.9571	128.0429							L,H
1Hz	128.957	129.043							L,H
1Hz	129.9569	130.0431							L,H
1Hz	130.9568	131.0432							L,H
1Hz, 2Hz	131.9567	132.0433							L,H
1Hz	132.9566	133.0434							L,H
1Hz	133.9565	134.0435							L,H
1Hz	134.9564	135.0436							L,H
1Hz	135.9563	136.0437							L,H
1Hz	136.9562	137.0438							L,H
1Hz, 2Hz	137.9561	138.0439							L,H
1Hz	138.956	139.044							L,H
E	139.8765	140.0035							L
E	139.8965	140.0035							H
1Hz, 2Hz	139.9559	140.0441							L,H
D	140.1865	140.2935							H
SB	140.3659	140.4541							H
1Hz	140.9558	141.0442							L,H
1Hz, 2Hz	141.9557	142.0443							L,H
1Hz	142.9556	143.0444							L,H
1Hz, 2Hz	143.9555	144.0445							L,H
1Hz	144.9554	145.0446							L,H
E	144.996	145.124							L
1Hz	145.9553	146.0447							L,H
1Hz	146.9552	147.0448							L,H
1Hz	147.9551	148.0449							L,H
1Hz	148.955	149.045							L,H
1Hz, 2Hz	149.9549	150.0451							L,H
1Hz	150.9548	151.0452							L,H
1Hz	151.9547	152.0453							L,H
1Hz	152.9546	153.0454							L,H
D			153.6552	153.7448	153.7448	153.7552	153.7552	153.8448	H

line type	mixed, isolated	mixed, left	all fake data	mixed, right	detector
1Hz, 2Hz	153.9545 154.0455				L,H
1Hz	154.9544 155.0456				L,H
1Hz	155.9543 156.0457				L,H
1Hz	156.9542 157.0458				L,H
1Hz, 2Hz, D		157.9047 157.9953	157.9953 158.0047	158.0047 158.0953	H
1Hz, 2Hz	157.9541 158.0459				L
1Hz	158.954 159.046				L,H
1Hz	159.9539 160.0461				L,H
1Hz	160.9538 161.0462				L,H
1Hz, 2Hz	161.9537 162.0463				L,H
1Hz	162.9536 163.0464				L,H
1Hz	163.9535 164.0465				L,H
E	164.4641 164.5759				H
1Hz	164.9534 165.0466				L,H
1Hz, 2Hz	165.9533 166.0467				L,H
SB	166.0738 166.1672				H
1Hz	166.9532 167.0468				L,H
1Hz, 2Hz	167.9531 168.0469				L,H
1Hz	168.953 169.047				L,H
1Hz, 2Hz	169.9529 170.0471				L,H
1Hz	170.9528 171.0472				L,H
1Hz, 2Hz	171.9527 172.0473				L,H
1Hz	172.9526 173.0474				L,H
1Hz, 2Hz	173.9525 174.0475				L,H
1Hz	174.9524 175.0476				L,H
1Hz, 2Hz	175.9523 176.0477				L,H
1Hz	176.9522 177.0478				L,H
1Hz, 2Hz	177.9521 178.0479				L,H
1Hz, M		178.952 179.0468	179.0468 180.953	180.953 181.0482	L,H
1Hz	181.9517 182.0483				L,H
1Hz	182.9516 183.0484				L,H
1Hz, 2Hz	183.9515 184.0485				L,H
1Hz	184.9514 185.0486				L,H
1Hz	185.9513 186.0487				L,H
E	186.5169 186.6631				L
1Hz	186.9512 187.0488				L,H
1Hz, 2Hz	187.9511 188.0489				L,H
1Hz	188.951 189.049				L,H
1Hz	189.9509 190.0491				L,H
1Hz	190.9508 191.0492				L,H
SB	191.783 191.8814				H
1Hz, 2Hz	191.9507 192.0493				L,H
1Hz	192.9506 193.0494				L,H
E	193.3462 193.4938				L
1Hz	193.9505 194.0495				L,H
1Hz	194.9504 195.0496				L,H
1Hz, 2Hz	195.9503 196.0497				L,H
1Hz	196.9502 197.0498				L,H
1Hz	197.9501 198.0499				L,H
1Hz	198.95 199.05				L,H
D	199.5106 199.6294				H
1Hz	199.9499 200.0501				L,H
1Hz	200.9498 201.0502				L,H
1Hz	201.9497 202.0503				L,H
1Hz	202.9496 203.0504				L,H
1Hz, 2Hz	203.9495 204.0505				L,H
1Hz	204.9494 205.0506				L,H
1Hz, 2Hz	205.9493 206.0507				L,H
1Hz	206.9492 207.0508				L,H
1Hz	207.9491 208.0509				L,H
1Hz	208.949 209.051				L,H

line type	mixed, isolated	mixed, left	all fake data	mixed, right	detector
1Hz	209.9489 210.0511				L,H
D	210.2995 210.4205				H
1Hz	210.9488 211.0512				L,H
1Hz	211.9487 212.0513				L,H
1Hz	212.9486 213.0514				L,H
1Hz, 2Hz	213.9485 214.0515				L,H
1Hz	214.9484 215.0516				L,H
1Hz, 2Hz	215.9483 216.0517				L,H
1Hz	216.9482 217.0518				L,H
SB	217.491 217.5946				H
1Hz, 2Hz	217.9481 218.0519				L,H
1Hz	218.948 219.052				L,H
1Hz	219.9479 220.0521				L,H
1Hz, 2Hz	220.9478 221.0522				L,H
1Hz, 2Hz	221.9477 222.0523				L,H
1Hz	222.9476 223.0524				L,H
1Hz	223.9475 224.0525				L,H
1Hz	224.9474 225.0526				L,H
1Hz, 2Hz	225.9473 226.0527				L,H
1Hz	226.9472 227.0528				L,H
1Hz	227.9471 228.0529				L,H
1Hz	228.947 229.053				L,H
1Hz	229.9469 230.0531				L,H
1Hz	230.9468 231.0532				L,H
1Hz	231.9467 232.0533				L,H
1Hz	232.9466 233.0534				L,H
E	233.1272 233.3328				L
1Hz, 2Hz	233.9465 234.0535				L,H
1Hz	234.9464 235.0536				L,H
1Hz, 2Hz	235.9463 236.0537				L,H
1Hz	236.9462 237.0538				L,H
1Hz	237.9461 238.0539				L,H
1Hz, M		238.946 239.0528	239.0528 240.947	240.947 241.0542	L,H
E		241.6564 241.7636	241.7636 241.7964	241.7964 241.9036	L
1Hz, 2Hz	241.9457 242.0543				L,H
1Hz	242.9456 243.0544				L,H
SB	243.1995 243.3083				H
1Hz, 2Hz	243.9455 244.0545				L,H
1Hz	244.9454 245.0546				L,H
1Hz	245.9453 246.0547				L,H
1Hz	246.9452 247.0548				L,H
1Hz, 2Hz	247.9451 248.0549				L,H
1Hz	248.945 249.055				L,H
1Hz	249.9449 250.0551				L,H
1Hz	250.9448 251.0552				L,H
1Hz, 2Hz	251.9447 252.0553				L,H
1Hz	252.9446 253.0554				L,H
1Hz, 2Hz	253.9445 254.0555				L,H
1Hz	254.9444 255.0556				L,H
1Hz, 2Hz	255.9443 256.0557				L,H
1Hz	256.9442 257.0558				L,H
1Hz	257.9441 258.0559				L,H
1Hz	258.944 259.056				L,H
1Hz, 2Hz	259.9439 260.0561				L,H
1Hz	260.9438 261.0562				L,H
1Hz, 2Hz	261.9437 262.0563				L,H
1Hz	262.9436 263.0564				L,H
1Hz, 2Hz	263.9435 264.0565				L,H
1Hz	264.9434 265.0566				L,H
1Hz, 2Hz	265.9433 266.0567				L,H
1Hz	266.9432 267.0568				L,H

line type	mixed, isolated		mixed, left		all fake data		mixed, right		detector
1Hz, 2Hz	267.9431	268.0569							L,H
SB	268.908	269.022							H
1Hz	268.943	269.057							L,H
1Hz, 2Hz	269.9429	270.0571							L,H
1Hz	270.9428	271.0572							L,H
1Hz	271.9427	272.0573							L,H
1Hz	272.9426	273.0574							L,H
1Hz, 2Hz	273.9425	274.0575							L,H
1Hz	274.9424	275.0576							L,H
1Hz	275.9423	276.0577							L,H
1Hz	276.9422	277.0578							L,H
1Hz, 2Hz	277.9421	278.0579							L,H
1Hz	278.942	279.058							L,H
1Hz, 2Hz	279.9419	280.0581							L,H
1Hz	280.9418	281.0582							L,H
1Hz, 2Hz	281.9417	282.0583							L,H
1Hz	282.9416	283.0584							L,H
1Hz	283.9415	284.0585							L,H
1Hz	284.9414	285.0586							L,H
1Hz, 2Hz	285.9413	286.0587							L,H
1Hz	286.9412	287.0588							L,H
1Hz	287.9411	288.0589							L,H
1Hz	288.941	289.059							L,H
1Hz, 2Hz	289.9409	290.0591							L,H
1Hz	290.9408	291.0592							L,H
1Hz	291.9407	292.0593							L,H
1Hz	292.9406	293.0594							L,H
1Hz	293.9405	294.0595							L,H
SB	294.6161	294.7351							H
1Hz	294.9404	295.0596							L,H
1Hz	295.9403	296.0597							L,H
1Hz	296.9402	297.0598							L,H
1Hz, 2Hz	297.9401	298.0599							L,H
1Hz, M			298.94	299.0588	299.0588	300.941	300.941	301.0602	L,H
1Hz	301.9397	302.0603							L,H
1Hz	302.9396	303.0604							L,H
1Hz	303.9395	304.0605							L,H
1Hz	304.9394	305.0606							L,H
1Hz	305.9393	306.0607							L,H
1Hz	306.9392	307.0608							L,H
1Hz, 2Hz	307.9391	308.0609							L,H
1Hz	308.939	309.061							L,H
1Hz	309.9389	310.0611							L,H
1Hz	310.9388	311.0612							L,H
1Hz, 2Hz	311.9387	312.0613							L,H
1Hz	312.9386	313.0614							L,H
1Hz	313.9385	314.0615							L,H
1Hz	314.9384	315.0616							L,H
1Hz, 2Hz	315.9383	316.0617							L,H
1Hz	316.9382	317.0618							L,H
1Hz	317.9381	318.0619							L,H
1Hz	318.938	319.062							L,H
1Hz, 2Hz	319.9379	320.0621							L,H
SB	320.3246	320.4488							H
1Hz	320.9378	321.0622							L,H
1Hz	321.9377	322.0623							L,H
1Hz	322.9376	323.0624							L,H
1Hz	323.9375	324.0625							L,H
1Hz	324.9374	325.0626							L,H
1Hz	325.9373	326.0627							L,H
1Hz	326.9372	327.0628							L,H

line type	mixed, isolated	mixed, left	all fake data	mixed, right	detector
1Hz	327.9371 328.0629				L,H
1Hz	328.937 329.063				L,H
VM		329.1476 329.2724	329.2724 329.3676	329.3676 329.4924	L
1Hz, E, VM		329.3376 329.4624	329.4624 329.9381	329.9381 330.0631	H
1Hz	329.9369 330.0631				L
1Hz	330.9368 331.0632				L,H
1Hz	331.9367 332.0633				L,H
1Hz	332.9366 333.0634				L,H
1Hz, 2Hz	333.9365 334.0635				L,H
1Hz	334.9364 335.0636				L,H
VM		335.187 335.313	335.313 335.747	335.747 335.873	L
1Hz, VM		335.437 335.563	335.563 335.9375	335.9375 336.0637	H
1Hz	335.9363 336.0637				L
1Hz	336.9362 337.0638				L,H
1Hz	337.9361 338.0639				L,H
1Hz	338.936 339.064				L,H
1Hz, VM		339.9359 340.0629	340.0629 349.9361	349.9361 350.0651	L
1Hz	339.9359 340.0641				H
1Hz	340.9358 341.0642				H
1Hz, SB, VM		341.9357 342.0631	342.0631 349.9361	349.9361 350.0651	H
1Hz	350.9348 351.0652				L,H
1Hz	351.9347 352.0653				L,H
1Hz	352.9346 353.0654				L,H
1Hz	353.9345 354.0655				L,H
1Hz	354.9344 355.0656				L,H
1Hz	355.9343 356.0657				L,H
1Hz	356.9342 357.0658				L,H
1Hz	357.9341 358.0659				L,H
1Hz, M		358.934 359.0648	359.0648 360.935	360.935 361.0662	L,H
1Hz	361.9337 362.0663				L,H
1Hz	362.9336 363.0664				L,H
1Hz	363.9335 364.0665				L,H
1Hz	364.9334 365.0666				L,H
1Hz	365.9333 366.0667				L,H
1Hz	366.9332 367.0668				L,H
1Hz	367.9331 368.0669				L,H
1Hz	368.933 369.067				L,H
1Hz	369.9329 370.0671				L,H
1Hz	370.9328 371.0672				L,H
SB	371.7405 371.8749				H
1Hz, 2Hz	371.9327 372.0673				L,H
1Hz	372.9326 373.0674				L,H
D	373.3832 373.6168				H
1Hz	373.9325 374.0675				L,H
1Hz	374.9324 375.0676				L,H
1Hz, 2Hz	375.9323 376.0677				L,H
1Hz	376.9322 377.0678				L,H
1Hz	377.9321 378.0679				L,H
1Hz	378.932 379.068				L,H
1Hz, 2Hz	379.9319 380.0681				L,H
1Hz	380.9318 381.0682				L,H
1Hz	381.9317 382.0683				L,H
1Hz	382.9316 383.0684				L,H
SB	383.5955 383.7323				H
1Hz, 2Hz	383.9315 384.0685				L,H
1Hz	384.9314 385.0686				L,H
1Hz	385.9313 386.0687				L,H
1Hz	386.9312 387.0688				L,H
1Hz	387.9311 388.0689				L,H
1Hz	388.931 389.069				L,H
1Hz	389.9309 390.0691				L,H

line type	mixed, isolated	mixed, left	all fake data	mixed, right	detector
1Hz	390.9308 391.0692				L,H
1Hz	391.9307 392.0693				L,H
D	392.1307 392.2693				L,H
1Hz	392.9306 393.0694				L,H
1Hz, 2Hz	393.9305 394.0695				L,H
1Hz	394.9304 395.0696				L,H
1Hz	395.9303 396.0697				L,H
1Hz	396.9302 397.0698				L,H
SB	397.4496 397.5892				H
1Hz	397.9301 398.0699				L,H
1Hz	398.93 399.07				L,H
D	399.23 399.37				L
1Hz	399.9299 400.0701				L,H
1Hz	400.9298 401.0702				L,H
D	401.3804 401.6196				H
1Hz, 2Hz	401.9297 402.0703				L,H
1Hz	402.9296 403.0704				L,H
1Hz	403.9295 404.0705				L,H
1Hz	404.9294 405.0706				L,H
1Hz	405.9293 406.0707				L,H
1Hz	406.9292 407.0708				L,H
1Hz	407.9291 408.0709				L,H
1Hz	408.929 409.071				L,H
SB	409.2995 409.4415				H
1Hz, 2Hz	409.9289 410.0711				L,H
1Hz	410.9288 411.0712				L,H
1Hz	411.9287 412.0713				L,H
1Hz	412.9286 413.0714				L,H
1Hz, 2Hz	413.9285 414.0715				L,H
1Hz	414.9284 415.0716				L,H
1Hz	415.9283 416.0717				L,H
1Hz	416.9282 417.0718				L,H
1Hz, 2Hz	417.9281 418.0719				L,H
1Hz, M		418.928 419.0708	419.0708 420.929	420.929 421.0722	L,H
1Hz, 2Hz	421.9277 422.0723				L,H
1Hz	422.9276 423.0724				L,H
SB	423.1582 423.303				H
1Hz	423.9275 424.0725				L,H
1Hz	424.9274 425.0726				L,H
1Hz	425.9273 426.0727				L,H
1Hz	426.9272 427.0728				L,H
1Hz	427.9271 428.0729				L,H
1Hz	428.927 429.073				L,H
1Hz, 2Hz	429.9269 430.0731				L,H
1Hz	430.9268 431.0732				L,H
1Hz, 2Hz	431.9267 432.0733				L,H
1Hz	432.9266 433.0734				L,H
1Hz	433.9265 434.0735				L,H
1Hz, 2Hz	434.9264 435.0736				L,H
SB	435.0125 435.1597				H
1Hz	435.9263 436.0737				L,H
1Hz	436.9262 437.0738				L,H
1Hz	437.9261 438.0739				L,H
1Hz	438.926 439.074				L,H
1Hz, 2Hz	439.9259 440.0741				L,H
1Hz	440.9258 441.0742				L,H
1Hz	441.9257 442.0743				L,H
1Hz	442.9256 443.0744				L,H
1Hz	443.9255 444.0745				L,H
1Hz	444.9254 445.0746				L,H
1Hz	445.9253 446.0747				L,H

line type	mixed, isolated	mixed, left	all fake data	mixed, right	detector
1Hz	446.9252 447.0748				L,H
1Hz, 2Hz	447.9251 448.0749				L,H
1Hz	448.925 449.075				L,H
1Hz	449.9249 450.0751				L,H
1Hz	450.9248 451.0752				L,H
1Hz	451.9247 452.0753				L,H
1Hz	452.9246 453.0754				L,H
1Hz	453.9245 454.0755				L,H
1Hz	454.9244 455.0756				L,H
1Hz	455.9243 456.0757				L,H
1Hz	456.9242 457.0758				L,H
1Hz	457.9241 458.0759				L,H
1Hz	458.924 459.076				L,H
1Hz	459.9239 460.0761				L,H
SB	460.7206 460.8728				H
1Hz	460.9238 461.0762				L,H
1Hz, 2Hz	461.9237 462.0763				L,H
1Hz	462.9236 463.0764				L,H
1Hz	463.9235 464.0765				L,H
1Hz	464.9234 465.0766				L,H
1Hz, 2Hz	465.9233 466.0767				L,H
1Hz	466.9232 467.0768				L,H
1Hz, 2Hz	467.9231 468.0769				L,H
1Hz	468.923 469.077				L,H
1Hz, 2Hz	469.9229 470.0771				L,H
1Hz	470.9228 471.0772				L,H
1Hz	471.9227 472.0773				L,H
1Hz	472.9226 473.0774				L,H
1Hz, 2Hz	473.9225 474.0775				L,H
1Hz	474.9224 475.0776				L,H
1Hz	475.9223 476.0777				L,H
1Hz	476.9222 477.0778				L,H
1Hz	477.9221 478.0779				L,H
1Hz, M		478.922 479.0768	479.0768 480.923	480.923 481.0782	L,H
1Hz, 2Hz	481.9217 482.0783				L,H
1Hz	482.9216 483.0784				L,H
1Hz	483.9215 484.0785				L,H
1Hz	484.9214 485.0786				L,H
1Hz	485.9213 486.0787				L,H
SB	486.4291 486.5865				H
1Hz	486.9212 487.0788				L,H
1Hz, 2Hz	487.9211 488.0789				L,H
1Hz	488.921 489.079				L,H
1Hz	489.9209 490.0791				L,H
1Hz	490.9208 491.0792				L,H
1Hz	491.9207 492.0793				L,H
1Hz	492.9206 493.0794				L,H
1Hz	493.9205 494.0795				L,H
1Hz	494.9204 495.0796				L,H
1Hz, 2Hz	495.9203 496.0797				L,H
1Hz	496.9202 497.0798				L,H
1Hz	497.9201 498.0799				L,H
1Hz	498.92 499.08				L,H
1Hz, 2Hz	499.9199 500.0801				L,H
1Hz	500.9198 501.0802				L,H
1Hz	501.9197 502.0803				L,H
1Hz	502.9196 503.0804				L,H
1Hz, 2Hz	503.9195 504.0805				L,H
1Hz	504.9194 505.0806				L,H
1Hz	505.9193 506.0807				L,H
1Hz	506.9192 507.0808				L,H

line type	mixed, isolated	mixed, left	all fake data	mixed, right	detector
1Hz, 2Hz	507.9191 508.0809				L,H
1Hz	508.919 509.081				L,H

TABLE V: Signal frequency ranges where the results might have contributions from fake data. When the results are entirely due to artificial data, the band is listed in the “all fake data” column; bands where the results comprise contributions from both fake and real data are listed in the other three columns. The “mixed, left” and “mixed, right” columns are populated only when there is a matching “all fake data” entry, which highlights the same physical cause for the fake data, i.e., the cleaning. The “mixed, isolated” column lists isolated ranges of mixed data. The list of input data frequencies where the data was substituted with artificial noise are given in Table I.